

LAKE HODGES CONDUIT AS CONSTRUCTED. Division #1.

Station	Grades	Type of Construction	42 in. Pipe	Open Conduit	Steel Flume #	Covered Conduit
0+00	254.00	Monolithic Pipe	266.0			
2+66	253.73	Open conduit		452.0		
7+13.5	253.53	Steel Flume			18.0	
7+31.5	253.52	Open conduit		42.0		
7+70.5	253.50	Steel Flume			108.0	
8+78.5	253.39	Open conduit		581.0		
14+56.5	253.13	Steel Flume			183.0	
16+39.5	252.95	Open conduit		717.0		
23+53.5	252.63	Steel flume			63.0	
24+15.5	252.57	Open Conduit		318.0		
27+31.5	252.43	Steel Flume			18.0	
27+49.5	252.41	Open conduit		232.0		
29+78.5	252.31	Steel Flume			18.0	
29+96.5	252.30	Open conduit		95.0		
30+88.5	252.25	Steel Flume			33.0	
31+21.5	252.22	Open conduit		426.9		
35+45.4	252.02	Steel Flume			18.0	
35+63.4	252.01	Open conduit		302.1		
38+62.5	251.86	Steel Flume			33.0	
38+95.5	251.83	Open conduit		72.0		
39+64.5	251.80	Steel flume			78.0	
40+42.5	251.72	Open conduit		126.7		
41+66.2	251.67	Steel Flume			33.0	
41+99.2	251.64	Open conduit		67.8		
42+64.0	251.61	Steel Flume			33.0	
42+97.0	251.60	Open conduit		99.5		
43+95	251.54	Syphon Intake Box		10.0		

Station	Grades	Type of Construction	42 in. Pipe	Open Conduit	Steel Flume #	Covered Conduit
44+05	247.54	42" Pipe	261.5			
46+50	247.27	Siphon Outlet Box		10.0		
46+60	251.27	Open conduit		230.		
48+90	251.16	Siphon Intake Box		10.		
49+00	247.16	42" Pipe	300.7			
51+95	246.85	Siphon Outlet Box		10.		
52+05	250.85	Open conduit		103.9		
53+08.9	250.80	Covered Conduit				209.1
55+18	250.71	Open conduit		06.58		
55+22.98	250.71	Steel Flume			36	
55+58.98	250.67	Open conduit		02.53		
55+60.01	250.67	Covered conduit				151.5
57+11.51	250.59	Open conduit		02.4		
57+12.45	250.59	Steel Flume			18	
57+30.41	250.58	Open conduit		02.91		
57+31.1	250.58	Covered conduit				23.9
57+55	250.57	Open conduit		03.94		
57+57+44	250.58	Steel Flume			18	
57+75.44	250.55	Open conduit		02.2		
57+76.14	250.55	Covered Section				258.4
60+34.54	250.43	Open conduit		03.18		
60+36.22	250.43	Steel flume			63	
60+99.22	250.37	Open conduit		02.3		
61+01.02	250.37	Covered conduit				185.7
62+86.72	259.26	Open conduit		05.42		
62+90.64	250.26	Steel Flume			72	
63+62.64	250.20	Open conduit		02.62		

Sheet #3

Station	Grades	Type of Construction	42 in. Pipe	Open conduit	Steel Flume #	Covered Conduit
63+63.76	250.20	Covered conduit				664.95
70+28.71	249.82	Open conduit		22.90		
71+51.61 =71+38 71+48	249.84 245.84	Siphon Intake Box		10		
73+63 =73+50 73+60	245.62 249.62	42' Pipe Siphon Outlet Box	215	10		
Total			1043.2	4082.88	843	1493.55

Steel Flume extends 1.5 ft. at each end beyond the center of 1st and last Trestle bent.

LAKE HODGES CONDUIT AS CONSTRUCTED. Division #2 & #3

Station	Grades	Type of Construction	42 in. Pipe	Open conduit	Steel Flume #	Covered Conduit
73+60	249.62	Open conduit		342.6		
77+02.6	249.47	Steel flume			42.0	
77+44.6	249.43	Open conduit		645.6		
83+90.2	249.14	Covered conduit				8.0
83+98.2	249.13	Open conduit		174.9		
85+73.1	249.05	Steel Flume			36.0	
86+09.1	249.01	Open conduit		324.4		
89+33.5	248.86	Steel Flume			33.0	
89+66.5	248.83	Open conduit		193.2		
91+59.7	248.74	Covered conduit				10.0
91+69.7	248.73	Open conduit		901.0		
100+70.7	248.33	Siphon intake box		9.0		
100+79.7	244.33	42" Pipe	152.7			
102+29.0	244.16	Siphon Outlet Box		8.0		
102+37.0	248.16	Open conduit		736.7		

Sheet #4

Station	Grades	Type of Construction	42" Pipe	Open conduit	Steel Flume #	Covered Conduit
109+73.7	247.83	Steel Flume				18.0
109+91.7	247.81	Open conduit		449.8		
114+41.5	247.61	Steel flume				33.0
114+74.5	247.58	Open conduit		205.3		
116+79.8	247.49	Steel flume				54.0
117+33.8	247.43	Open conduit		1401.8		
131+35.6	246.80	Covered conduit				10.0
131+45.6	246.81	Open conduit		822.8		
139+68.4	246.41	Covered conduit				10.0
139+78.4	246.40	Open conduit		671.6		
146+50	246.08	Covered conduit				10.0
146+60	246.07	Open conduit		1566.6		
162+26.6	245.53	Covered conduit				10.0
162+36.6	245.52	Open conduit		1621.6		
178+58.2	245.01	Covered conduit				15.0
178+73.8	244.99	Open conduit		244.2		
183+17.4	244.85	Covered conduit				8.0
183+25.4	244.85	Open conduit		881.3		
192+06.7	244.60	Open conduit		4.0		
192+10.7	243.60	42" Pipe	191.3			
194+02.0	244.44	Open conduit		1678.0		
210+80.0	243.94	Siphon Intake Box		8.0		
210+88.0	239.94	42" Pipe	1105.0			
221+86.0	242.88	Manhole		4.0		
(221+90.0 (221+78.0	242.88	42" Pipe	686.0			
228+60.0	241.33	42" gate & Air Vent	1.4			
228+61.4	"	Open conduit		8.6		

Station	Grades	Type of Construction	42" Pipe	Open Conduit	Steel Flume #	Covered Conduit
228+70	242.27	Open Conduit		1080.0		
239+50	241.94					
245+50	241.52	Unlined conduit				
Total			2122.0 2135.	14183.0	216.0	81.0

Location of Special Structures

43+89.04 44+17 45+24.40	to	43+93.04 45+32	Sand traps Siphon Trestle #11 Siphon Blow off.
48+84.30 49+52 49+75.42	to	48+88.30 51+32	Sand trap Siphon Trestle #12 Siphon Blowoff
71+46.91 72+13.53 72+79.53	to	71+50.91 72+82.53	Sand trap Siphon Trestle #21 Siphon Blowoff
100+65 101+36 101+49.3 215+92.7 225+53.6	to	100+69 101+90	Sand traps Siphon Trestle #27 Siphon Blowoff Siphon Blowoff Siphon Blowoff

210+75 to 210+79

Location and number of units in flume trestles

Trestle No.	Length	Station	No. of units in bent
1	15	7+15 7+30	1 1
2	105	7+72 7+87 8+02 8+17 8+32 8+47 8+62 8+77	1 2 2 2 3 4 3 1
3	180	14+58 14+73 14+88 15+03 15+18 15+33 15+48 15+63 15+78 15+93 16+08 16+23 16+38	1 1 1 1 2 4 5 8 8 6 4 2 1
4	60	23+55 23+70 23+85 24+00 24+15	1 2 4 2 1
4A	15	27+33 27+48	1 1
5	15	29+80 29+95	1 1
6	30	30+90 31+05 31+20	1 2 1
7	15	35+46.9 35+61.9	1 1
8	30	38+64 38+79 38+94	1 2 1
9	75	39+66 39+81 39+96 40+11 40+26 40+41	1 1 4 4 1 1

Trestle No.	Length	Station	No. of Units in bent
10	30	41+67.7	1
		41+82.7	1
		41+97.7	1
10A	30	42+65.5	1
		42+80.5	1
		42+95.5	1
12	180	49+52	0
		49+67	1
		49+82	1
		49+97	1
		50+12	2
		50+27	1
		50+42	1
		50+57	1
		50+72	1
		50+87	1
		51+02	1
		51+17	2
		51+32	0
13	33	55+24.48	1
		55+33.48	1
		55+48.48	2
		55+57.48	1
14	15	57+13.91	1
		57+28.91	1
15	15	57+58.94	1
		57+73.94	1
16	60	60+37.72	1
		60+52.72	1
		60+67.72	3
		60+82.72	2
		60+97.72	1
18	69	62+90.64	1
		63+05.64	2
		63+20.64	6
		63+29.64	5
		63+44.64	4
		63+59.64	1
21	69	72+13.53	0
		72+22.53	0
		72+37.53	2
		72+52.53	5
		72+67.53	5
		72+82.53	0
24	33	85+74.6	1
	33	85+83.6	3
		85+98.6	2
		86+07.6	1

Trestle No.	Length	Station	No. of Units in bent
25	30	89+35	1
		89+50	3
		89+65	1
28	15	109+75.2	1
		109+90.2	1
29	30	114+45	1
		114+58	3
		114+73	1
30	51	116+81.3	1
		116+90.3	2
		117+02.3	4
		117+17.3	3
		117+32.3	1
22	39	77+04.1	1
		77+19.1	3
		77+34.1	1
		77+43.1	1

Total length of Trestles -	Flume	990
	Pipe Siphons	318
		<u>1308</u>

DESCRIPTION OF CARROLL CONDUIT

Beginning at a point whence Section corner common to Sections 18 and 19, Township 13 South, Range 2 West, and Sections 13 and 24, Township 13 South, Range 3 West, San Bernardino Meridian, bears South 28° 57' West, 3831.94 feet;

Thence South 70° 14' West 258.27 feet;
 Thence South 50° 43' West 93.01 feet;
 Thence on a 200 ft. Radius Curve to the right 31.65 feet;
 Thence South 59° 47' West 151.24 feet;
 Thence on a 200 ft. Radius Curve to the right 35.84 feet;
 Thence South 70° 03' West 137.13 feet;
 Thence South 58° 54' West 61.00 feet;
 Thence South 27° 54' West 197.04 feet;
 Thence on a 100 ft. Radius Curve to the right 43.23 feet;
 Thence South 52° 40' West 62.53 feet;
 Thence on an 80 ft. Radius Curve to the left 47.01 feet;
 Thence South 19° 00' West 142.19 feet;
 Thence on a 100 ft. Radius Curve to the right 22.69 feet;
 Thence South 32° 00' West 134.38 feet;
 Thence on a 200 ft. Radius Curve to the right 34.56 feet;
 Thence South 41° 54' West 275.60 feet;
 Thence on a 200 ft. Radius Curve to the left 28.27 feet;
 Thence South 33° 48' West 271.68 feet;
 Thence on a 200 ft. Radius Curve to the right 105.88 feet;
 Thence South 64° 08' West 146.94 feet;
 Thence on a 100 ft. Radius Curve to the right 60.85 feet;
 Thence North 81° 00' West 15.55 feet;

Thence South 56° 40' West 119.68 feet;
 Thence on a 100 ft. Radius Curve to the right 71.44 feet;
 Thence North 82° 24' West 17.65 feet to a point on the east line of Section 13, Township 13 South, Range 3 West, San Bernardino Meridian, whence the corner common to Sections 18 and 19, Township 13 South, Range 2 West, and Sections 13 and 24, Township 13 South, Range 3 West, San Bernardino Meridian, bears South 1768.16 feet;

Thence continuing North 82° 24' West 81.28 feet;
 Thence on a 100 ft. Radius Curve to the right 39.39 feet;
 Thence North 59° 50' West 45.56 feet;
 Thence South 82° 44' West 75.82 feet;
 Thence on a 50 ft. Radius Curve to the right 71.00 feet;
 Thence North 15° 54' West 95.68 feet;
 Thence North 60° 38' West 38.62 feet;
 Thence on a 50 ft. Radius Curve to the left 36.65 feet;
 Thence South 77° 22' West 34.23 feet;
 Thence South 31° 02' West 87.55 feet;
 Thence on a 50 ft. Radius Curve to the right 38.85 feet;
 Thence South 75° 32' West 10.74 feet;
 Thence on a 70 ft. Radius Curve to the right 46.71 feet;
 Thence North 66° 14' West 18.95 feet;
 Thence on a 50 ft. Radius Curve to the left 44.27 feet;
 Thence South 63° 02' West 17.21 feet;
 Thence on a 50 ft. Radius Curve to the right 52.16 feet;
 Thence North 57° 12' West 140.57 feet;
 Thence South 70° 18' West 36.01 feet;
 Thence on a 100 ft. Radius Curve to the left 37.52 feet;
 Thence South 48° 48' West 77.09 feet;

Thence on a 40 ft. Radius Curve to the right 65.83 feet;
 Thence North 36° 54' West 54.30 feet;
 Thence on an 80 ft. Radius Curve to the left 60.55 feet;
 Thence North 80° 16' West 110.64 feet;
 Thence South 35° 12' West 80.24 feet;
 Thence on a 40 ft. Radius Curve to the right 59.46 feet;
 Thence North 59° 38' West 19.06 feet;
 Thence on a 120 ft. Radius Curve to the left 43.98 feet;
 Thence North 80° 38' West 94.78 feet;
 Thence on a 30 ft. Radius Curve to the left 31.15 feet;
 Thence South 39° 52' West 33.05 feet;
 Thence on a 50 ft. Radius Curve to the right 48.00 feet;
 Thence North 85° 08' West 305.27 feet;
 Thence on a 70 ft. Radius Curve to the right 37.87 feet;
 Thence North 54° 08' West 3.05 feet;
 Thence on a 60 ft. Radius Curve to the left 65.10 feet;
 Thence South 63° 42' West 8.30 feet;
 Thence on a 60 ft. Radius Curve to the right 69.11 feet;
 Thence North 50° 18' West 76.56 feet;
 Thence on a 400 ft. Radius Curve to the left 167.55 feet;
 Thence North 74° 18' West 161.47 feet;
 Thence North 68° 18' West 41.32 feet;
 Thence on a 100 ft. Radius Curve to the left 36.65 feet;
 Thence North 89° 18' West 9.98 feet;
 Thence on a 150 ft. Radius Curve to the right 56.29 feet;
 Thence North 67° 48' West 9.34 feet;
 Thence on a 70 ft. Radius Curve to the right 52.94 feet;
 Thence North 24° 28' west 0.03 feet;

