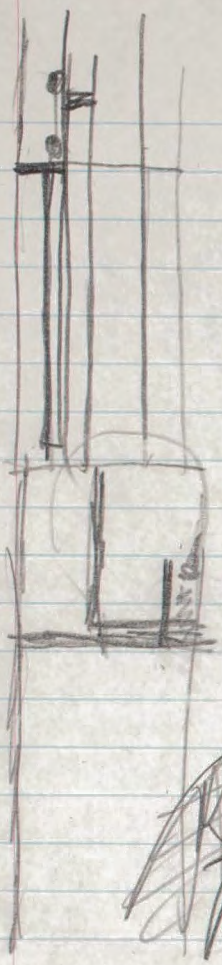
	Mel.	Carb	~~el. cond.~~ resist	W
U	1150C°	(4200)	Microhm cm	
Pu				
Ta	2977	—	71[1500]; 102[2500]	4.19
Mo	2610	4700	46[1500] 77[2500]	4.2
Ni				
Os	2700	5500	9.5[20]	4.55
Cu				
Al	660		7.30[400]	
Ag	960	2210	9.3 [1100]	
W	3370C	5900C	65 [2000]	4.52
Zirc.	1845	(4900)		
Caes.	29.7	700		
Cu	1083	(2590)	2.93(200)	
Gold	1063	(2950)		
Ruth	(2500)	(4900)		
Va	750	(3350)		
Zi	1845	(4900)		4.21
Th	1850	(3500)		3.35
C	3550	4200	1100[2000]	

Hydrides W, | Ta solubl. in U or Pu



$15 \times 50 \times = 10^4$

$750 X = 10^4$

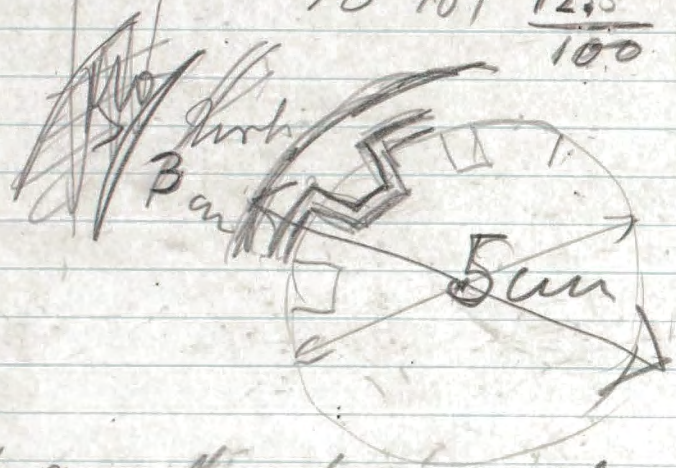
~~14.3~~ amps / cm² for 10 KW units

$H_0 = \frac{KW}{15 \times 20} = \frac{KW}{300} = 30$ gauss for 10 KW / per unit

$H_0 = 300$ gauss for 100 KW / per unit

10 104 $\frac{12.5}{100} \frac{1}{20} \frac{}{100}$ cm² = $\frac{A}{B}$

$\frac{125}{20} = 5 cm^2$



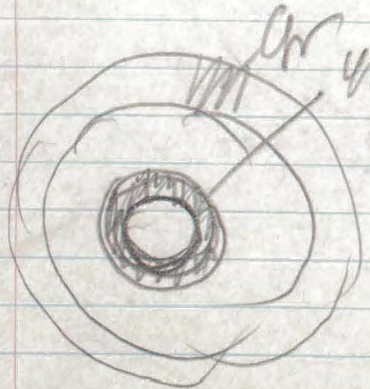
Cut armature

50 cm²

$2\pi (R_2 - R_1)^2 = 60$

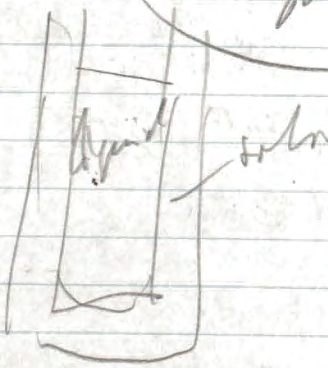
$(R_2 - R_1)^2 = 10$

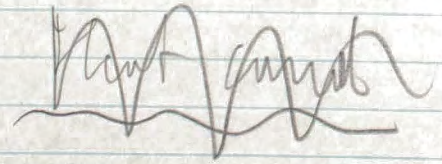
$R_2 - R_1 \approx 3$ cm



"Yes" = ~~50~~ 50 / optimum

Minimum wheat price





Melting Points

	mp	bp
Cr	1850	2430
Zr	2443	5300
Pt	1769	4500
Rhe	3145	=
Rhod	1960	4500
Ru Th	2500	(4900)
Ta	2977	—
Th	1850	3500
W	3380	(6700)
Va	1750	
Zi	1845	
Ti	1730	3260

	Low melt		High boil
3.75	Ba	710	(1800)
1.54	Ca	850	1690
2.63	Sr	770	(1360)
1.84	Be	1284	2967
2.7	Al	660	(2500)
6.68	Sb	630	(1640)

Melting points 1000 or less
above vapour press at 1000 ≈ two Atm

Bi	271	1560
Cd	(800)	(2500)
Co	1083	2590
Ga	29.8	2070

Heat conductivity

4

0.0004

Argon. Calc.

2.5 $4 \cdot 10^{-5}$ ~~0.0004~~ ~~cal~~ / cm° $\frac{1}{\alpha}$ = ~~25~~ cal ≈ 20 watt / cm

λ 10^{-5} cm 1 Ohm for A

10^{-2} cm $\frac{1}{1000}$ Ohm

$\frac{1}{22000}$ $\frac{N_1}{N_0}$ ~ N_0

$e^{-\frac{W}{6000}}$ / Δ 5 cm → $e^{\frac{W}{RT}\frac{\Delta T}{T}}$

$\frac{e^{-\frac{W}{RT}}}{e^{-\frac{W}{R(T+\Delta T)}}}$

$e^{+\frac{24}{T}\frac{\Delta T}{T}}$

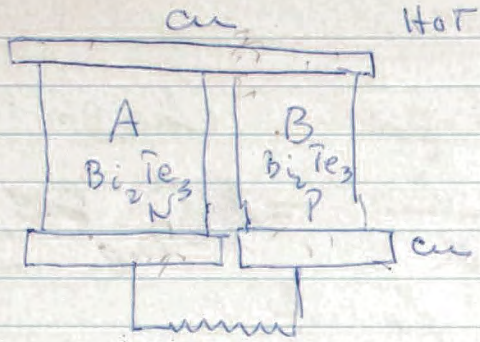
$\left(1 + \frac{24}{1000}\right)^{100}$

Compute output W argon

$\frac{1}{3} v \cdot \frac{10^{-5}}{22000} \frac{3}{2} k$ $\frac{1}{cm} = 10^{-5}$ Ohm

$= \frac{1}{6} \frac{4 \times 10^4}{2.2 \cdot 10^4} 10^{-5} \frac{3}{2} 600 =$

$\frac{1}{3} \frac{4 \cdot 10^4}{2.2 \cdot 10^4} 10^{-5} \frac{3}{2} 2 = \frac{4}{6.6} 3 \cdot 10^{-5} = \boxed{2 \cdot 10^{-5}}$



10^2 ohm^{-1} cm^{-1}

$$\frac{\alpha^2 \sigma T}{K}$$

$\frac{200\ \mu V}{^\circ C}$

600 °C 200 10^{-6}

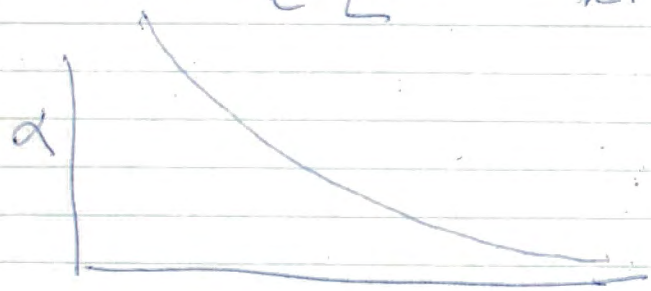
12 pairs

0.12 Volts

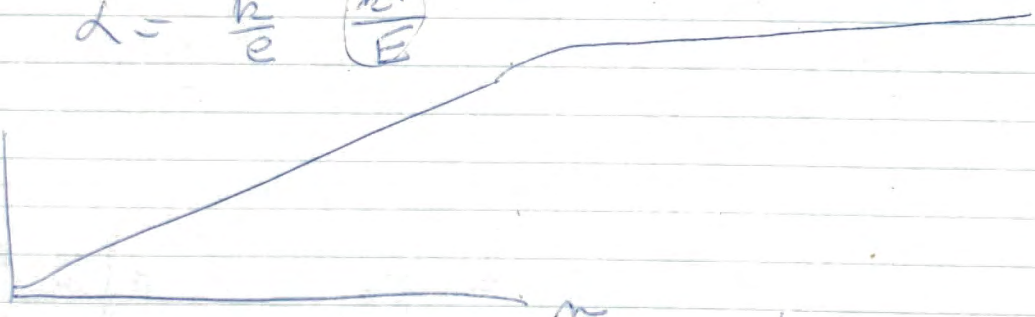
12%

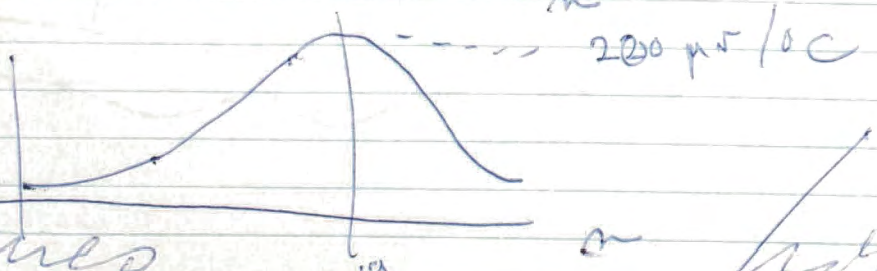
S.C

$$\alpha = \frac{k}{e}\left[2 + \frac{\Delta E}{kT}\right]$$



might $\alpha = \frac{k}{e}\left(\frac{kT}{E}\right)$



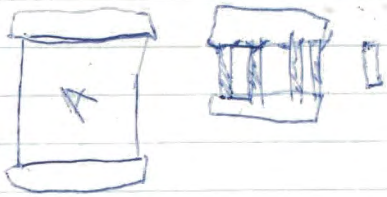


100 times

Intrinsic Resistivity

Mary Beth Sterns
Valley Watson

RCA
Los Alamos
Hal Lewis
Jaffe Lewis



Pl. 91686
Kerst

230

Ted Taylor

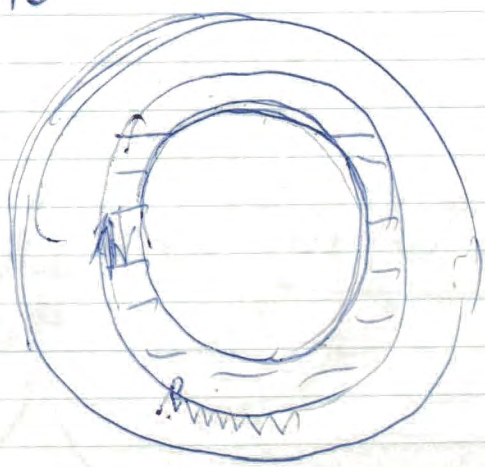
Hal Lewis
Rosenbluth
Kerst

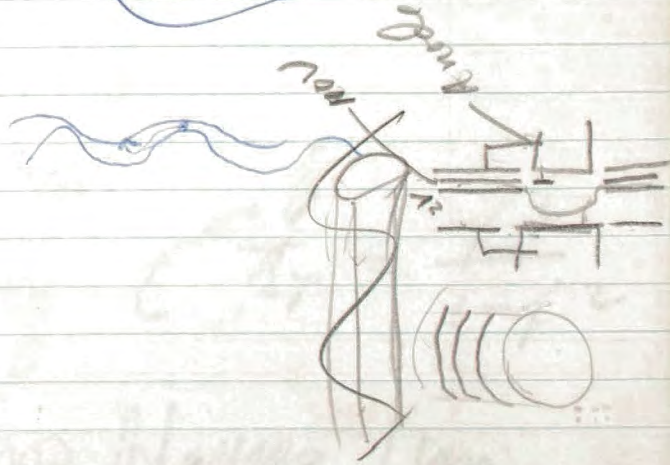
Dave Rose
Fortescue (Peter)
Simmad
Duffield