Thence on a 60 ft. Radius Curve to the left 87.44 feet;
 Thence South 72° 02' West 33.65 feet;
 Thence on a 50 ft. Radius Curve to the right 47.41 feet;
 Thence North 53° 38' West 63.80 feet;
 Thence North 76° 18' West 141.12 feet;
 Thence on a 100 ft. Radius Curve to the left 28.51 feet;
 Thence South 87° 22' West 13.26 feet;
 Thence on a 100 ft. Radius Curve to the right 38.75 feet;
 Thence North 70° 26' West 111.06 feet;
 Thence North 76° 18' West 244.0 feet;
 Thence South 77° 42' West 105.76 feet;
 Thence on a 100 ft. Radius Curve to the right 31.42 feet;
 Thence North 84° 18' West 56.92 feet;
 Thence on a 200 ft. Radius Curve to the right 27.93 feet;
 Thence North 76° 18' West 91.86 feet;
 Thence South 61° 42' West 116.81 feet;
 Thence on a 60 ft. Radius Curve to the right 37.35 feet;
 Thence North 82° 38' West 41.10 feet;
 Thence North 77° 38' West 52.12 feet;
 Thence on a 200 ft. Radius Curve to the right 29.67 feet;
 Thence North 69° 08' West 79.83 feet;
 Thence on a 200 ft. Radius Curve to the right 40.14 feet;
 Thence North 57° 38' West 89.67 feet;
 Thence on a 100 ft. Radius Curve to the right 36.65 feet;
 Thence North 36° 38' West 4.73 feet;
 Thence on a 60 ft. Radius Curve to the left 48.35 feet;
 Thence North 82° 48' West 164.96 feet;
 Thence on a 100 ft. Radius Curve to the left 42.75 feet;

Thence South $72^{\circ} 42'$ West 81.49 feet;
 Thence on a 60 ft. Radius Curve to the right 57.60 feet;
 Thence North $52^{\circ} 18'$ West 72.33 feet;
 Thence on a 100 ft. Radius Curve to the right 60.21 feet;
 Thence North $17^{\circ} 48'$ West 47.88 feet;
 Thence North $85^{\circ} 49'$ West 45.00 feet;
 Thence on a 100 ft. Radius Curve to the left 21.82 feet;
 Thence South $81^{\circ} 41'$ West 95.05 feet;
 Thence on a 400 ft. Radius Curve to the right 44.22 feet;
 Thence South $88^{\circ} 01'$ West 65.93 feet;
 Thence on a 70 ft. Radius Curve to the right 73.30 feet;
 Thence North $31^{\circ} 59'$ West 2.13 feet;

Thence on a 100 ft. Radius Curve to the left 5.06 feet
 to a point whence a point 2640 feet north of the corner common to
 Sections 13, 14, 23 and 24, Township 13 South, Range 3 West, San
 Bernardino Meridian, bears West 363.46 feet;

Again beginning at a point whence a point 2640 feet
 north of the corner common to Sections 13, 14, 23 and 24, Township
 13 South, Range 3 West, San Bernardino Meridian, bears East
 695.19 feet;

Thence on an 80 ft. Radius Curve to the right 81.33 feet;
 from a tangent which bears South $53^{\circ} 12'$ West;

Thence North $68^{\circ} 33'$ West 46.78 feet to a point whence
 a point 2640 feet north of the corner common to Sections 13, 14,
 23 and 24, Township 13 South, Range 3 West, San Bernardino Meridian,
 bears East 809.73 feet;

Again beginning at a point whence a point 2640 feet north

of the corner common to Sections 13, 14, 23 and 24, Township 13
 South, Range 3 West, San Bernardino Meridian, bears East 961.19 feet;

Thence South $69^{\circ} 47'$ West 37.90 feet;

Thence on a 100 ft. Radius Curve to the right 45.38 feet;

Thence North $84^{\circ} 13'$ West 50.81 feet;

Thence on a 100 ft. Radius Curve to the right 28.80 feet;

Thence North $67^{\circ} 43'$ West 17.60 feet to a point whence

a point 2640 feet north of the corner common to Sections 13, 14,
 23 and 24, Township 13 South, Range 3 West, San Bernardino Meridian
 bears East 1136.07 feet;

Again beginning at a point whence a point 2640 feet
 north of the corner common to Sections 13, 14, 23 and 24, Township
 13 South, Range 3 West, San Bernardino Meridian, bears East 1566.08
 feet;

Thence South $6^{\circ} 45'$ West 10.77 feet;

Thence on a 50 ft. Radius Curve to the right 52.38 feet;

Thence South $66^{\circ} 45'$ West 47.04 feet;

Thence on a 200 ft. Radius Curve to the right 24.43 feet;

Thence South $73^{\circ} 45'$ West 40.58 feet;

Thence on a 100 ft. Radius Curve to the right 27.63 feet;

Thence South $89^{\circ} 35'$ West 147.65 feet;

Thence on a 100 ft. Radius Curve to the right 47.12 feet;

Thence North $63^{\circ} 25'$ West 42.19 feet;

Thence on a 100 ft. Radius Curve to the left 45.09 feet;

Thence North $89^{\circ} 15'$ West 201.65 feet;

Thence on a 50 ft. Radius Curve to the left 67.63 feet;

Thence South $13^{\circ} 15'$ West 94.40 feet;

Thence on a 100 ft. Radius Curve to the right 84.94 feet;

Thence South 61° 55' West 30.34 feet;
 Thence on a 60 ft. Radius Curve to the right 53.41 feet;
 Thence North 67° 05' West 160.04 feet;
 Thence South 19° 54' West 42.30 feet;
 Thence South 22° 37' East 42.23 feet;
 Thence on a 40 ft. Radius Curve to the right 49.57 feet;
 Thence South 48° 23' West 107.52 feet;
 Thence South 0° 52' West 61.10 feet;
 Thence South 77° 09' East 123.60 feet;
 Thence on a 150 ft. Radius Curve to the right 154.46 feet;
 Thence South 18° 09' East 258.49 feet;
 Thence on a 100 ft. Radius Curve to the right 59.34 feet;
 Thence South 15° 51' West 206.23 feet;
 Thence on a 100 ft. Radius Curve to the right 29.96 feet;
 Thence South 33° 01' West 212.18 feet;
 Thence on a 400 ft. Radius Curve to the right 41.89 feet;
 Thence South 39° 01' West 180.35 feet;
 Thence on a 100 ft. Radius Curve to the right 34.91 feet;
 Thence South 59° 01' West 8.67 feet to a point on the
 North and South center line of Section 14, Township 13 South, Range
 3 West, San Bernardino Meridian, whence the one-quarter corner
 common to Sections 14 and 23, Township 13 South, Range 3 West, bears
 South 0° 30' West 1119.9 feet;

Thence continuing South 59° 01' West 38.02 feet;
 Thence on a 70 ft. Radius Curve to the left 40.56 feet;
 Thence South 25° 49' West 174.60 feet;
 Thence on a 100 ft. Radius Curve to the right 54.92 feet;

Thence South 57° 17' West 155.17 feet;
 Thence on a 250 ft. Radius Curve to the right 245.80 feet;
 Thence North 66° 23' West 167.50 feet;
 Thence on a 25 ft. Radius Curve to the left 45.83 feet;
 Thence South 8° 35' West 249.29 feet;
 Thence on a 70 ft. Radius Curve to the right 70.41 feet;
 Thence South 66° 13' West 95.62 feet;
 Thence on a 100 ft. Radius Curve to the right 41.02 feet;
 Thence South 89° 43' West 66.25 feet;
 Thence on a 70 ft. Radius Curve to the right 46.43 feet;
 Thence North 52° 17' West 62.46 feet;
 Thence on a 20 ft. Radius Curve to the left 55.73 feet;
 Thence South 31° 57' East 54.73 feet;
 Thence on a 300 ft. Radius Curve to the left 46.25 feet;
 Thence South 40° 47' East 81.45 feet;
 Thence on a 100 ft. Radius Curve to the right 87.38 feet;
 Thence South 9° 17' West 30.67 feet;
 Thence on a 100 ft. Radius Curve to the right 56.78 feet;
 Thence South 41° 49' West 249.06 feet to a point on the
 south line of Section 14, Township 13 South, Range 3 West, San
 Bernardino Meridian, whence the corner common to Sections 14, 15,
 Twp 13 South, R 3 West, San Bernardino Meridian
 22 and 23 bears North 89° 42' West 1511.1 feet;

Thence South 44° 33' West 290.26 feet;
 Thence on a 100 ft. Radius Curve to the right 97.74 feet;
 Thence North 79° 27' West 294.69 feet;
 Thence on a 200 ft. Radius Curve to the left 47.12 feet;
 Thence South 87° 03' West 89.48 feet;
 Thence on a 100 ft. Radius Curve to the right 53.52 feet;

Thence North 62° 17' West 43.48 feet;
 Thence on a 20 ft. Radius Curve to the left 45.86 feet;
 Thence South 13° 39' East 32.55 feet;
 Thence on a 200 ft. Radius curve to the right 226.31 feet;
 Thence South 51° 11' West 49.69 feet;
 Thence on a 200 ft. Radius curve to the right 54.69 feet;

Thence South 66° 51' West 575.01 feet to a point on
 the west line of Section 23, Township 13 South, Range 3 West,
 San Bernardino Meridian, whence the corner common to Sections
 14, 15, 22 and 23, ^{Twp 13 South, Range 3 West, San Bernardino Meridian} bears North 0° 12' East 702.5 feet;

Thence continuing South 66° 51' West 72.95 feet;
 Thence on a 100 ft. Radius Curve to the right 30.54 feet;
 Thence South 84° 21' West 344.54 feet;
 Thence on a 120 ft. Radius Curve to the right 124.27 feet;
 Thence North 36° 19' West 83.92 feet;
 Thence on a 25 ft. Radius Curve to the left 42.99 feet;
 Thence South 45° 09' West 136.54 feet;
 Thence on a 100 ft. Radius Curve to the right 118.68 feet;
 Thence North 66° 51' West 142.52 feet;
 Thence on a 50 ft. Radius Curve to the left 59.05 feet;
 Thence South 45° 29' West 31.07 feet;
 Thence on a 200 ft. Radius Curve to the right 210.60 feet;
 Thence North 74° 11' West 258.09 feet;
 Thence on a 300 ft. Radius Curve to the right 48.87 feet;
 Thence North 64° 51' West 275.71 feet;
 Thence on a 100 ft. Radius Curve to the left 67.19 feet;
 Thence South 76° 39' West 133.72 feet;

Thence on a 100 ft. Radius Curve to the right 66.32 feet;
 Thence North 65° 21' West 244.56 feet;
 Thence on a 200 ft. Radius Curve to the left 40.72 feet;
 Thence North 77° 01' West 203.61 feet;
 Thence on a 200 ft. Radius Curve to the left 38.40 feet;
 Thence North 88° 01' West 227.93 feet;

Thence on a 200 ft. Radius curve to the right 22.22 feet;
 to a point on the easterly line of the Rancho San Dieguito, whence
 Corner No. 8, being the northeast corner of the said Rancho San
 Dieguito marked S D No 2, bears North 4° 50' West 3081.1 feet;

Thence continuing on said 200 ft. Radius Curve to the
 right 80.75 feet;

Thence North 58° 31' West 50.56 feet;
 Thence on a 400 ft. Radius Curve to the left 162.20 feet;
 Thence North 81° 45' West 385.91 feet;
 Thence on a 100 ft. Radius Curve to the left 47.01 feet;
 Thence South 71° 19' West 149.67 feet;
 Thence North 85° 41' West 1142.07 feet;
 Thence on a 100 ft. Radius Curve to the right 34.85 feet;
 Thence North 65° 43' West 580.10 feet;
 Thence on a 100 ft. Radius Curve to the right 51.14 feet;
 Thence North 36° 25' West 203.96 feet;
 Thence on a 500 ft. Radius Curve to the left 190.53 feet;
 Thence North 58° 15' West 224.69 feet;
 Thence on a 200 ft. Radius Curve to the right 47.71 feet;
 Thence North 44° 35' West 322.49 feet;

Thence on a 300 ft. Radius Curve to the left 116.94 feet;
 Thence North 66° 55' West 446.15 feet, whence a point on
 the San Dieguito Dam, which is the beginning of Distribution Line,
 bears North 88° 40' West 1864.25 feet, said point on San Dieguito
 Dam lying South 7° 03' West 1694.3 feet from Corner No. 7 Patent
 Survey, Rancho San Dieguito, a stone in mound of rock marked
 S. D. No. 3.