10^{-3} Ohm cm
1 Ohm $\kappa = 10^{-5}$

$\frac{1}{10}$ 10^{-3} Ohm 1 cm

$\frac{1}{100}$ cm





Argon ~~0.0000~~ $\frac{4 \times \sqrt{10}}{\sqrt{3}}$

$8 \times 10^{-5} \quad 10^{3} \quad 10^{2} = \frac{8\ \text{cal}}{\text{cm}^2}$ / $\frac{30\ \text{watt}}{\text{cm}^2}$

$$\frac{f^2}{1-f^2} = \frac{3 \times 10^4}{p_{m/m}(T, N_0)} \left(\frac{T}{3000}\right)^{5/2} e^{-\frac{3.8\ \text{volts}}{RT\ (\text{volts})}}$$

$\frac{\text{ion}}{\text{cm} \times \text{ohm}}$

total pressure

or

$$\sigma = \frac{10^{-12}}{(eV)^2}\ \text{cm}^2$$

10^2 el/cc $\quad L = 1$ cm

$$\frac{2kT}{p} \frac{(2\pi m kT)^{3/2}}{h^3} e^{-\frac{eV}{kT}} = \frac{f^2}{1-f^2}$$

$h = 6 \times 10^{-27}$

Los Alamos, 1 cm
Mobility

gain $\frac{1}{2}$ i Watt

at 10 ~~Amps~~/cm² ~~5 Volt~~ 5 Watt

at 30 " " 15 Watt

at $T_{ions} = 2300$ has $(2.43-1)$ 18 Watt = too much!

$$\frac{Q_1 - Q_2}{Q_1} = \frac{T_1 - T_2}{T_1}$$

Heat cond p. Coe

0.0002 1000° C 0.2 cal per cm² for 2 cal per cm diff 1000° C

$\frac{3}{2}\ \frac{1}{10}$ $\frac{d\ v}{22000}$ $\frac{N}{N_0}$ $\frac{3}{2}$ $\frac{R\ N_0}{R}$ $\frac{1}{d}$ $\frac{1}{1000}$ cm 1 Ohm

$\frac{1}{10}\ \frac{1}{10}$ $\frac{3}{22}\ \frac{3}{2}$ 6000 v = $\frac{1}{10}$ Ohm $\frac{1}{1000}$ cm

$\frac{3}{44}$ 60 = 3 cal

$CO_2 = \frac{33}{12}$ 1 cm / 1

$\frac{3 \times 50}{}$ 0.00017 $\phi\ \frac{3}{2}$ $\frac{1}{100}$ Ohm

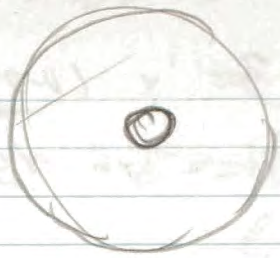
$4\ 10^{-5}$ ~~$4\ 10^{-2}$ cal~~ 4 cal $4\ 10^{-5}$

$\frac{1}{100}$ cm η $i = 30$ 100 Watt loss at cathode

$\frac{1}{100}$ Ohm $\frac{1}{100}$ cm

$\frac{1}{100}$ Ohm i_0^{-2} cm

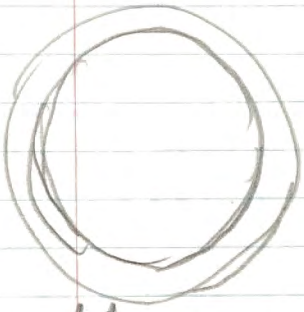
Radiation



T_1

Lower by factor 4 T_1 lowered by 120°C°

Abs/cm² of inside $\frac{\text{Block at } T_1}{30}$ (or $\frac{\text{Block at } T_1}{4}$ if Wooded)



If both coated

$\frac{\text{Block}}{4}$ at T_2

H depends only on i and l

$$H = \frac{1}{10}\frac{il}{2}$$

Radiation $A\,4T^3\Delta T = \frac{AT^4}{108}$

$4\Delta T = T$

$\Delta T = \frac{T}{4\times 8} = \frac{T}{50} = \frac{2000}{40}$

T_{abs} 2000 = 90 Watt/8 = 11.2 Watt/cm²

$T_{abs} = 2300$ = 1.7 × 11.2 Watt/cm²

= 19 Watt/cm²

$T_{abs} = 3000$ 100 Watt/cm²

Atomic hydrogen welding

½ Volt higher at 4 Volt makes ½ in T

½ = makes increase in Radiation factor 2.43

$\frac{20\ cm^2}{10}$ 4 $\frac{200\ 000}{3 \times 100}$ Watts $= 2.6\ 10^5$ Watt $= \underline{260}$ KWatt

2.6K Watt

transmission length 10 cm

transmission

$1\ mm \times \underline{200\ mm} = 200\ (mm)^2$

10 cm length upper end only — 1 Volt = $\gamma_{max} = \underline{2000\ \#/mm^2}$

$\gamma_{max} = 2\pi\tau \frac{530}{2}$

5300

1 Volt Hg = 34 mm for H = 25 gauss

1/6 Volt Hg = 13.6 mm

H = 25 gauss $\rho = 0.5\ mm$

$$\frac{n}{l}\frac{v}{3}W = 30 \times 3\,10^{9}\ \text{dyn/stat}\ (30\ \text{dyne})$$

10^{-3}

Assume v corresp 1 Volt $= 2\,10\ 3\,10$

$\frac{1}{3} n \frac{6\,10^{7}}{1} \frac{1}{20} = 10^{11} \frac{1}{5} 10^{10} = 6\,10^{7}$ amp/cc

$n\ 10^{6}$ amp/cc $= 2\,10^{20}$

$n = \underline{2\,10^{14}}$

ρ: mean free path in Cu

$10^{14}\ 10^{-14} = \frac{1}{20}$

$n\sigma = 2$

mean free path $\frac{1}{2}$ cm if $\Pi = n$

could $\frac{1}{10}$ we Coes Dans^2?

1 unit 10 KWatts

$r = 3$ cm $\quad i = 53$ Amps/cm² for $l = 10$ cm

$2\pi r \approx 19$ cm² $\quad i = 26$ Amps/cm² for $l = 20$

$\underline{\underline{il = 530 \text{ Amp}}}$

~~Watts~~ $H_{max} = 2\pi r \frac{530}{2}$

$l = 10$ cm

$\overline{\overline{H}} = 2\pi r \frac{530}{4}$

$H_{max} = \frac{53}{2} = \underline{26 \text{ Watts}}$

$H_{max} = \frac{1}{2\pi r^2} \frac{1 \text{ Watts}}{\text{Volts}} \frac{1}{10}$

for given watts per unit H is inversely prop to r

l could be made longer for lower i if Watts fixed

$l = 20$ cm $\quad \overline{\overline{H}} = 2\pi r \frac{530}{4}$

Copper $= F$ cm²

$\frac{1}{10} \frac{1}{20} \frac{1}{F} \frac{1}{100} \frac{19 \times 530}{4} = \frac{1}{10}$ Volt

$F = \frac{1}{20} \frac{10^4}{100 \times 4} = 1.2$ cm²

corresponding W wall $20 \times 1.2 = 22$ cm²

1 cm wall $\underline{r = 3 \text{ cm}}$

heat transfer 1.3×10^{15} v

$v = 218 \text{ cm/sec} \times 3 = 660 \text{ cm/sec}$, [at 3000 = 1 atm]

$1.3 \times 10^{15} \times 660 \times 10 \; \frac{3}{2} k T$ $\quad k = \frac{R}{6 \times 10^{23}}$

$= \frac{3}{2} \frac{1.3 \times 10^{15} \times 660 \times 10 \times 600 \times 10}{6 \cdot 10^{23}} =$

$\frac{2 \times 40 \times 10^{21}}{6 \cdot 10^{23}} = \frac{2}{60} = \frac{1}{10} \text{ cal/cm}^2$ | 1 m gap

Radiation per cm^2 at $T_{atm} = 2000$ 90 Watts black

and with 0.03 reflect 3 Watts/cm^2

1 Amp: ~~Useful 0.7 Watt~~

Total 3 Watts

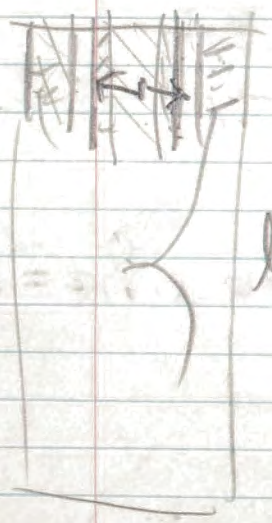
+ 1 Watt

Wilson 0.7 Volt

1.3 Amps.

$1.3 \times 9.2 = 7$

$\frac{+3}{10}$



$i \geq 1$ Amps

$i \, 2\pi r R \, V = \text{Watts}$ { 1000 KWatts / 1 power KWatts

1 Unit < 10 KW / 100 KW — 1 or Units

$i = 1$ Amps | $i = 30$ Amps

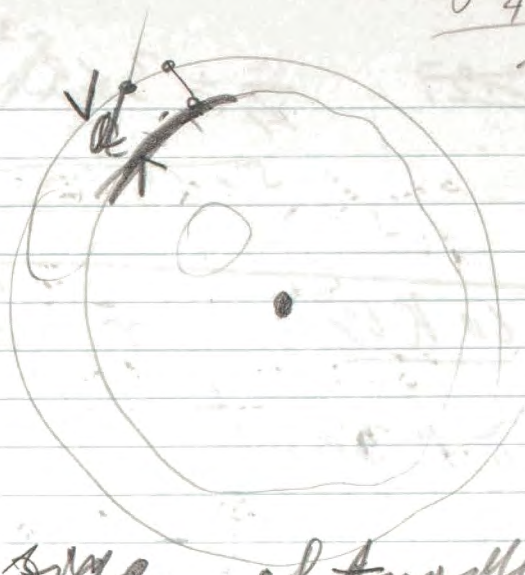
$l = 10$ cm

$\#A \, 2\pi r i = 1000$

$\pi i = \frac{1000}{2\pi} = 160$

$\sigma 4\pi r^2$

r, $4\pi r dr$ is Pot



The minimum size of nuclei:
Plum loss determined

heat transport

corresponds to R

$\frac{v}{3}\frac{N}{N_0}\frac{3}{2}\frac{K N_0}{22000}\frac{2000}{1000}\frac{1}{}$

10^4

$\nu = 10^4$ | $\frac{3}{4}\frac{10}{22000}$ cal/grade

$\frac{1}{20000}$ cal/grade

$\frac{v}{3}\frac{3}{2} R N$

$\frac{1}{10} N 10^{-16} = \frac{1}{10^{17}}$

$N =$

$5.6\ 10^{-6}$ cm $\quad \frac{1}{1\text{km}}$ | $\frac{1}{1000}$ km $\quad 5.6\ 10^{-3}$ cm

$6 = (3.42)^2 \pi\ 10^{-16}$ $\quad \rho = \frac{1}{x}$ km

$x\ 5.6\ 10^{-6}$ cm $= \frac{1}{10}$ cm

$x = \frac{10^6}{56} \approx 10^4$ | $N = \frac{6\ 10^{23}}{22{,}400 \times 2\ 10^4}$

$N = \frac{6}{4\pi} = 1.3\ 10^{15}$ $\quad \nu = 1$ mm

1 Volt ||

$\frac{v}{H} = 2\,10^{-3} \times 3\,10^{10} = 6\,10^{+7}$ cm/sec

5×10 cm/sec $50 = 25 \times 10^{6}$

Try 10 KW $\quad r = 3 \quad i = 30$

$10^4 = 2\pi r\, 30 \cdot l$ $\quad l = \frac{10^4}{60} = 166.5$ cm

$2\pi \cdot 30$

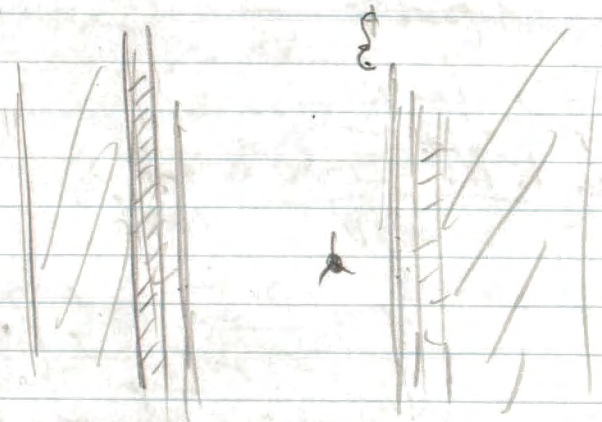
600

10000 Amp $\quad M = \frac{10^4}{2 \times 3 \cdot 2\pi \cdot 10} = \frac{10^4}{400} = 25$ Gauss

Ohmic Loss: $\frac{1}{4}$ Watts / Volts $\quad$ Res. $= \frac{1}{10}$

$\text{Res} = \frac{\frac{1}{2} l}{100} \frac{1}{\pi r 100}$ $\quad \frac{1}{20} \simeq \frac{1}{100} \frac{1}{100} 20 \frac{1}{10}$

$= \frac{1}{20}\, 10^{-4}$



$\frac{1}{2} 2\pi r i \cdot l = \mathcal{Y}$ (for H)

$H = \frac{1}{20} i l$

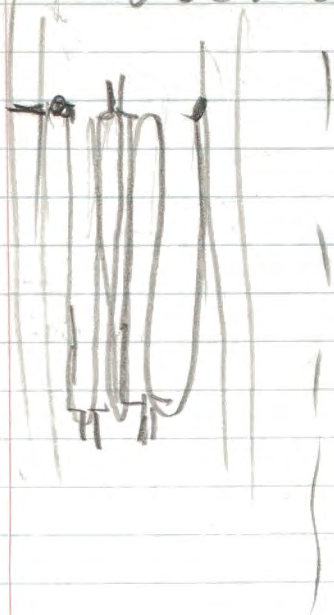
$\mathcal{Y}_{max} = \frac{1}{2} i l 2\pi r$

Watts $= i l$ Volts $2\pi r$

$\frac{1}{2}$ Watts / Volts $= \mathcal{Y}_{max} 2\pi r$

$\frac{1}{100} = N$

Double duralumin tube



Coils
of small gap
and coil for
rest work to
be cut out

~~Hg~~ $\gamma = 40 \times 30 = 10^3$

$M = \frac{100}{2\pi} = 10$

Hg 1 Volt = 3.3 mm

Min current density 1 Amps
~~Assin~~ ~~Hg~~ and ~~A = 1000~~ π
current density at surface at knife = i
current at ~~knife~~ upper and lower
end of unit

$\gamma > \frac{1}{2} 2\pi r l$

$\gamma = \frac{1}{2} 2\pi r l \, i$ (10)

$\gamma V > 2\pi r l$ ~~watt~~

$\gamma V \geq 2\pi r \, i \, l$ Watt

~~Hg~~ $\frac{\text{Watt}}{\text{Volt}} = 2\pi r i$ (10) mm

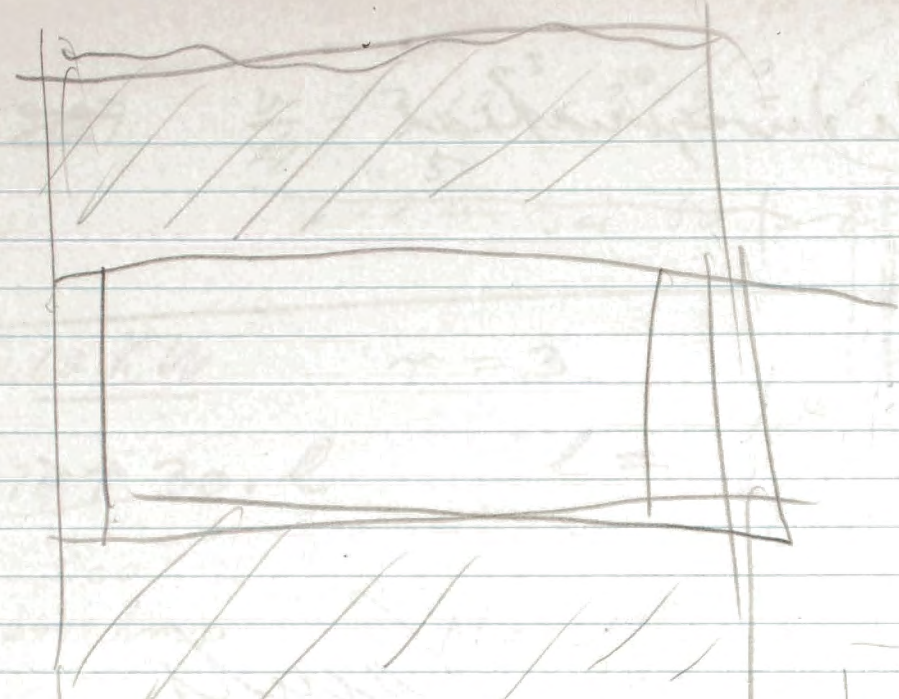
$r < \frac{1}{2\pi} \frac{\text{Watt}}{\text{Volt}} \frac{1}{i} \frac{1}{10}$

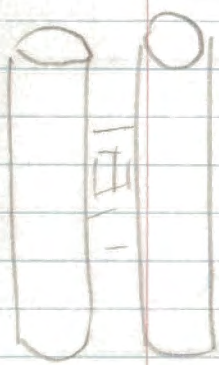
$r = \frac{1}{l = 20}$ $\gamma > 120$ Amp

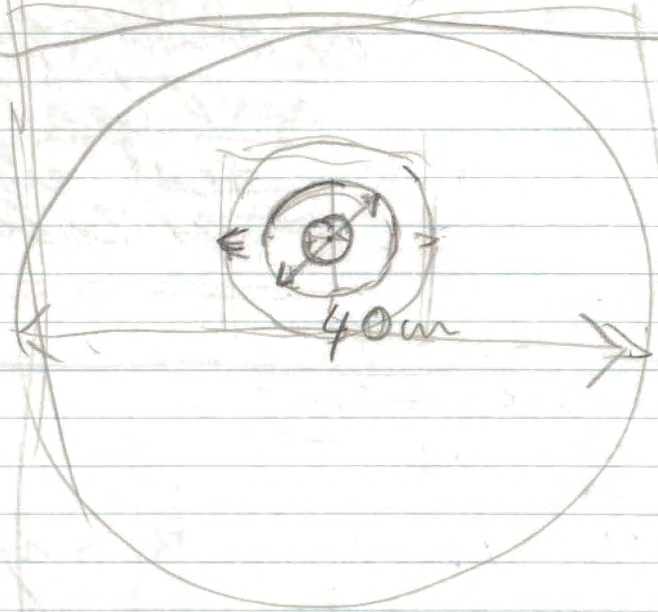
$\gamma_0 \simeq$ ~~AWM~~ $\parallel$ Watts $\times \frac{1}{\text{Volt}}$ $\frac{1}{2}$ 10 KW

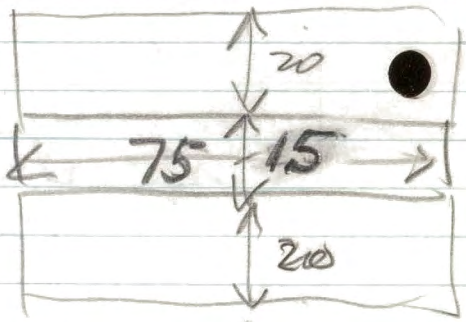
$r < 3$ cm

$H = \frac{1}{2} \frac{\text{Watts}}{\text{Volts}} \frac{1}{2\pi r} \frac{1}{10}$