Description

1917 54-A

Beginning at a point whence the Sec. corner common
 to Sections 18 and 19, S. 13 S. R. 2 W. and
 Secs 13 + 24, S. 13 S. R. 3 W. 5 B.M. ^{bears South 28° 54' W. 3831.94 ft.} Thence S 70° 14' W. 258.27 ft. Thence
 S 50° 43' W. 93.01 ft. Thence to the right along a 200 ft. radius curve
 31.65 ft. Thence S 59° 47' W. 151.24 ft.
 Thence to the right along a 200 ft. radius curve
 35.84 ft. Thence S 70° 03' W. 137.13 ft. Thence S 58° 54' W. 61.0 ft.
 Thence S 27° 54' W. 197.04 ft. Thence to the right along a 100 ft
 radius curve, 43.23 ft. Thence S 52° 40' W
 62.53 ft. Thence to the left along an 80 ft. radius
 curve 47.01 ft. Thence S 19° 00' W. 142.19 ft. Thence
 to the right along a 100 ft. radius curve
 32.69 ft. Thence S 32° 00' W. 134.38 ft. Thence to the right
 along a 200 ft. radius curve 34.56 ft. Thence S 41° 54' W
 275.60 ft. Thence to the left along a 200 ft. radius
 curve 28.27 ft. Thence S 33° 48' W. 271.68 ft. Thence
 to the right along a 200 ft. radius curve 105.87 ft.
 Thence S 64° 08' W. 146.94 ft. Thence to the right along
 a 100 ft. radius curve 60.55 ft. Thence N 51° 00' W. 15.55 ft.
 Thence S 56° 40' W. 119.68 ft. Thence to the right along a 100 ft.
 radius curve 71.44 ft. Thence N 82° 24' W. 98.93 ft. Thence
 to the right along a 100 ft. radius curve
 39.39 ft. Thence N 59° 50' W. 45.56 ft. Thence S 82° 44' W. 75.82 ft.
 Thence to the right along a 50 ft. radius curve.
 71.00 ft. Thence N 15° 54' W. 95.68 ft. Thence N 60° 38' W
 38.62 ft. Thence to the left along a 50 ft. radius
 curve 36.65 ft. Thence S. 77° 22' W. 34.23 ft. Thence
 S. 31° 02' W. 87.55 ft. Thence to the right along a 50 ft.
 radius curve 38.84 ft. Thence S 75° 32' W. 10.74 ft.
 Thence to the right along a 70 ft. radius curve
 46.71 ft. Thence N 66° 14' W. 18.95 ft. Thence to the left

along a 50 ft. radius curve ——— 44.27 ft. Thence S63°02'W
 17.21 ft. Thence ——— to the right along a 50 ft. radius curve.
 52.16 ft. Thence N57°12'W, 140.57 ft. Thence S70°18'W
 36.01 ft. Thence ——— to the left along a 100 ft. radius curve
 37.52 ft. Thence S48°48'W, 58.56 ft. Thence ———
 to the right along a 40 ft. radius curve ——— 65.83 ft.
 Thence N36°54'W, 54.36 ft. Thence ——— to the left along an
 80 ft. radius curve ——— 60.55 ft. Thence N80°16'W, 110.64 ft.
 Thence S35°12'W, 80.24 ft. Thence ——— to the right along a 40 ft.
 radius curve ——— 59.46 ft. Thence N59°35'W, 19.06 ft. Thence
 ——— to the left along a 120 ft. radius curve ———
 43.98 ft. Thence N80°35'W, 94.78 ft. Thence ——— to the left
 along a 30 ft. radius curve ——— 31.15 ft. Thence S39°52'W
 33.05 ft. Thence ——— to the right along a 50 ft. radius curve
 48.00 ft. Thence N85°08'W, 305.27 ft. Thence
 ——— to the right along a 70 ft. radius curve ———
 37.87 ft. Thence N54°08'W, 3.05 ft. Thence ——— to the left
 along a 60 ft. radius curve ——— 65.10 ft. Thence S63°42'W, 8.30 ft.
 Thence ——— to the right along a 60 ft. radius curve, 69.11 ft. Thence N50°18'W
 76.56 ft. Thence ——— to the left along a 400 ft. radius
 curve ——— 167.55 ft., Thence N74°18'W, 161.47 ft. Thence
 N68°18'W, 41.32 ft. Thence ——— to the left, along a
 100 ft. radius curve ——— 36.65 ft., Thence N89°18'W,
 99.8 ft. Thence ——— to the right along a 150 ft. radius curve
 56.29 ft., Thence N67°48'W, 9.34 ft. Thence ———
 to the right along a 70 ft. radius curve ——— 52.94 ft.
 Thence N44°27'W, 0.03 ft. Thence ——— to the left along a
 60 ft. radius curve ——— 87.44 ft., Thence S. 72°02'W
 33.65 ft. Thence ——— to the right along a 50 ft. radius
 curve ——— 47.41 ft. Thence N53°38'W, 63.80 ft. Thence
 N76°18'W, 141.12 ft. Thence ——— to the left along
 a 100 ft. radius curve ——— 28.51 ft. Thence S87°22'W
 13.26 ft. Thence ——— to the right along a 100 ft. radius.

curve ——— 38.75 ft. Thence N70°26'W, 111.06 ft. Thence
 N76°18'W, 244.0 ft. Thence S77°42'W, 105.76 ft. Thence
 ——— to the right along a 100 ft. radius curve ———
 31.42 ft. Thence N84°18'W, 56.92 ft. Thence ——— to the
 right along a 200 ft. radius curve ——— 27.93 ft. Thence
 N76°18'W, 91.86 ft. Thence S. 61°42'W, 116.81 ft. Thence ———
 to the right along a 60 ft. radius curve ——— 37.35 ft.
 Thence N82°38'W, 41.10 ft. Thence N. 77°38'W, 52.12 ft. Thence ———
 to the right along a 200 ft. radius curve ——— 29.67 ft.
 Thence N69°08'W, 79.83 ft. Thence ——— to the right along a
 200 ft. radius curve ——— 40.14 ft. Thence N59°38'W
 89.67 ft. Thence ——— to the right along a 100 ft. radius curve
 36.65 ft. Thence N36°38'W, 4.73 ft. Thence ———
 to the left along a 60 ft. radius curve ——— 48.35 ft.
 Thence N82°48'W, 164.96 ft. Thence ——— to the left along a
 100 ft. radius curve ——— 42.76 ft. Thence S72°42'W,
 81.49 ft. Thence ——— to the right along a 60 ft. radius curve
 57.60 ft. Thence N52°18'W, 72.33 ft., Thence ———
 to the right along a 100 ft. radius curve ——— 60.21 ft.
 Thence N17°48'W, 47.58 ft. Thence N85°49'W, 45.0 ft. Thence
 ——— to the left along a 100 ft. radius curve ———
 21.82 ft. Thence S81°41'W, 95.03 ft. Thence ——— to the
 right along a 400 ft. radius curve ——— 44.22 ft.
 Thence S. 88°01'W, 65.98 ft. Thence ——— to the right along
 a 70 ft. radius curve ——— 73.30 ft. Thence N31°59'W
 2.13 ft. Thence ——— to the left along a 100 ft. radius curve
 47.12 ft. Thence N58°59'W, 12.48 ft. Thence ———
 to the left along a 100 ft. radius curve ———
 46.25 ft. Thence N85°29'W, 53.20 ft. Thence ——— to the right
 along a 400 ft. radius curve ——— 69.81 ft., Thence N75°29'W
 50.19 ft. Thence ——— to the right along a 400 ft. radius
 curve ——— 69.81 ft. Thence N65°29'W, 21.45 ft.,

thence — to the right along 100 ft. radius curve —
 37.52 ft, thence N 43° 59' W, 18 ft. to an intersection
 with the line between Secs 13 & 14 - T. 13 S. R. 3 W, it produced, 2783.94
 ft, North, from the corner common to Secs 13, 14, 23 & 24, T. 13 S,
 R. 3 W, S. B. M, thence continuing N 43° 59' W, 99.15 ft, thence N 81° 30' W
 52.94 ft, thence S 32° 29' W, 57.76 ft, thence — to the right along
 a 60 ft. radius curve — 46.07 ft, thence S 76° 29' W
 25.04 ft, thence — to the right along a 200 ft. radius
 curve — 48.87 ft, thence N 89° 31' W, 166.70 ft, thence
 S 54° 37' W, 89.34 ft, thence — to the right along a 50 ft.
 radius curve — 44.51 ft, thence N 74° 23' W, 34.85 ft,
 thence — to the left along a 50 ft. radius curve —
 56.00 ft, thence S 41° 27' W, 83.25 ft, thence to —
 the right along an 80 ft. radius curve —
 99.74 ft, thence N 68° 33' W, 87.46 ft, thence — to
 the left along a 100 ft. radius curve — 72.72 ft,
 thence S 69° 47' W, 83.16 ft, thence — to the right
 along a 100 ft. radius curve — 45.38 ft, thence
 N 94° 13' W, 50.81 ft, thence — to the right along a
 100 ft. radius curve — 28.80 ft, thence N 67° 43' W
 85.41 ft, thence — to the left along a 100 ft. radius
 curve — 41.02 ft, thence N 88° 47' W, 48.88 ft, thence
 — to the right along a 140 ft. radius curve —
 87.96 ft, thence N 55° 13' W, 70.54 ft, thence S 60° 16' W, 154.91 ft,
 thence S 5° 45' W, 36.41 ft, thence — to the right along
 a 50 ft. radius curve — 52.36 ft, thence S 66° 45' W
 47.04 ft, thence — to the right along a 200 ft. radius
 curve — 24.43 ft, thence S 73° 45' W, 40.58 ft, thence
 — to the right along a 100 ft. radius curve —
 27.63 ft, thence S 89° 35' W, 147.65 ft, thence —
 to the right along a 100 ft. radius curve — 47.12 ft,
 thence N 63° 25' W, 42.19 ft, thence — to the left along

a 100 ft. radius curve — 45.09 ft, thence N 89° 15' W, 201.65 ft,
 thence — to the left along a 50 ft. radius curve —
 67.63 ft, thence S 13° 15' W, 94.40 ft, thence —
 to the right along a 100 ft. radius curve — 84.94 ft,
 thence S 61° 55' W, 30.34 ft, thence — to the right along
 a 60 ft. radius curve — 53.41 ft, thence N 67° 05' W
 160.04 ft, thence S 19° 54' W, 42.30 ft, thence S 22° 37' E, 42.23 ft,
 thence — to the right along a 40 ft. radius curve —
 49.57 ft, thence S 48° 23' W, 107.52 ft, thence S 0° 52' W,
 61.10 ft, thence S 77° 09' E, 123.60 ft, thence — to the
 right along a 150 ft. radius curve — 154.46 ft,
 thence S 18° 09' E, 258.49 ft, thence — to the right
 along a 100 ft. radius curve — 59.34 ft, thence
 S 15° 51' W, 206.23 ft, thence — to the right along a
 100 ft. radius curve — 29.96 ft, thence S 33° 01' W
 242.18 ft, thence — to the right along a 400 ft. radius
 curve — 41.89 ft, thence S 39° 01' W, 190.35 ft, thence
 — to the right along a 100 ft. radius curve —
 34.91 ft, thence S 59° 01' W, 8.67 ft, to an intersection
 with the East line of the Staat Property; whence the quarter corner
 common to — Secs 14 & 23, T. 13 S, R. 3 W, S. B. M, ^{bear 50° 30' W, 1119.9 ft} thence
 continuing S 59° 01' W, 33.02 ft, thence — to the left
 along a 70 ft. radius curve — 40.52 ft, thence
 S 25° 49' W, 174.62 ft, thence — to the right along a
 100 ft. radius curve — 54.98 ft, thence S 57° 17' W,
 155.17 ft, thence — to the right along a 250 ft. radius
 curve — 245.80 ft, thence N 66° 23' W, 167.50 ft, thence
 — to the left along a 25 ft. radius curve —
 45.85 ft, thence S 8° 35' W, 249.29 ft, thence — to the
 right along a 70 ft. radius curve — 70.45 ft, thence
 S 66° 13' W, 95.62 ft, thence — to the right along 100 ft.
 radius curve — 41.03 ft, thence S 89° 43' W, 66.25 ft, thence

Beginning at a Point whence the Sec. Corner, common to Sections 14, 15, 22 & 23, T. 13 S, R. 3 W. S. B. M, bears N 89° 42' W, 1511.1 ft, thence S 44° 33' W, 290.26 ft, thence to the right along a 100 ft. radius curve, 97.74 ft, thence *

to the right along a 70 ft. radius curve 46.43 ft, thence N 52° 17' W, 62.46 ft, thence to the left along a 250 ft. radius curve 55.73 ft, thence S 31° 57' E, 54.73 ft, thence to the left along a 300 ft. radius curve 46.25 ft, thence S 40° 47' E, 81.45 ft, thence to the right along a 100 ft. radius curve 87.38 ft, thence S 9° 17' W, 30.67 ft, thence to the right along a 100 ft. radius curve 56.78 ft, thence S 41° 49' W, 249.06 ft, to an intersection with the South line of Sec. 14, T. 13 S, R. 3 W, S. B. M, whence the corner

common to Secs 14, 15, 22 and 23, T. 13 S, R. 3 W, S. B. M, bears N 89° 42' W - 1511.1 ft, thence S 44° 33' W, 290.26 ft, thence to the right along a 100 ft. radius curve 97.74 ft, thence N 79° 27' W, 294.69 ft, thence to the left along a 200 ft. radius curve 47.12 ft, thence S 87° 03' W, 89.48 ft, thence

to the right along a 100 ft. radius curve 53.52 ft, thence N 62° 17' W, 43.48 ft, thence to the left along a 20 ft. radius curve 45.84 ft, thence S 13° 39' E, 32.55 ft, thence to the right along a 200 ft. radius curve 226.31 ft, thence S 51° 11' W, 49.69 ft, thence to the right along a 200 ft. radius curve 54.69 ft, thence S 66° 51' W, 575.01 ft, to an intersection with the line between Secs 22 and 23, T. 13 S, R. 3 W, S. B. M, whence the corner common to Secs

14, 15, 22 & 23, T. 13 S, R. 3 W, S. B. M, bears N 0° 12' E, 702.5 ft, thence continuing S 66° 51' W, 72.95 ft, thence to the right along a 100 ft. radius curve 30.54 ft, thence S 84° 21' W, 344.54 ft, thence to the right along a 120 ft. radius curve 124.27 ft, thence N 36° 19' W, 83.92 ft, thence to the left along a 25 ft. radius curve 42.98 ft, thence S 45° 09' W, 136.54 ft, thence to the right along a 100 ft. radius curve 118.68 ft

"7"

thence $N66^{\circ}51'W$, 142.52 ft, thence ~~to the left~~ along
 a 50 ft. radius curve ~~59.05 ft, thence $S45^{\circ}31'W$~~
~~31.07 ft, thence~~ to the right along a 200 ft. radius
 curve ~~210.60 ft, thence $N74^{\circ}11'W$, 258.09 ft, thence~~
~~to the right~~ along a 300 ft. radius curve
 45.87 ft, thence $N66^{\circ}51'W$, 275.71 ft, thence ~~to the~~
 left along a 100 ft. radius curve ~~67.19 ft, thence~~
 $S76^{\circ}39'W$, 133.72 ft, thence ~~to the right~~ along a
 100 ft. radius curve ~~66.32 ft, thence $N65^{\circ}21'W$~~
 244.56 ft, thence ~~to the left~~ along a 200 ft. radius
 curve ~~40.72 ft, thence $N77^{\circ}01'W$, 203.61 ft,~~
 thence ~~to the left~~ along a 200 ft. radius curve.
 38.40 ft, thence $N88^{\circ}01'W$, 227.93 ft, thence
 to the right along a 200 ft. radius curve ~~22.22~~
 ft, to the intersection with the East line of Rancho San
 Dieguito, whence corner $N^{\circ}8$, ^{of said Rancho San Dieguito} located by a rock marked S.D.N.2
 bears $N4^{\circ}50'W$, 3081.1 ft

$\frac{3081.1}{43.3}$

Carroll Conduit.

Carry in.
 Proposed to carry a safe yield of
 $M I = \text{--- sec. ft.} - \underline{10,000}$ Acc ft. annually.

Carroll System.

Hydraulic ~~of the system~~ Data.

Safe Yield. The safe yield arrived
by Port was ~~11,000~~ 10,400 Acre ft.

Can provide for 14,500 Acre ft
ultimate -

Provide a maximum run-
during summer of 15% per month
or 2200 Acre ft or 36 sec ft.

15-00
10-00

25-00

15-00
19-00

34-00

25-

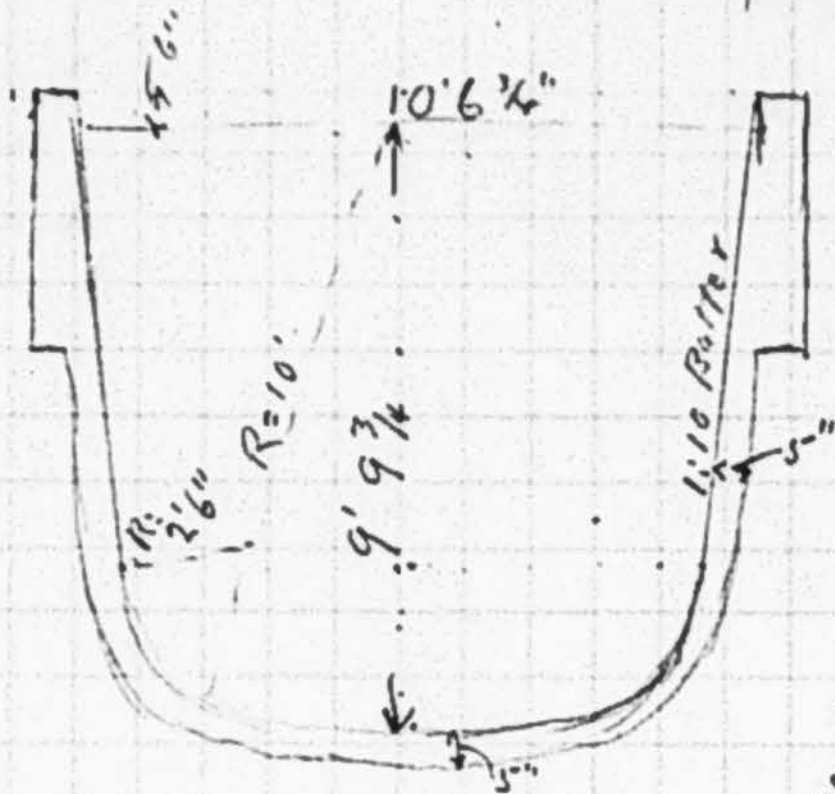
4400

1900

3400

HAMMERMILL
POSTOFFICE BOX

Los Angeles Aqueduct. Conduit Sections

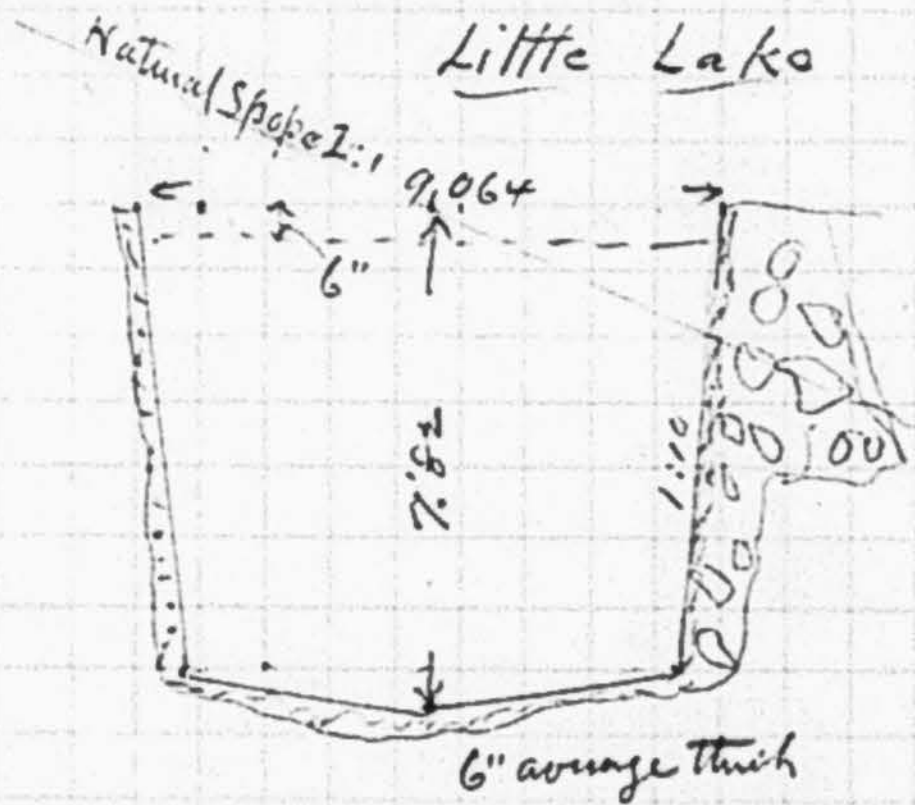


Red Rock, Dixie + Rose Valley -

$Q = 430$	excavation	4.06
$S = .0004$	concrete Conduit	0.561
$n = .014$	" Crew	0.159
$A = 89.16$	steel in "	25.1 #
$R = 3.43$		
$C = 130$		
$V = 4.825$		

Economical cost found to be for above 430 Q
 $S = .0004 + n = .014$ when $\frac{\text{Depth}}{\text{Width}} = .97 \text{ to } 1.00$

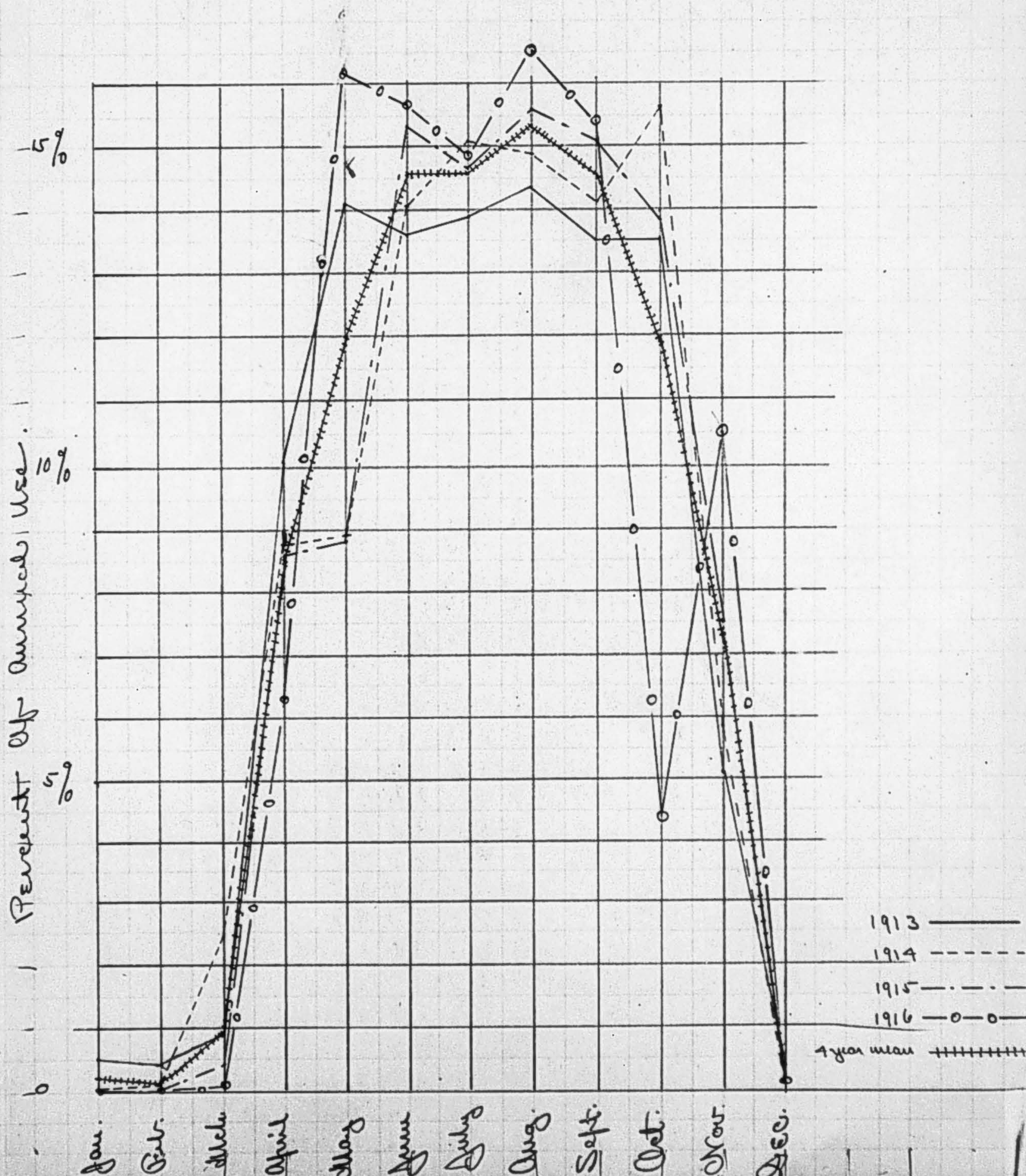
Little Lake Bench Conduit.



$Q = 429$	excav.	2.91	1.00	2.91
$S = .0009$	concrete	0.46	6.93	3.19
$n = .014$	crew	0.12	7.62	0.93
$A = 66.64 \text{ sq. ft.}$	steel	19 #	3.15	0.59
$R = 2.865$				
$C = 126.8$				
$V = 6.45$				
Total Cost				7.62

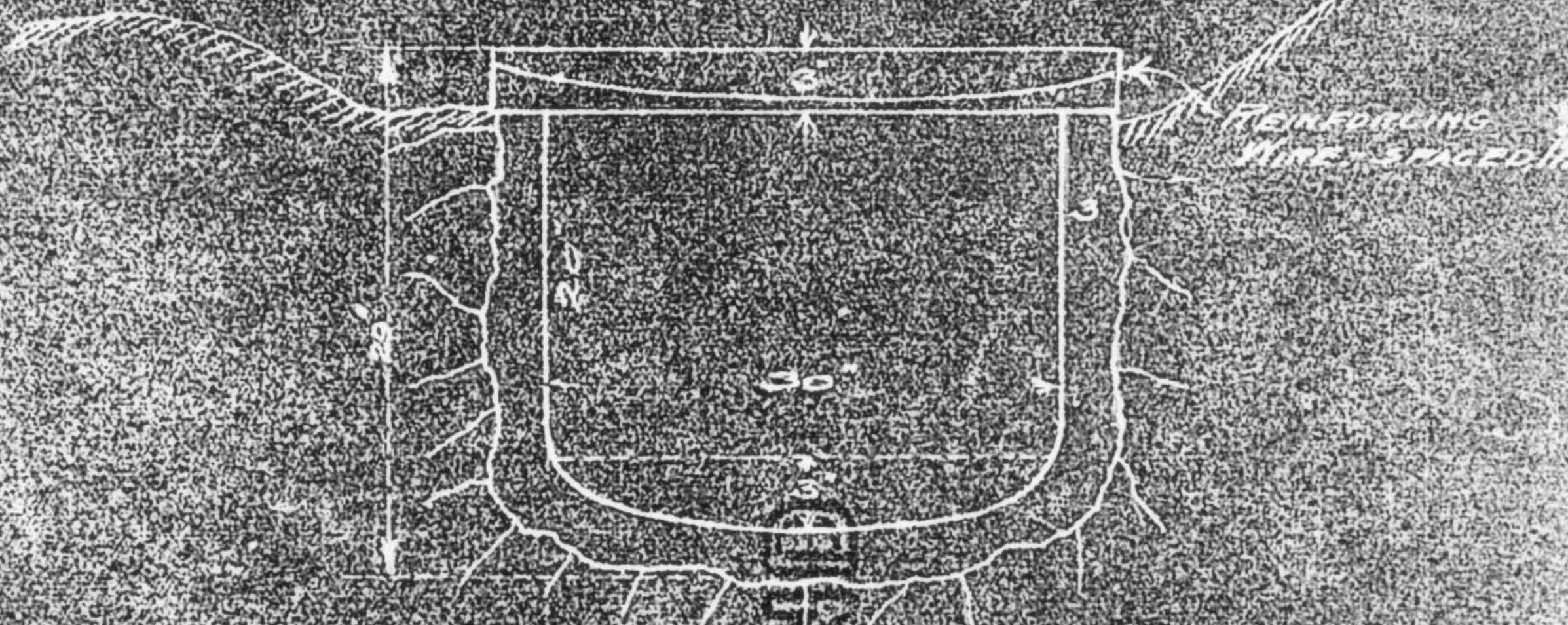
Economic sect. covered = $\frac{\text{Depth}}{\text{width}} = .97$
 " " uncovered = " = .55

Diagram of Use of Water at Hercul.
 Showing Monthly Percentages of Annual Use.