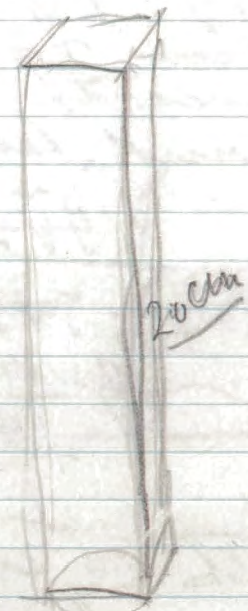








30 × 4 × 20
3,000 watt
3kw



~~100~~ 2 $\frac{0.1 \times 1000}{10}$ cal
10
100 watt
10 cal/sec
20 cal 80 watt

~~3/4~~ $\frac{1}{2}$ m²

300 watt

100 m² 30 amps

1.5

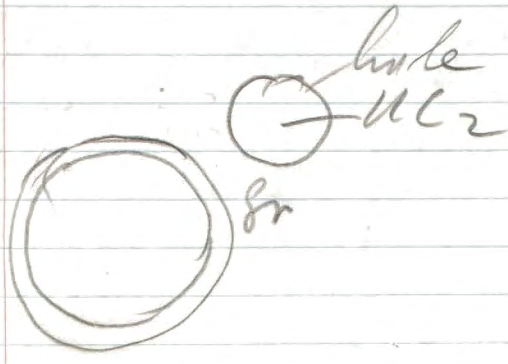
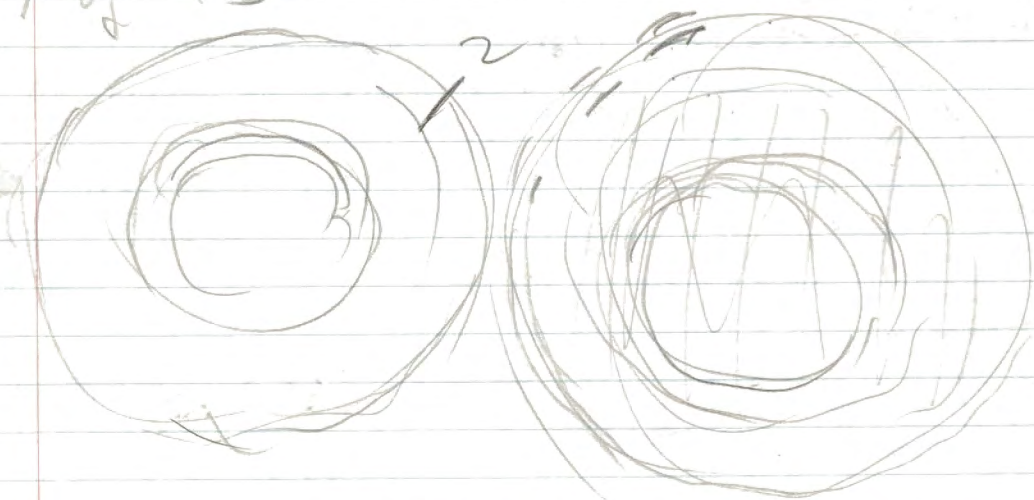
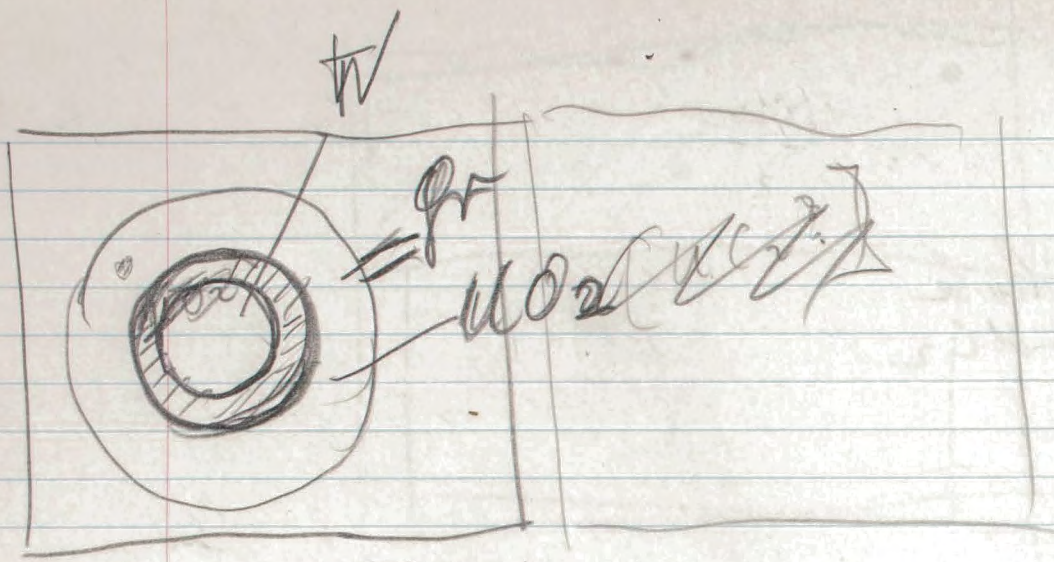
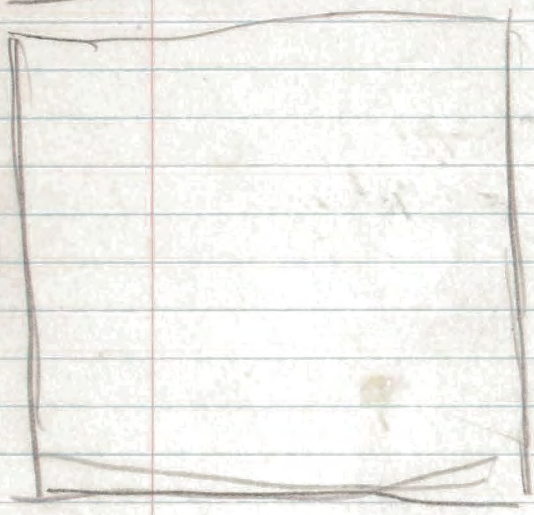
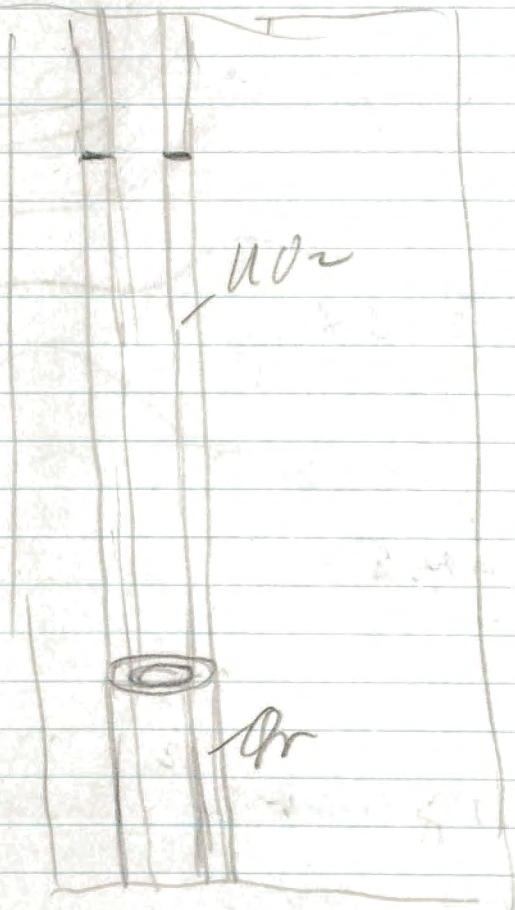


Fig 4B









for U (not Pu, Pu requires less

Since $M_c = 60\left(\frac{S_f}{11.3}\right)^{-2}$ Kg

60 Kg density 10 ≡ 6 liter

We take 20 liter ; 30 cm length for tubes

15 cm

(1 cm²)

Volt = 10 × 1/2 × 1/6.5 × 1/100 × 1/20

Cu

2 × 6.5 × 10 × 20 = 2600 Amps permitted

Surface ~ 60 cm² 2600/60 = 44 Amps/cm² at anode

at cathode 1/5 44 Amps/cm² = 5156

24 − 2

Co 5-2010 } 730 KW Inverter }
Mo 2-1513 }

"Cathode" "Cathode"

"anode"

Maintain a density gradient along tube Anode

Na

Core

alternative

output per tube = ~~XXXXXXXXXX~~ 5 KW ~~XXXXXX~~

100 tubes 500 KW

Estimate

4 cm² 25 cm length

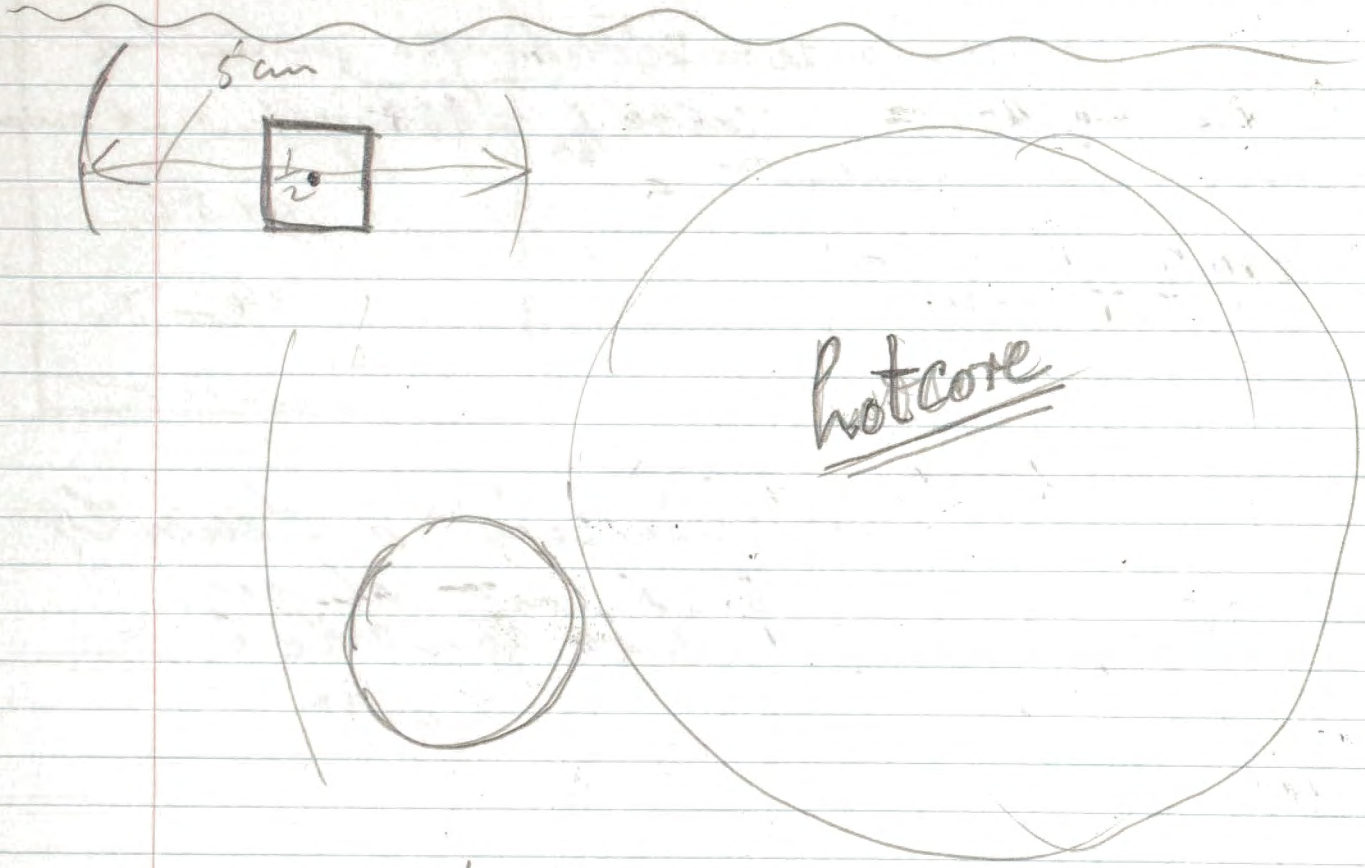
$\frac{1}{10}$ Volt loss ~~$\frac{1}{20}$~~ $\frac{1}{20}$ of Hg

current density

$\frac{1}{10} = \frac{1}{4} \frac{1}{400} \frac{1}{20} \frac{1}{y}$

$y = \frac{4 \times 400 \times 20}{10} \cong 30\,000$ Amp

or on surface $\frac{3000}{8} \cong 300$ Amps/cm²



1 cm²

25 cm $\frac{1}{10} = \frac{1}{2} \frac{1}{20} \frac{1}{4} \frac{1}{100} \frac{1}{y}$

$2 \times 20 \times 4 \times 100 = y$

~~100 100~~ $y = 1600$

or per cm² surface of anode $\frac{1600}{4 \times 25} = 16$

or per cm of Kathode ~3 Amps and 3 Watt

Tubs 2800 K has $\frac{340}{50}$ Watt = 7 Watt + 12 Watt

No

$100\sqrt{\text{Volts}}\, e^{\frac{-4.2-0.5}{kT}}$

$e^{-\frac{3.7}{kT}}$

$4 \times 10^{+6}\ 10^{-10}$

400×10^{-4} 20

Pauo

1.38×10^{-16} erg 2000 $= 2.76\ 10^{-13}$ erg

1 ev volt $= 1.6 \times 10^{-12}$ erg

3167,69 // 3168

$\frac{1.6 \times 10^{-12}\ \text{erg}}{X} = 2.76 \times 10^{-13}$

$X = \frac{2.76 \times 10^{-13}}{1.6 \times 10^{-12}}$ $\frac{16 \times 10^{-13}}{2.73\ 10^{-13}}$