CIVIL ENGINEERING

SECTIONAL SLAB COVER 36"x18"



COTTONWOOD CREEK CONDUIT

Showing Slab Covers

Designed by Wm. M. Hollander

Sept - 27

Vol of Concrete per 1 ft. = 0.568 cu yds

2000 ft of conduit @ 0.568 = 1136 cu yds of concrete

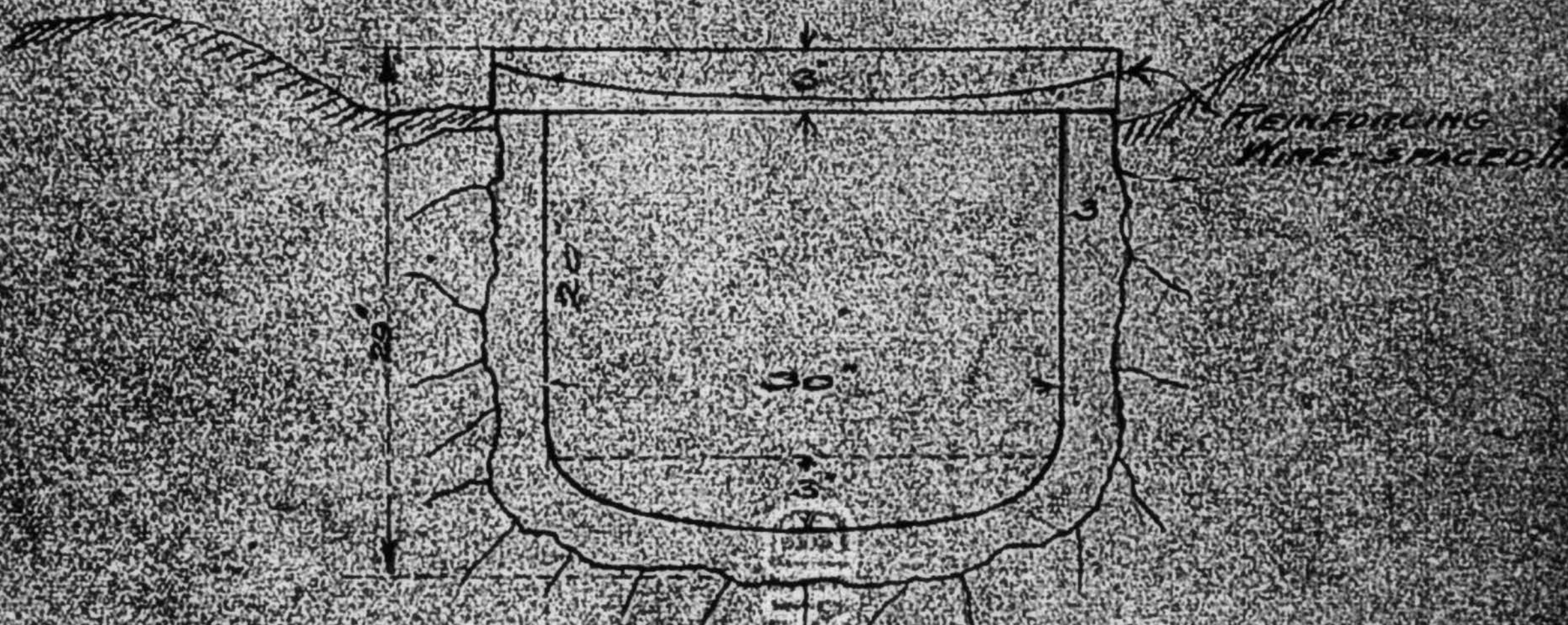
CIVIL ENGINEERING

5-39

10

CALIFORNIA

SECTIONAL SLAB COVER 36" x 18"



COTTONWOOD CREEK CONDUIT

Showing Slab Covers

Designed by Wm. Mulholland

Sept. 1907

Vol. of Concrete per 1 ft. = 0.568 cu yds.

2000 ft. of conduit @ .0568 = 113.6 cu yds. of concrete.

5-39

CALIFORNIA

COTTONWOOD POWER-PLANT CONDUIT (Designed for 24 sec.ft.)

	Cubic Yds.	Cost per cu. yd.	Lin. ft.	Cost per lin.ft.	Total Cost.
Excavation -	3,176	\$.89	7,042	\$.40	\$2,825.45
Lining -	956	9.95	7,042	1.35	9,500.89
		<u>\$10.84</u>			
Back-fill -	-	-	7,042	.03	179.59
Engineering -	-	-	7,042	<u>.08</u>	<u>589.32</u>
Average cost per foot	-	-	-	\$1.86	\$13,095.15 (Total)

Sand and rock averaged about 50 cents per c.y. concrete.

3,885 sacks of cement used, or an average of 1 barrel per cu.yd.

Mixture, 1 - 3 - 6.

Price of cement, \$2. per sack. 17 barrels only at \$5.40 per bbl.

Conduit.

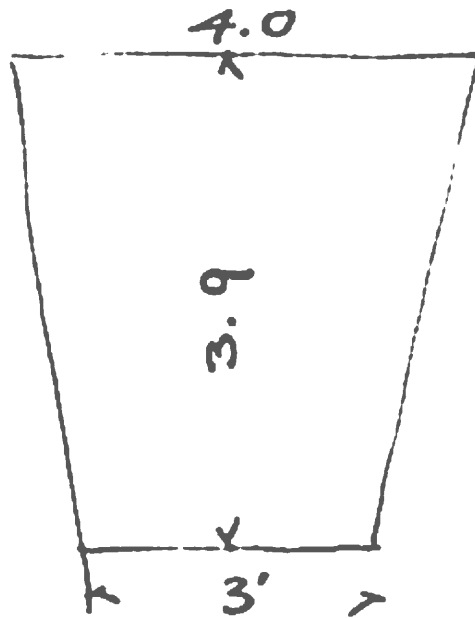
using $n = .015$ Kutter.
slopes $\frac{1}{2}$ to 1

Grade per 1000	Bottom width	Depth Water Surface	Q.
1	4	3.5	94
1	3	3.5	73
1	4	3	70

$\frac{1}{2}$	4	3.5	66
$\frac{1}{2}$	4	3	49.5
$\frac{1}{2}$	4	3.2	54.5
$\frac{1}{2}$	3.5	3.5	57.
$\frac{1}{2}$	3.5	4.0	72.

Adopt 3.5 4' 2" for 68 seft.

$$\frac{15}{50} = \frac{5}{250}$$



35.6 sq. feet
 $S. = .0005$

GRAPEVINE DIVISION

S = 0.0017

Scale $\frac{3}{4}$ " = 1'

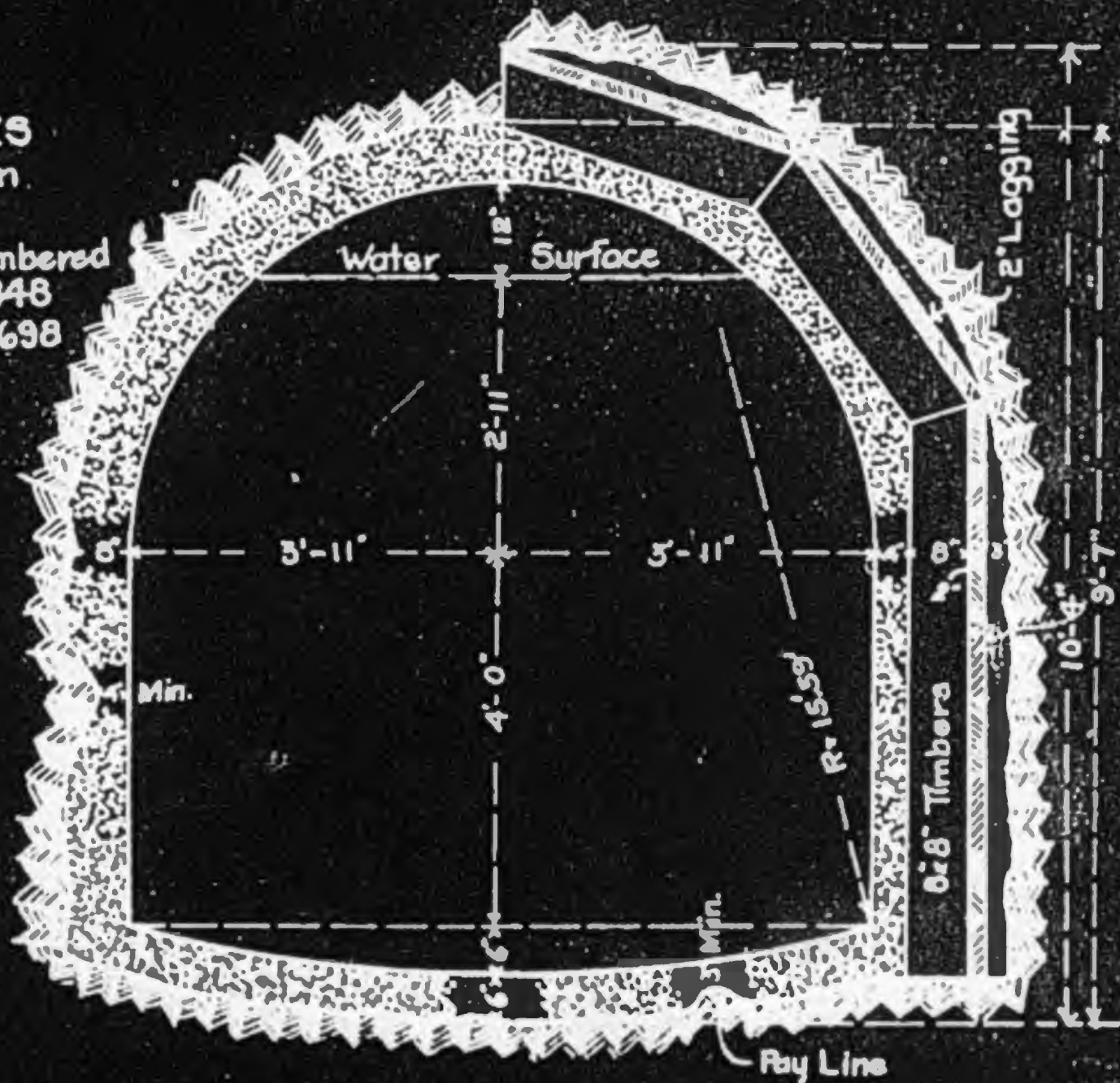
CONSTRUCTION QUANTITIES

Per Lineal foot of Tunnel Normal Section

	Unit	Timbered	Untimbered
Excavation	Cu Yds	3.514	2.848
Concrete in Lining	" "	.945	.698
Timbers	B.M.	32.0	
Spreaders	" "	5.0	
Shoulder Braces	" "	7.0	
Logging	" "	47.0	

HYDRAULIC PROPERTIES

Slope	.0017
Capacity	434.13
Velocity	7.97
Area	54.462
Wetted Perimeter	22.499
Hydraulic Radius	2.42
<i>n</i>	.014
<i>C</i>	124.29



GRAPEVINE DIVISION

S = 0.0017

Scale $\frac{1}{4}'' = 1'$

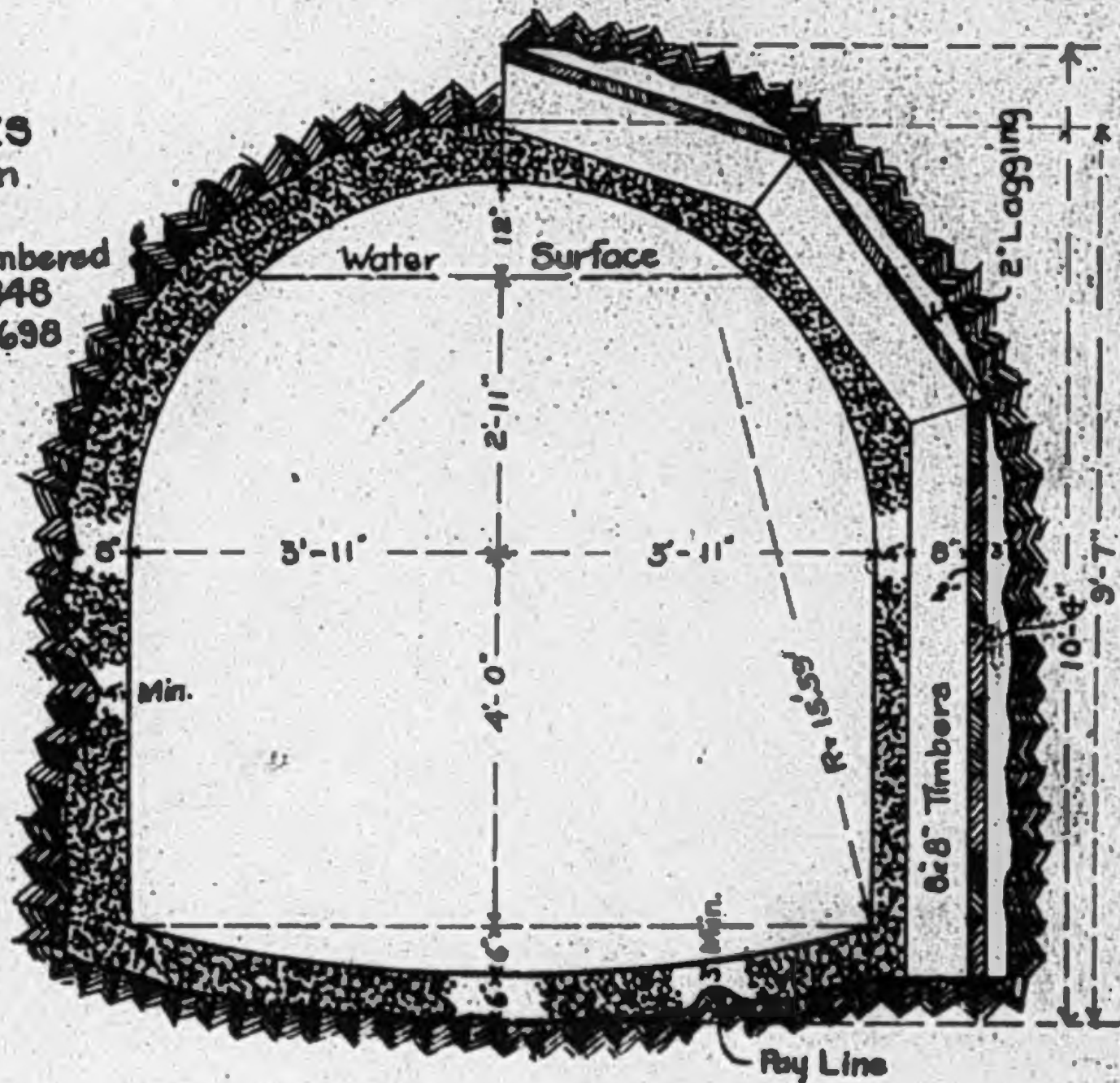
CONSTRUCTION QUANTITIES

Per Lineal foot of Tunnel Normal Section.

	Unit	Timbered	Untimbered
Excavation	Cu Yds	3.514	2.848
Concrete in Lining	"	.945	.698
Timbers	B.M.	32.0	
Spreaders	"	5.0	
Shoulder Braces	"	7.0	
Logging	"	47.0	

HYDRAULIC PROPERTIES

Slope	.0017
Capacity	434.13
Velocity	7.97
Area	54.462
Wetted Perimeter	22.499
Hydraulic Radius	2.42
<i>n</i>	.014
<i>C</i>	124.29



Hardest of 43 miles of tunnel 10 x 10
lined \$22 (for a short distance \$27)

No timbering necessary in Hard Rock.

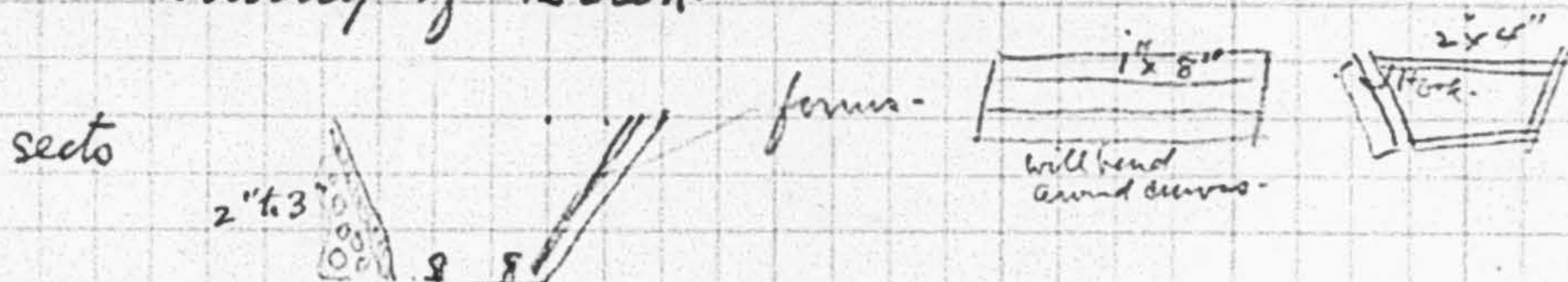
No lining necessary except to avoid friction
& possible seepage.

Melkalland says \$ should make
7 x 7 without being perfectly safe figure

Notes on Sprockels contract
Cottonwood Cr. Del. Zura, Cal.

10 miles of ditch - decomposed granite
 $\frac{3}{4}$ mile of tunnels - \$20 per ft. Hard granite unlined -
 lost money @ \$15. 4.6" x 6.6" good miners took contracts
 @ \$15 with Co. furnishing powder cost \$2.50 ± - about crew.
 Grading contract by Crowley & Sherer 75 cts
 per yd. decomposed granite some shooting.
 lost money.

Lining of Ditch.



Cement 1 bbl to 1 yd -
 Sand .65 c.y " 1 "
 Crushed Rock & gravel 1.00 ± 1 "
 1 yd

Gang averaged 14 batches per day in place

Gang =	1 Foreman	\$4	4
	1 Handy man	\$3	3
	2 Helpers	2.50	5
	8 men	2.00	<u>16</u>

\$2 per yd - for all handling -
 does not include delivery of materials -

This ditch average 10 c.f. per running ft =
 one gang would do 93 lineal ft per day average.

If mixer could be used. \$1.00 or less

$\frac{1}{4}$ yd charge - 9 H.P. gas engine -

on basis of 3" thick.

Cost of Labor for lining sidewalls of
ditch per sq foot by - hand \$0.74.

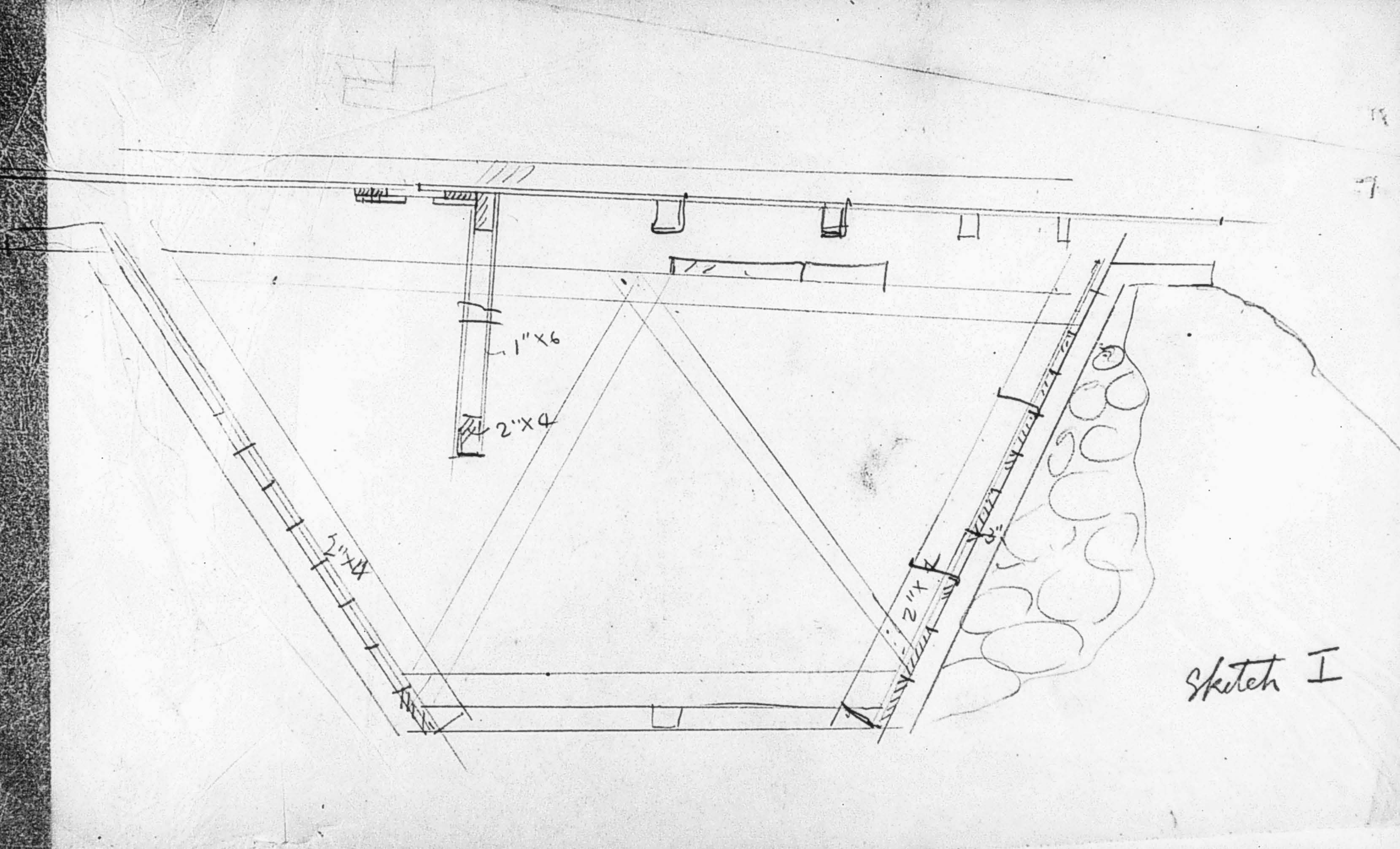
Cost of Labor for lining sidewalls of ditch using
machines - = .0348 per sq ft

Cost of lumber for forms 800⁰⁰ per mile of ditch

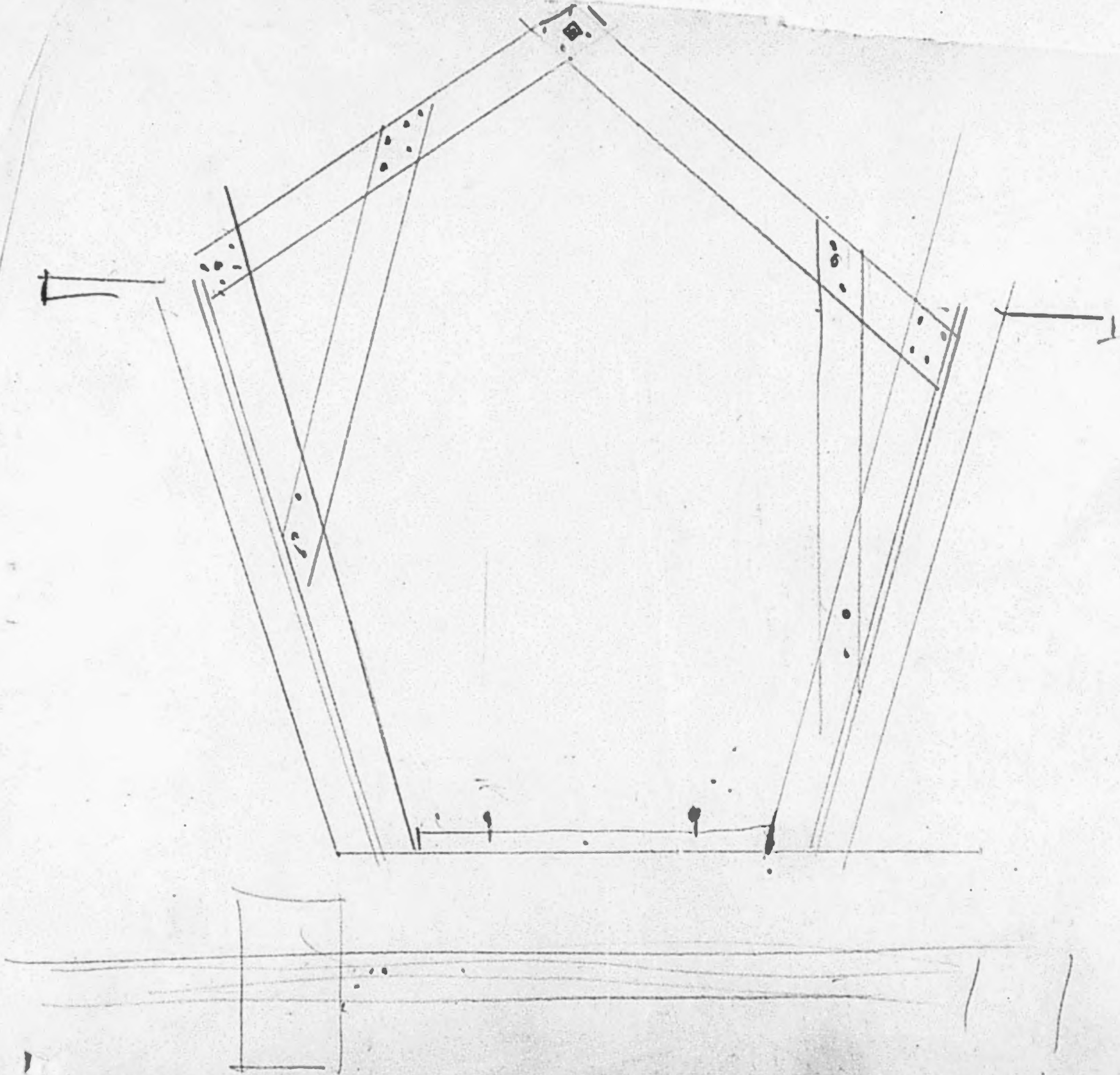
Forms are worth say 1 Cent per sq ft of ditch

expansion joint

grouting in neat cement

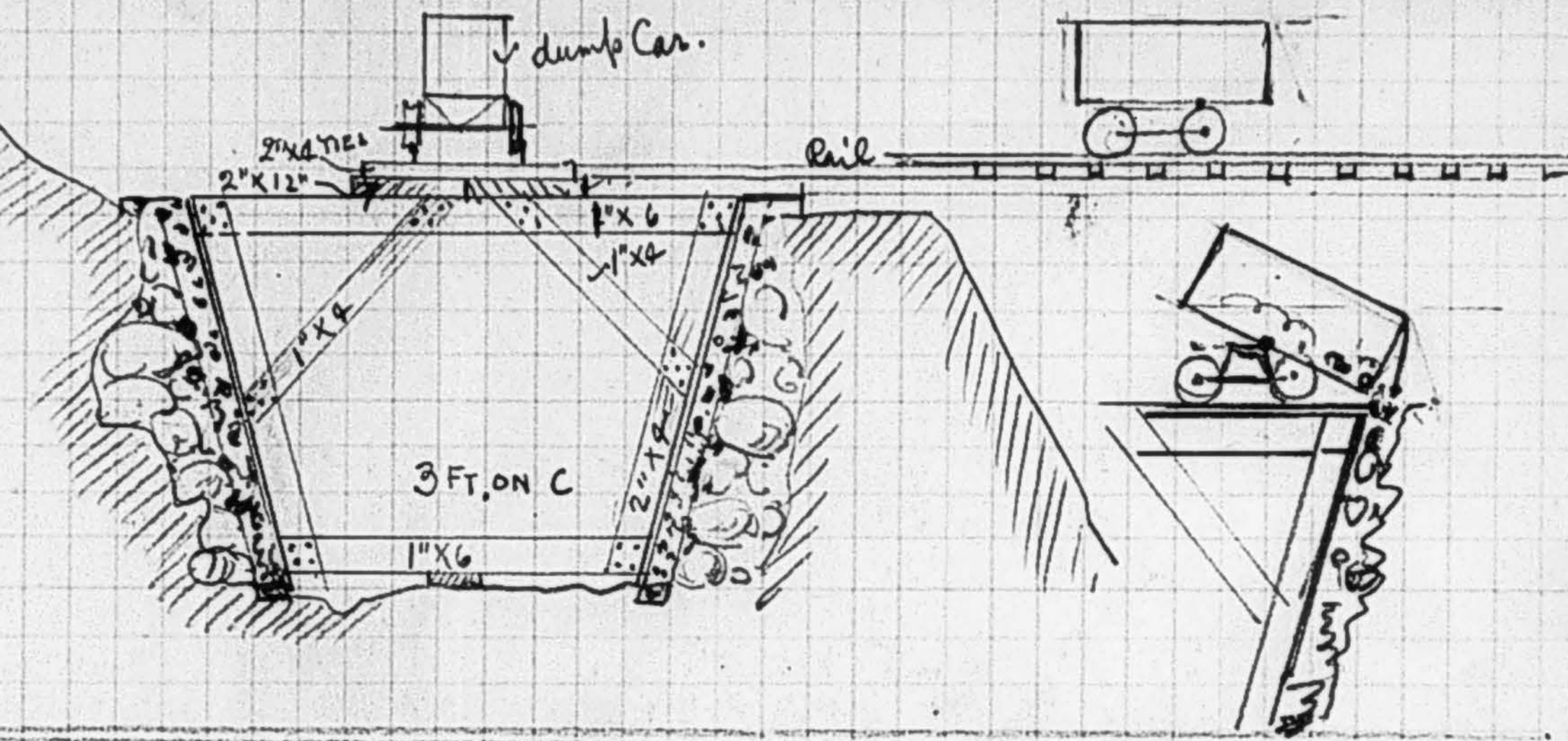
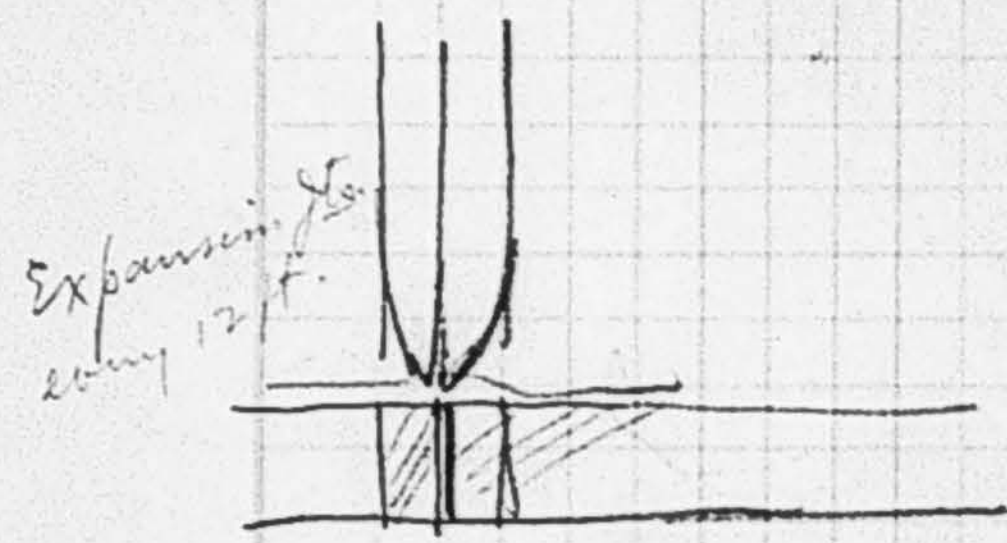