$X = \frac{16}{2.73} = 5.85$

Changing N !

double ΔV

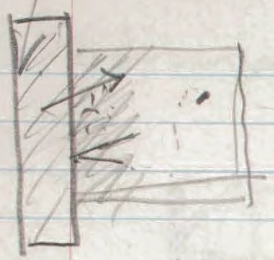
N_i becomes 4 times greater

$6\Delta V$

$\frac{N_i}{N}$ becomes 6 greater which is 20

for $\Delta V = \frac{1}{2}$

4 Volt



1.8

$\frac{N}{}$ $\frac{N_i'}{}$

4- ΔV

$$\frac{N_i'}{N_i} = A e^{-\frac{(2,87 - 2\Delta V)}{kT}}$$

$$\frac{n_i'}{n'} = e^{\frac{+(4-1,8)+\Delta V}{kT}} = B$$

$n_i + n \rightarrow$

$\leftarrow \nu N_i + \nu N$

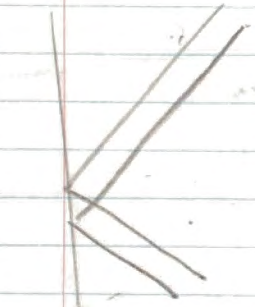
~~$N_i + N$~~ $n_i' + n' = \nu(N_i + N)$

~~$\frac{N_i}{N} = B$~~

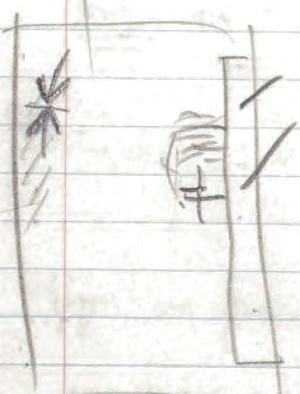
$\frac{N_i}{N}$ $\frac{n_i'}{n'} = B$

$n' = \nu N$

$n_i' = \nu N_i$



$\frac{n_i'}{n'} = B$ $\frac{N_i}{N} = \frac{B}{}$



X

Wigner says about Klein diffusion of gases through ~~thick~~ hot metal sheets
in ash Belloge : / Frye
Chidwyn : Barrett

1.) $\Delta E = \frac{1}{2}\frac{e^2}{\lambda}$; $\lambda = \sqrt{\frac{kT}{4\pi N_i e^2}}$

$\frac{N_i}{N} = e^{+W - 1.8 + 2\Delta E}$

$1.8 \cong 2\Delta E$

1.) $\lambda = \frac{1}{2}\frac{e^2}{\Delta E} = \sqrt{\frac{kT}{4\pi N_i e^2}}$

$\frac{1}{4}\frac{e^4}{(\Delta E)^2} = \frac{kT}{4\pi N_i e^2}$

$N_i = \frac{kT}{\pi e^6}(\Delta E)^2$

$N = N_i\, e^{-(W + \frac{3}{2}\Delta E) + 3.87}$

$\Delta E = \frac{1}{2}$ Volts

$N_i = \frac{1}{6}\frac{[\Delta E \text{ in Volts}]^2}{\pi}$

$1eV = 1.6 \times 10^{-12}$ erg

$N_i = \frac{\frac{1.6}{6}10^{-12} \times [\Delta E \text{ volts}]^2 \times (1.6)^2 10^{-24}}{(2)^6 \pi (5)^6 10^{-60}}$

$= \frac{(2)^6 \frac{1.6}{6} 10^{-36} (1.6)^2 (\Delta E \text{ Volts})^2}{\pi\, 10^{-54}}$

$\Delta V = 1/2$ $\quad N_i = 10^{18}\frac{4}{6}\times\frac{64}{\pi}[\Delta V]^2 = 1.36 \times 10^{18}(\Delta V)^2$

$N = N_i$

Transplen el. emiss.

25 cm $\frac{1}{10}$ Volt

1 cm² | 4 cm²

$\int_0^{x_0} x^2\,dx = \frac{1}{3}x^3 = \frac{1}{3}\left(\frac{1}{2}\right)^3 \frac{1}{4\times 20}$ Volt per Amp

$\frac{y}{100} \times \frac{1}{160}$ Volt/Amp² $= \frac{1}{10}$

$y = \frac{16000}{10} = \frac{1600}{\text{Amps}}$

100 cm² | permits 16 Amps/cm²

8 Amps/cm² on hot cathode; or if circular: πr^2 $2\pi r$ $\frac{2}{\pi} = 4$ $r = \frac{1}{2}$

$\frac{Q_1 - Q_2}{Q_1} = \frac{T_1 - T_2}{T_1}$ | $\frac{2400 - 800}{2400} = \frac{2}{3}$ 66%

1600 Amps | Volt
1600 watt
or 400 cal/sec.

10 10^3 cc Na | Total: 800 cal Sec.

Silver (take $\frac{5}{1.7}$ $\frac{60}{3}$ | 20 times Ag |
copper
Tungsten emissive

$e^{-\frac{W}{kT}}$ 2700 K || $\varepsilon_T = 0.32$
1.63 Amps/cm²

factor 4 for 100°C at K = 2000 el emission

11600 °C = 1 e Volt

K = 2000 $\frac{1}{6}$ Volt

$e^{+W_0 + \frac{1}{6}(1+0.05)} = e^{+W_0 \frac{1}{6}}$

$\frac{e^{-\frac{W}{kT}}}{e^{-\frac{W}{kT}(1.05)}} = e^{-\frac{W}{kT}2\Delta T}$ $e^{\frac{W}{kT}\frac{\Delta T}{T}}$

$1.4 = \frac{W}{kT}\frac{5}{100}$ $kT = \frac{1}{6}$

$1.4 = \frac{30}{100} W$

$\frac{140}{30} = W = 4.67$

Tungsten

~~$kT = 1.6 \times 10^{-12}$ eV~~

Radiation
$K_{const} = 5.7\ 10^{-5}$ erg/cm²

Rad. loss (black) $= 5.7 \times 10^{-12}$ Joule $\left(\frac{T_{abs}}{1000}\right)^4 10^{12}$

$= 5.7 \times \left(\frac{T_{abs}}{1000}\right)^4$ watts

$T_{abs} = 2000 = 5.7 \times 16$ watts $= 90$ watts

$T_{Abs} = 2500 = 5.7 \times 39$ $= 233$ watts

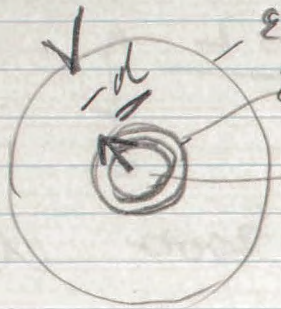
$T_{abs} = 3000 =$ $= 460$ watts

↳ for W this means 14.2 Amp/cm²

$T = 3000$ $5.7 \times 81 \simeq 450$ Watts
Tungst. Ampl.

2000 = T_{abs}
3.54 Amp/cm²
5.7 × 6 = 340 Watt

Radiation Gradient needed:

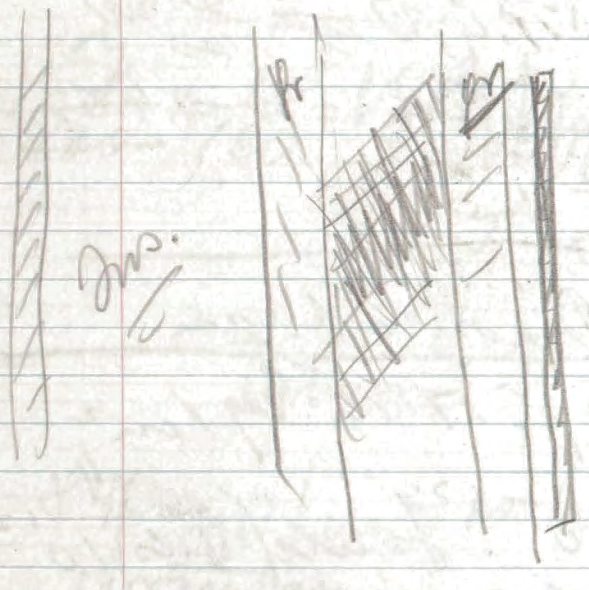


maximal Temp Diff
lower temp must not condense upper Temp must be low enough to have stall ~~Carb Dioxid~~.
Plus determines diameter of ~~Core~~ "anode".

$\frac{1}{10}$ of block and factor 3 × Coe Work pumpkin $\frac{1}{30}$

$A \Delta J T^3 = \frac{1}{30} A T^4$

$\Delta T = \frac{T}{30}$ $\quad \frac{200°}{30} = 60°C$



50 cm length
1 cm diam = $\frac{5000 \text{ Watt}}{1200 \text{ cal}}$
$3 \times 30 \times 50$ watt
10 meter H₂O
$.75 \times 10^3$
750 cc