Sketch I

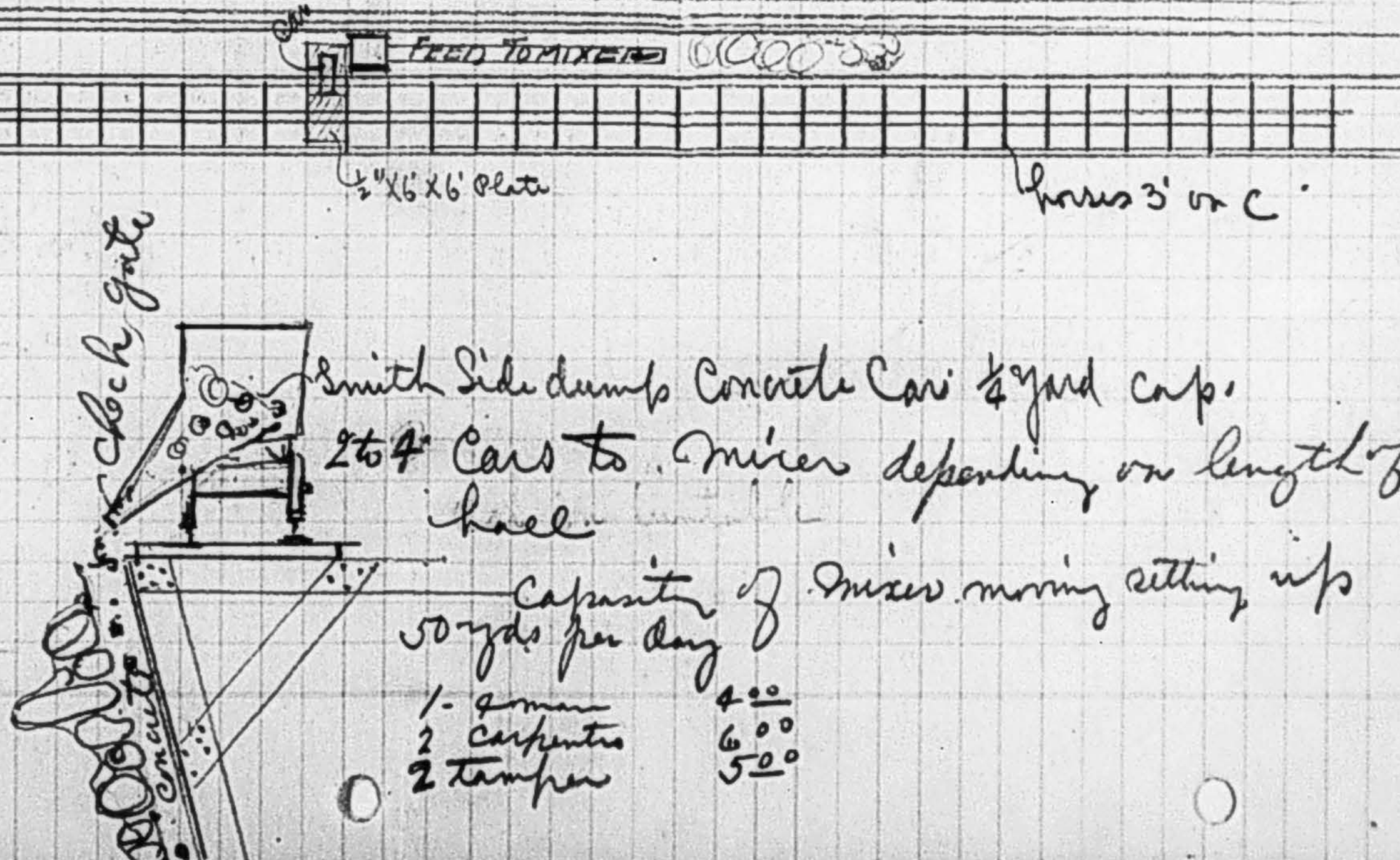


Sketch
II

LINE DITCH BY HAND.
SIDE WALLS PER MILE



1	tending Cement	2 00	2
3	" Rock	2 00	6
2	" Sand	2 00	4
1	Gas Smege	4 10	4
1	Trowel	4 10	4
2	Tampers	2 50	5
3	CR Men	2 00	6
2	carpenters	3 00	6
2	helpers	2 50	5
2	utility men	2 00	4
		<u>\$46 00</u>	
		Gasoline	
		<u>4 700</u>	
		Cost 50 yds	



Capacity of mixer moving setting up
50 yds per day

1 - 4 man	4 00
2 carpenters	6 00
2 tampers	5 00

houses 3' on C

Table Showing Cu Yds Per Lin Foot Excavation for each Foot of Φ Cut in Various Slopes

Depth of Cut	Slope 1:1	Slope 1:2	Slope 1:4	Level	Sec Taken Inside Dimension
0 ft	.09	.05	.04	.03	
1 ft	.20	.19	.17	.17	
2 ft	.37	.33	.33	.30	
3 ft	.56	.50	.49	.48	
4 ft	.80	.69	.67	.66	
5 ft	1.06	.92	.88	.87	
6 ft	1.41	1.16	1.13	1.10	

Table Showing Cu Yds per Lin Foot Excavation for each Foot of Φ Cut in cuts from 7' to 10' deep incl Taken 3'5 ft wide at bottom & sides at $\frac{1}{2}$:1 slopes

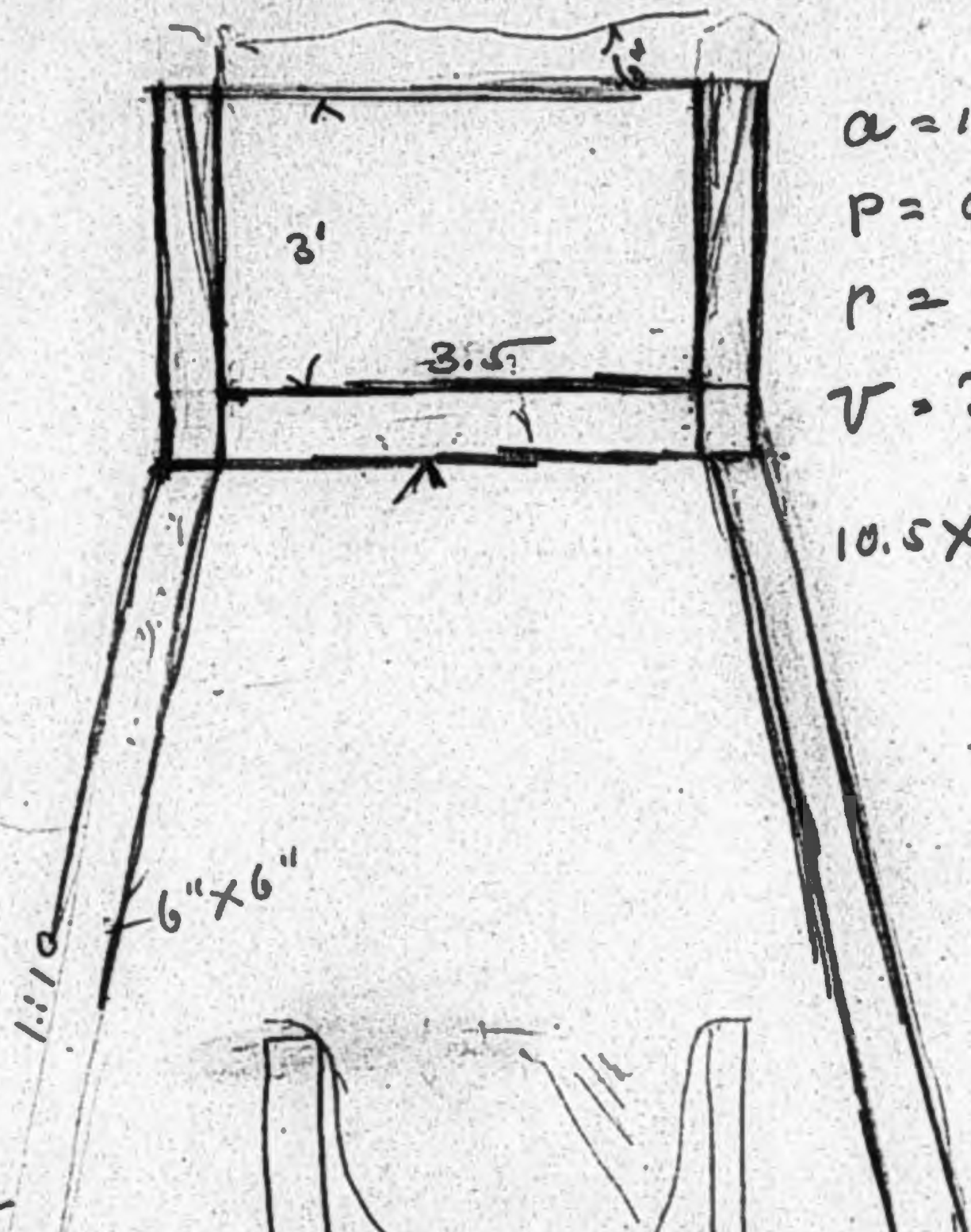
Depth of Cut	Cu Yds
7 ft	1.85
8 ft	2.22
9 ft	2.67
10 ft	3.15