$3\frac{1}{14}$ cm²

45cm 75 1 meter | 25 × 3 × 30 Amp + 2500 Amp

$\frac{6 \text{ cal}}{3 \text{ hrs}} = \frac{1}{4}$

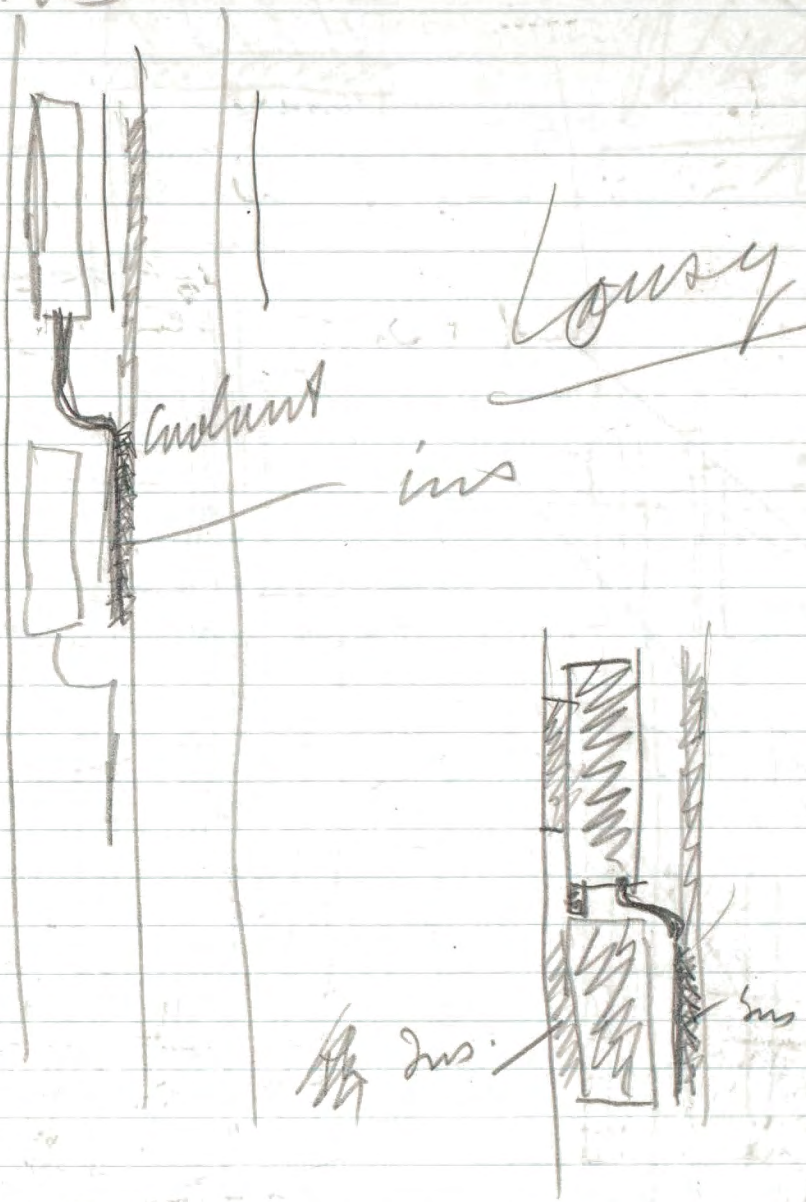
2500 + 2500 Watt

$\frac{1}{2}$ in²

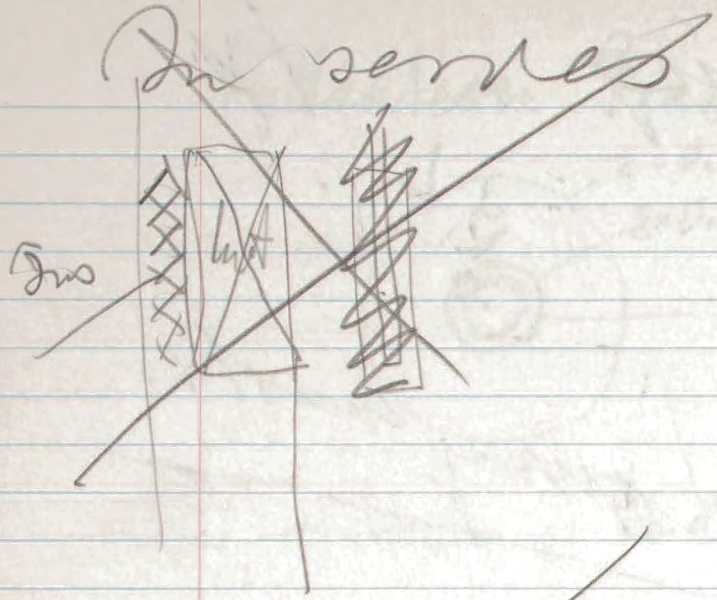
$\frac{1}{6}\Omega$ $\quad \frac{1}{6 \times 50}\Omega = \frac{1}{300}$

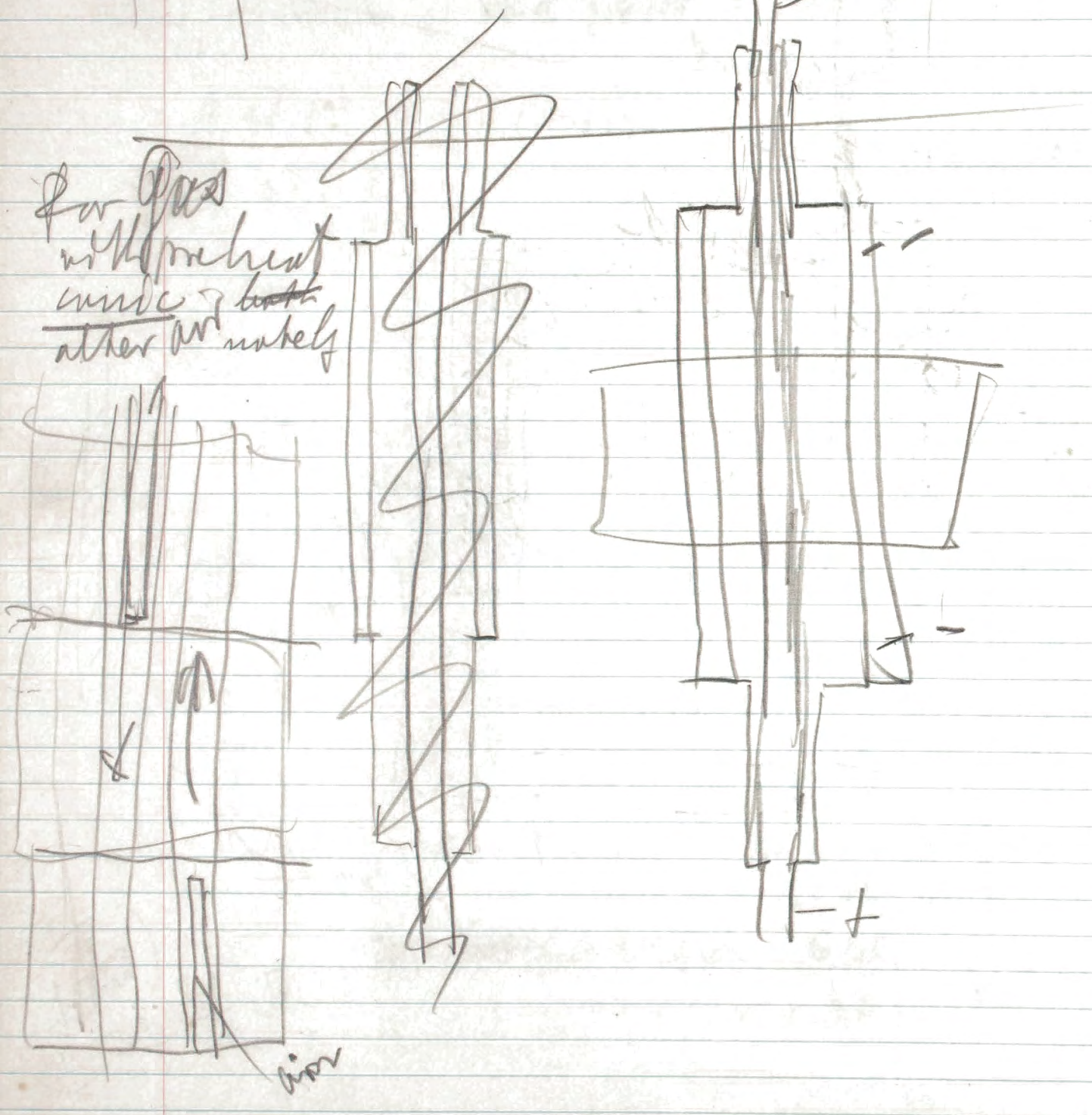
Radiation cooling

in series



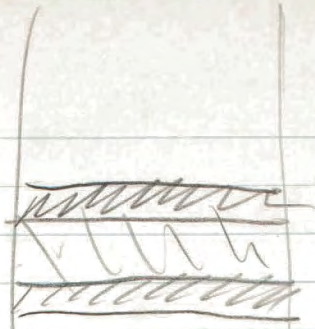
In series 2



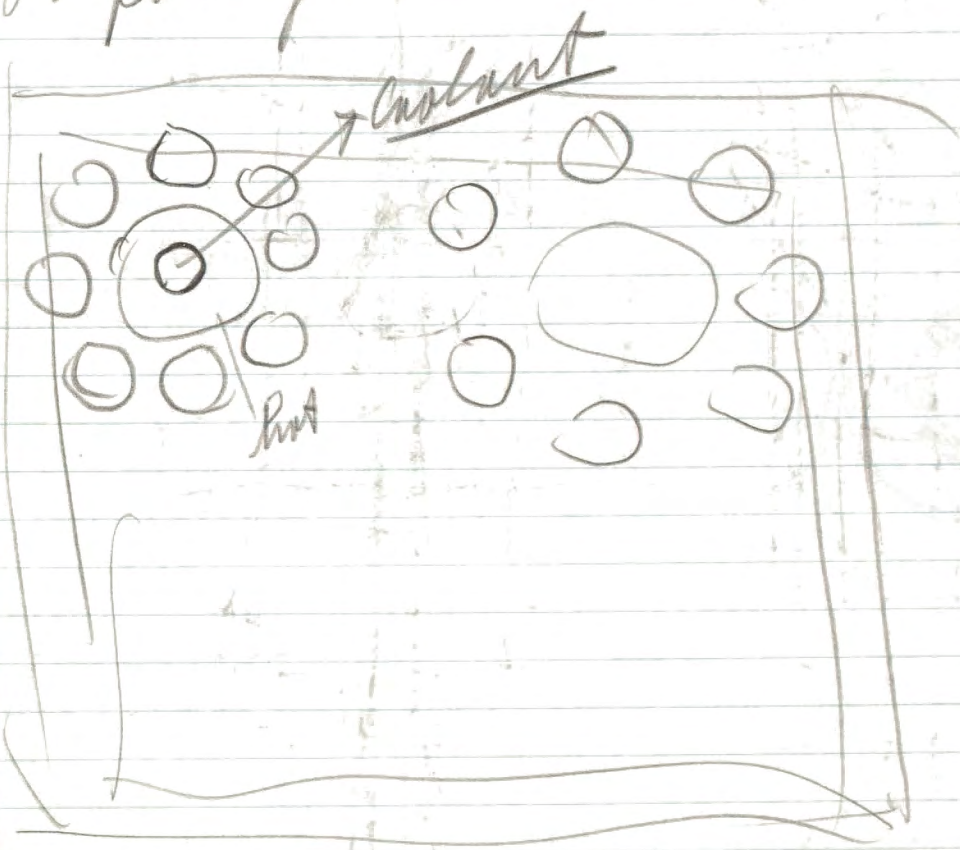


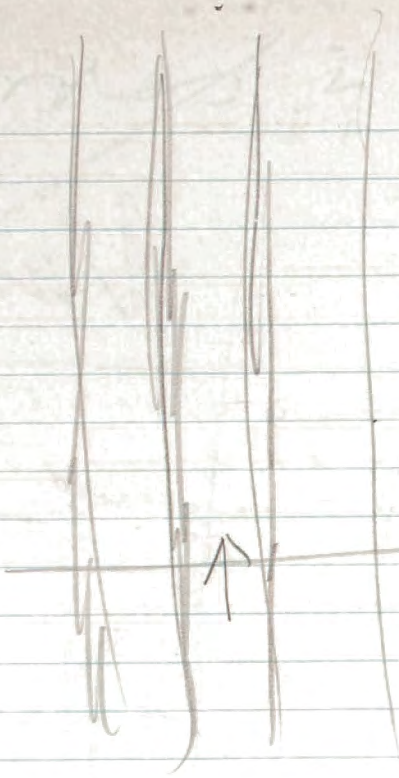
For Pass
with current
wire ~~both~~
other are wisely

Nuclear



vs fusion

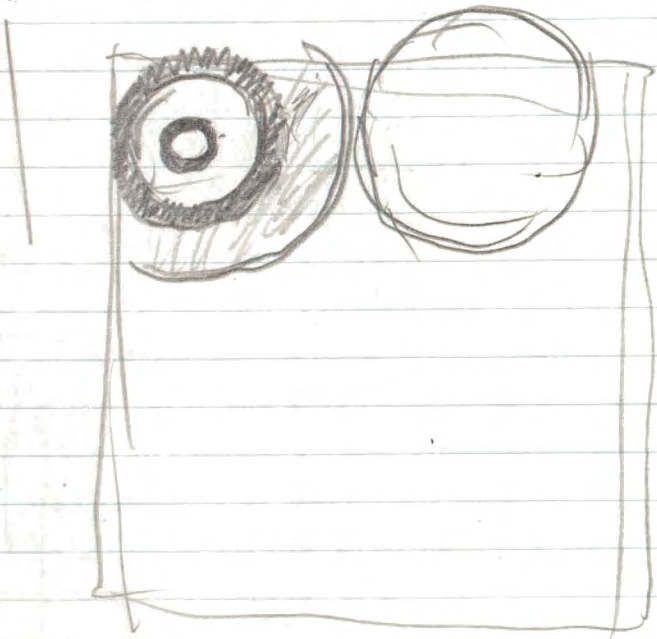




or

6 cm 50 cm 30 watt/cm²

300 cm² 300×30 = 10 kW



Maxwell

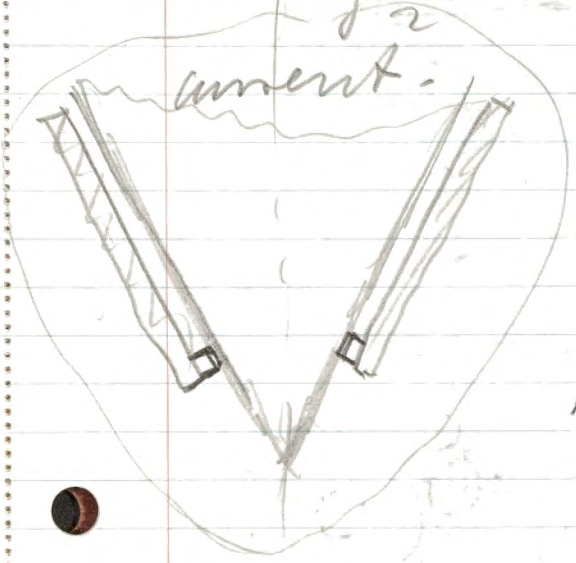
$v \geq \sqrt{\frac{1}{20}\, 10^{12}} \approx 2\, 10^{5}$ M

at 200K

$v_{el} = \sqrt{1800}\; 2 \times 10^{5}$ cm

$40 \times 2 \times 10^{5}$ cm and $\frac{1}{2}$ Volt to touch.

keeping $\frac{1}{2}$ current.



$\frac{Ni\ 4 \times 10^{6} \cdot 5\,10^{-10}}{3\,10^{9}}$ e^{-3} Amps/cm²

for 1 Amp

$N_i = \frac{4 \times 3\,10^{9}\ 10^{13}}{4 \times 10^{6}} = 3\ 10^{16}$

O.K.

Solve Dept.

Energy loss in yrs

for $\frac{1}{2}$ eV we have therefore for N_i

$$\frac{2.7 \times 3.75 \times 10^{-14}}{300} \frac{\frac{3}{5} 10^{+12}}{\sqrt{RT}} \sqrt{N_i}$$

$$= \frac{1}{5} 10^{-15} 10^{+12} \sqrt{N_i} \frac{1}{\sqrt{\frac{3}{5} 10^{12}}}$$

$$= \frac{1}{5} 10^{-3} \sqrt{N_i} \frac{1}{\sqrt{10^{11}}}$$

$$\sqrt{N_i}$$

$$5 10^{3} \sqrt{10^{11}} = \sqrt{N_i}$$

$$\sqrt{2.5\, 10^{18}} = \sqrt{N_i}$$

$3 10^{17} = N_i$ $\quad \sqrt{\frac{1}{2} RT + N} = v$

for H atom $v = \sqrt{\frac{1}{2} RT} \cong \sqrt{\frac{9}{2} \frac{1}{12}}$ eV

$$\Delta E = \frac{1}{2}\frac{e^2}{\lambda_D}$$

$$\lambda_D = \sqrt{\frac{kT}{4\pi N_i e^2}}$$

$$\lambda_D = \sqrt{\frac{RT}{4\pi N_i e^2 6\,10^{23}}}$$

$$\Delta E = \frac{1}{2}\frac{e^3\sqrt{4\pi\, 6\,10^{23}}\sqrt{N_i}}{\sqrt{RT}}$$

$$\Delta E = \frac{1}{2}\frac{5^3 10^{-30}\sqrt{2.4\pi}\,10^{12}\sqrt{N_i}}{\sqrt{RT}}$$

$\frac{1}{2}$ el volt → compute N_i

$$\frac{1}{2} = \frac{1}{2}\frac{300 \times 125 \times 10^{-18} \times 2.7 \times \sqrt{N_i}}{\sqrt{300}\,10^{-18}}$$

$$= \frac{3.75\times10^4 \times 2.7\sqrt{N_i}}{\sqrt{\frac{300}{6}}}$$

$$1 = 5\,10^{-10}\frac{1}{300}\,\text{erg} = 1\,\text{eV}$$

or ΔE in el volts =

$$\frac{3}{5}10^{12}\left[\quad\right]$$

$\frac{1}{2}$ el volt ~

$\sim 10^{-12}$ erg

$\lambda_D = \frac{1}{2}\frac{25\,10\,10^{-20}}{}$

$\lambda_D = 10^{-7}$ cm

4 Amp/cm² an Kathode

$$\frac{n^2}{n_a} = 1.7 \times 10^{20} e^{-\frac{W_i}{KT}}$$

for K = 2000

neutral Atoms

$$1.7 \times 10^{20} \not{\pi} = \frac{(2\pi K T m)^{3/2}}{h^3} e^{-\frac{W_i}{KT}}$$

UC

Pidd

Tantalum. 2 cm² T = 2025

ca 10^{-4} m/m 0.12 Amp/cm²

(H)

UC | ~~12 Amps 15%~~

Temp

15% 2000°

85% ZrC_1

2700°

Temp ZrC ~~444~~ 60/cm²

30 Watts / per cm² useful

1 Volt 30 Amps

Temp. Tantalum (Cos.)

G.N. HATSOPOULOS & J. Kaye

Proc. of IRE Sept.

p. 1574 Sept. ~~1958~~ 58

No Coesium

Volney Wilson

Memo Report No EP-4

Nov 1958

Coesium 1.5 mm

1.3 Amps

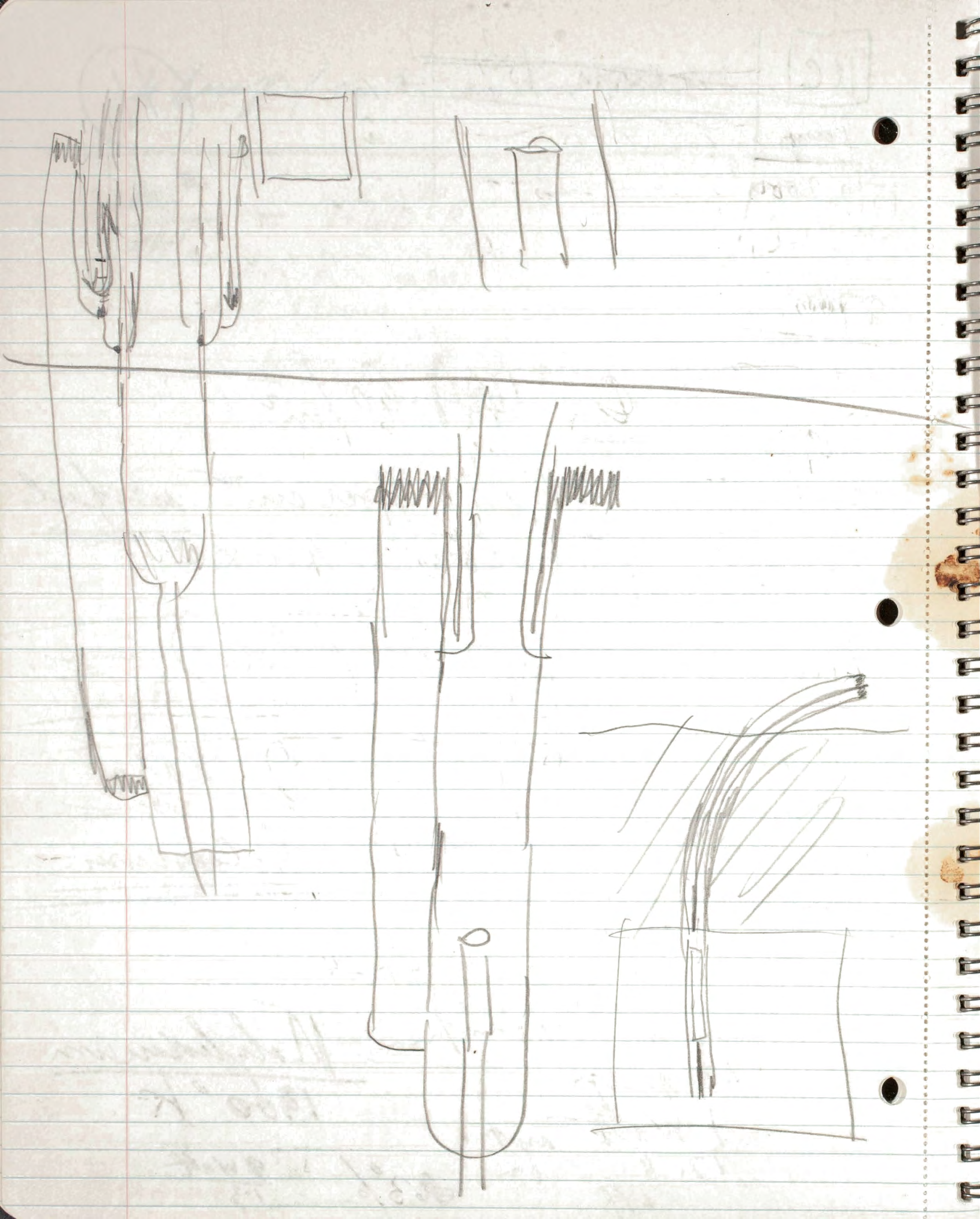
1 Watt apt

12.4 in 8.3%

Molybdenum

1900° K.

9 Watt / 1.3

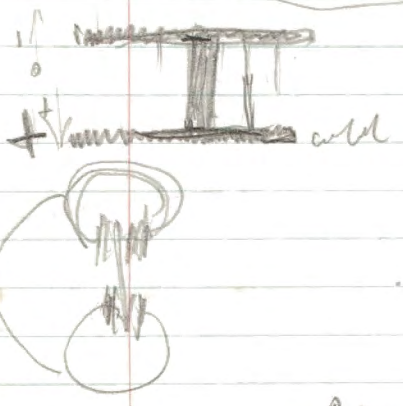


$5.7 \times 10^{-8} \times 10^{-4} T^4$ watts/cm^2

100 Amps 1 Volt. gain

loss for $T = 2000°C$ 16×10^{12}

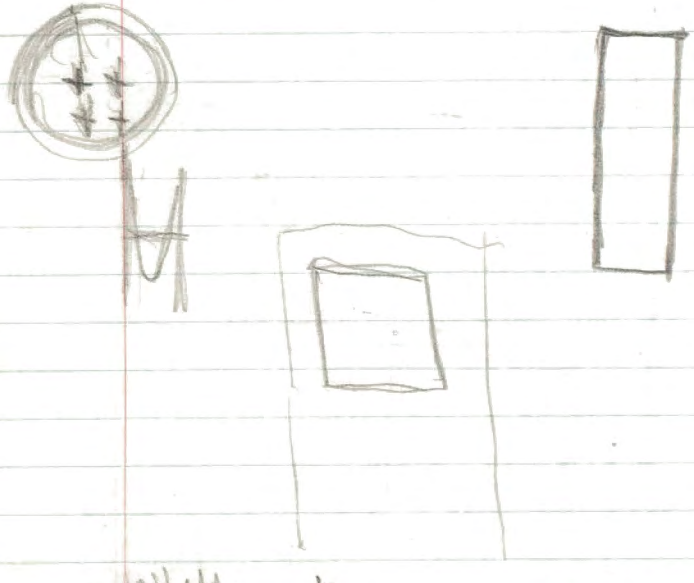
5.7×16 100 watts/cm^2



$60 \times 4 \times 10^6 = 2.4 \times 10^8$ Amps

$\Delta T =$ $\bar{e}$ 600 300

$A = 1$ $4 \times 10^6 \times \bar{e}^{-\frac{23}{16}} = 410^6 \bar{e}$



$$\int_{T_1}^{T} T^4 \, dT \cdot \frac{1}{2} - \frac{dT}{dt} = T^4$$

$$\int_{T_1}^{T} dT \frac{1}{T^4} = dt$$

$$\frac{T^{-3}}{-3} \Big|_{T_1}^{T} = t$$

$$\frac{1}{-3} T^{-4} \Big|_{T_1}^{T} = t$$

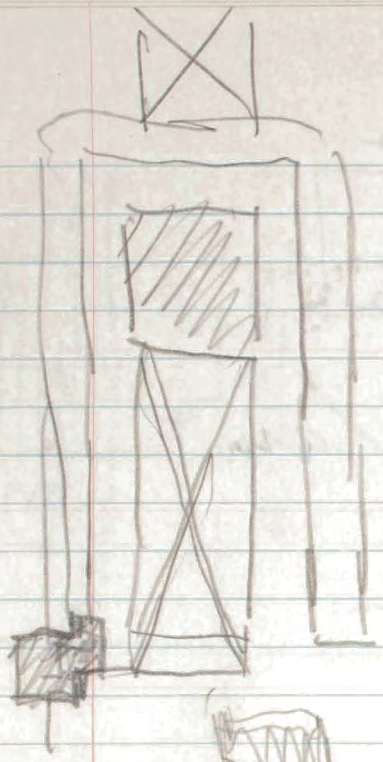
$$T^{-3} \left[\frac{1}{3} \frac{1}{T^3} \right]_{T_1}^{T} = t$$

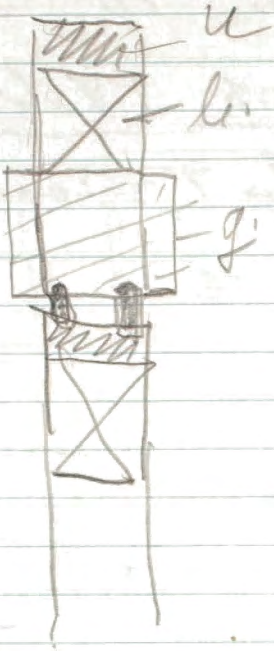
4 Volt R

(24)

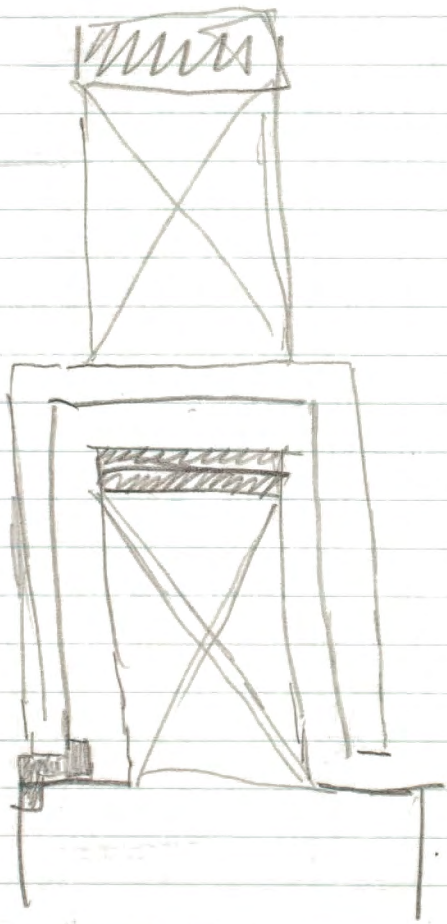
RT ln $\frac{\text{# Amps}}{\text{Amps for } \frac{3}{4}}$ $\frac{27}{764}$

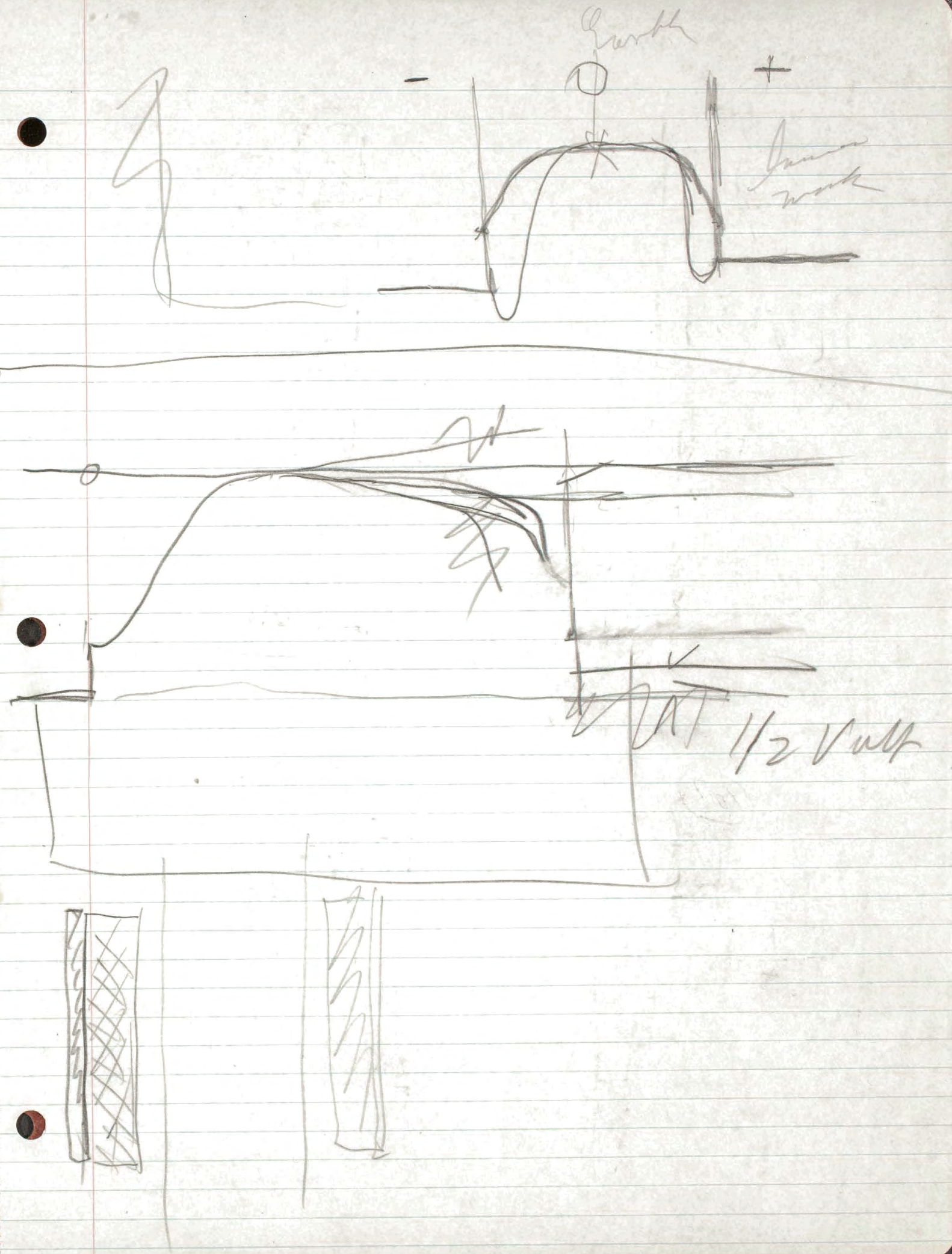
Show 9





or




Earth
−
+
Inner
Mark
1/2 Volt

1000 mil² meter

$6\,10^{23}$/liter = $6\,10^{20}$/cc

$6\,10^{+17}$ *

$6\,10^{17} \times 10^{4}$ $5\,10^{-10}$ el shot/sec cm²

$\frac{1}{300} \times 1$ Coulomb $= 10^{7}$ erg

1 Count = $3\,10^{9}$ el shot

Amps = $6\,10^{17} \times 10^{4} \times \frac{5}{3}\,10^{-19} = 10^{3}$ Amps

$RT \ln \frac{}{6\,10^{20}}$ $\frac{3.6}{e^{\frac{1}{6}}}$

$\frac{1}{36} \ln 10^{3} = 6$

$\frac{1}{6}$ $2.3 \times 7 \times \ln \frac{1}{\varphi}$

$600\,10^{18}$

$\sqrt[3]{600} \times 10^{6}$

10^{7}

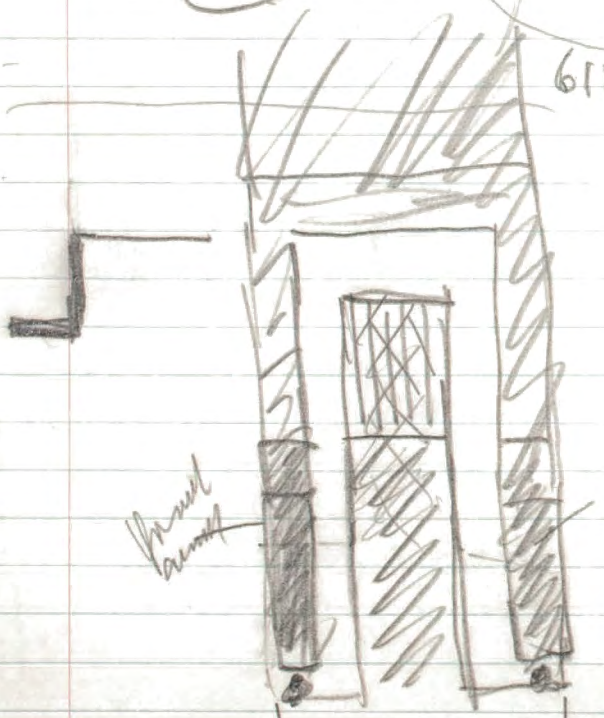
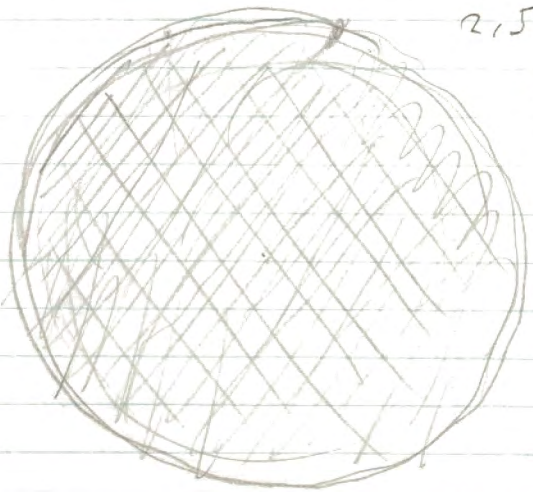
$RT \ln \frac{10^{24}}{10^{17}}$

$6\,10^{17}$ At/cc

10^{7} $25\,10^{-20}$

$\frac{}{10^{7}}$ 8^{-20}

$2.5\,10 \times 10$

2.3

$e^{-\frac{3.7}{1/6}}$