Carroll Canal 6 2/5

$$\begin{array}{r} 267 \\ 185 \\ \hline 82 \end{array}$$

$$\begin{array}{r} 315 \\ 222 \\ \hline 93 \end{array}$$

$$\begin{array}{r} 315 \\ 93 \\ \hline 408 \end{array}$$



$$a = 10.5$$

$$p = 9.5$$

$$r = 1.1$$

$$V = 3.34$$

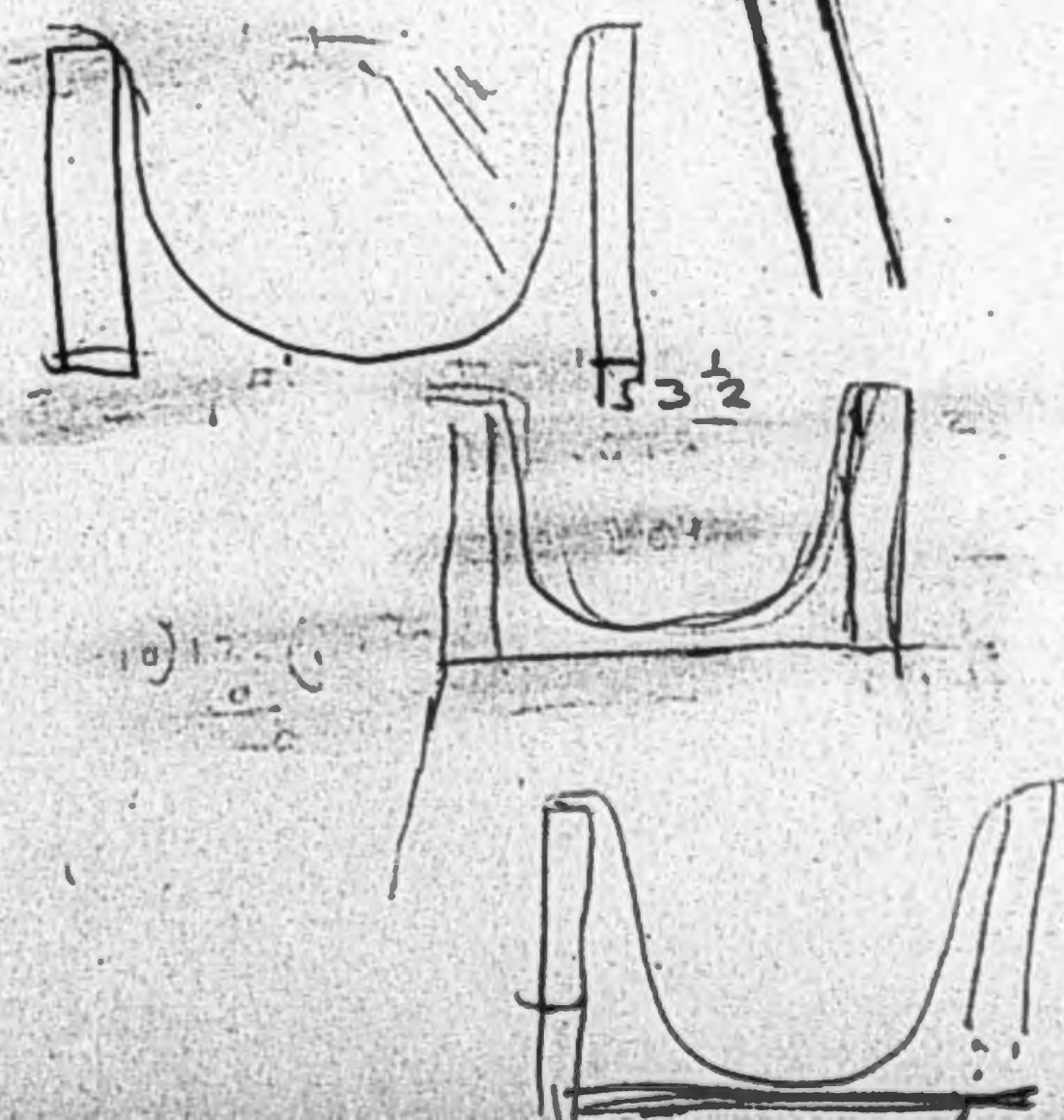
$$10.5 \times 3.34 = 35.2$$

300 ft

$$\begin{array}{r} 3.13 \\ 3.55 \\ \hline 6.68 \\ 3.34 \end{array}$$

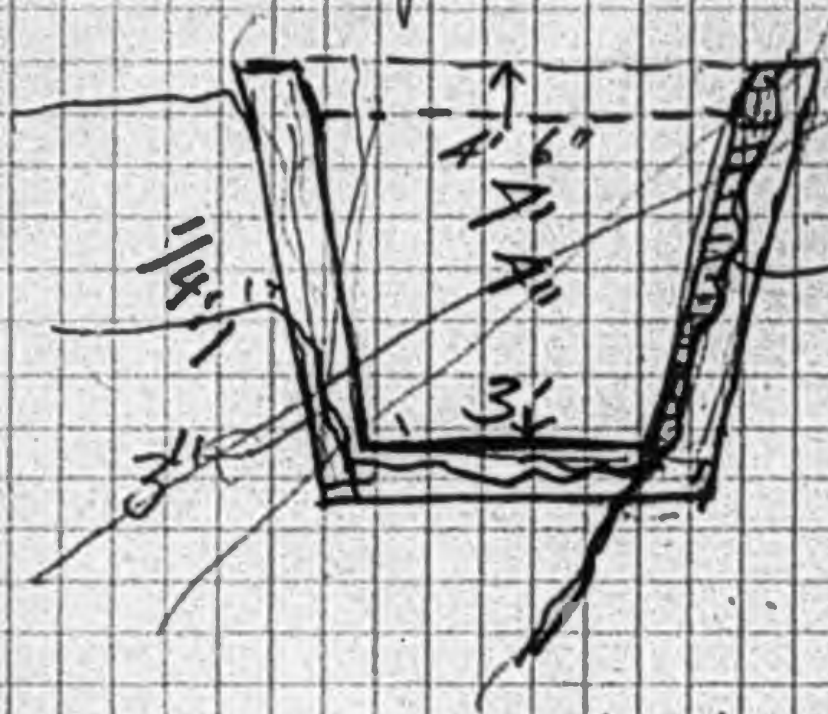
12 ft
10

$$\frac{10.5}{9.5} = 1.1$$

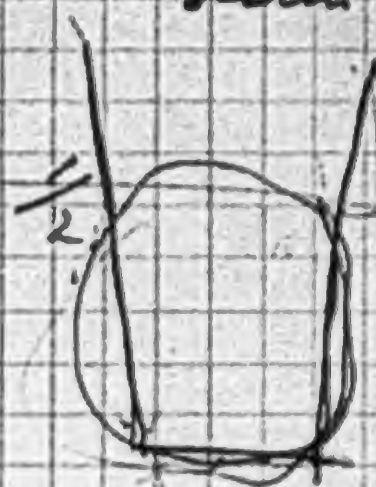
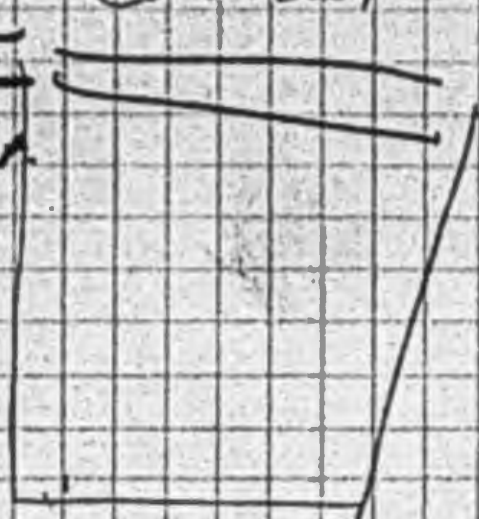


Open conduit

Covered conduit Deep section



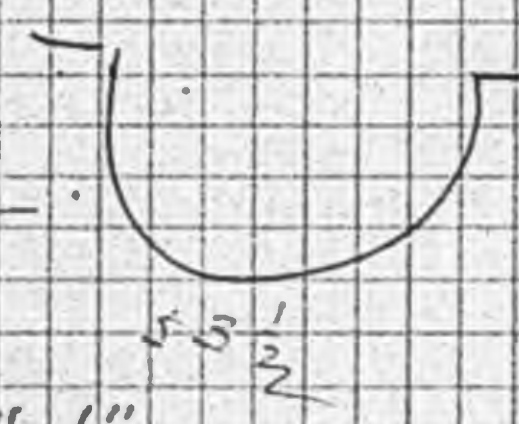
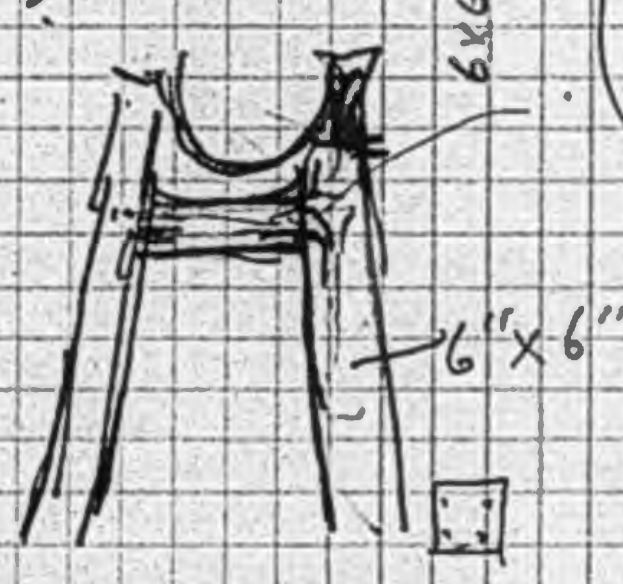
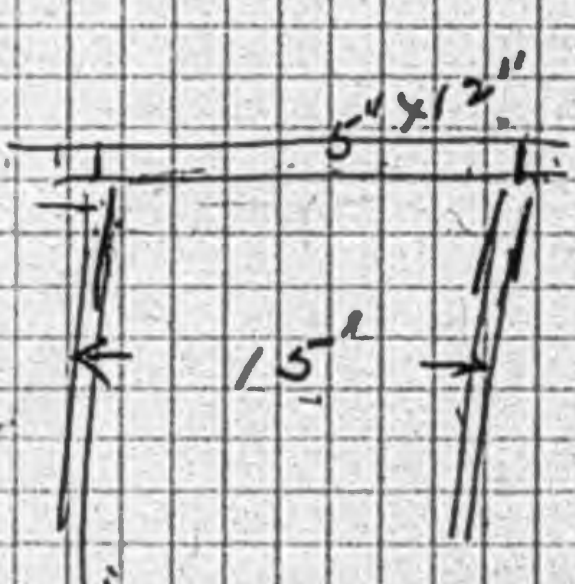
4" Slab.
1/2 #3 Rods @ 2'.



Load = 500#

Flume + Truss

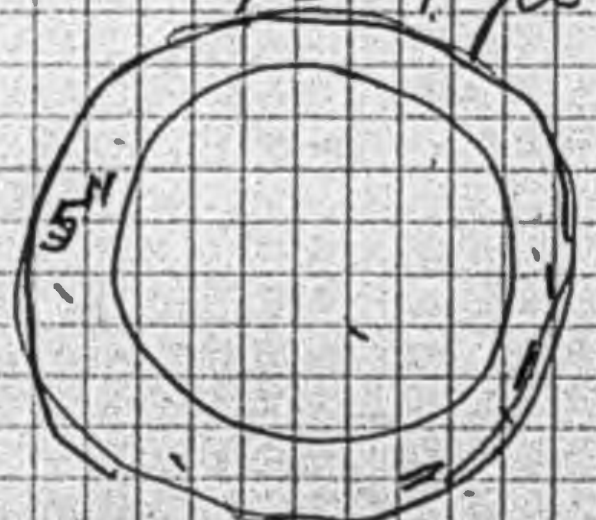
steel 2-1/2" sq. bars.



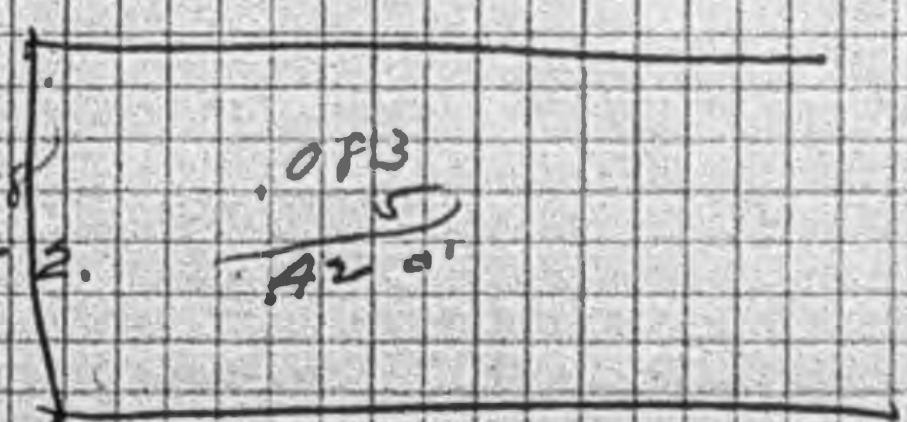
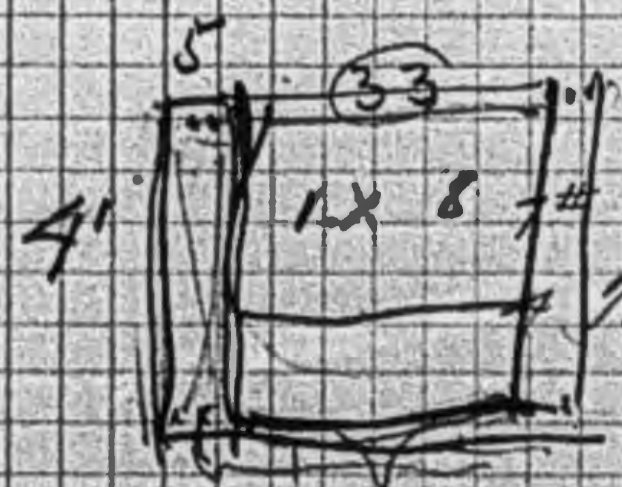
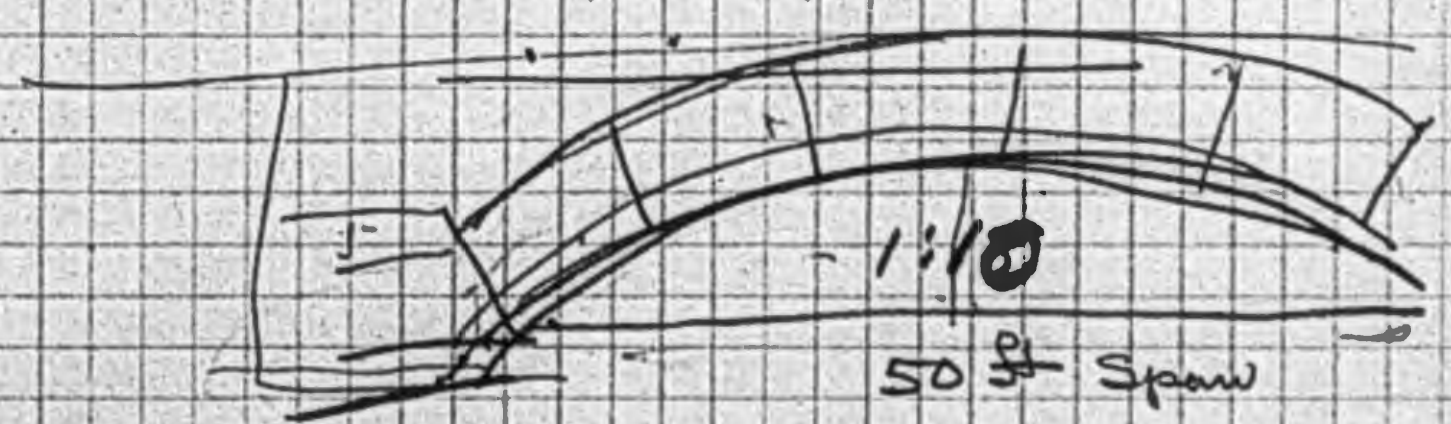
62.5'

Reinforced Pipe

42" Pipe



Pipe Arch



Grades

254.00

Elevation at 0+00

963 Siphon + Tristle @ 1
3037 Conduit @ .45

.96
1.37 2.33

Elevation at 40+00

251.07

277 Siphon + Tristle @ 1
623 Conduit @ .45

.38
.28 .66

Elevation at 50+00

251.01

221 Tristle @ 1
777 Conduit @ .45

.22
.35 .57

Elevation at 60+00

250.44

145 Tristle @ 1
855 Conduit @ .45

.14
.39 .53

249.91

Elevation at 70+00

286 Siphon + Tristle @ 1
714 Conduit @ .45

.28
.32 .60

249.31

Elevation at 80+00

157 Tristle @ 1
1833 Conduit @ .45

.17
.23 1.00

248.31

Elevation at 100+00

194 Tristle + Siphon @ 1
1506 Conduit @ .45

.19
.81 1.00

247.31

Elevation at 120+00

50 Tristle @ 1
1950 Conduit @ .45

.05
.88 .93

246.38

Elevation at 140+00

50 Tristle @ 1
950 Conduit @ .45

.05
.43 .48

245.90

Elevation at 150+00

32 Tristle @ 1
968 Conduit @ .30

.03
.29 .32

245.58

Elevation at 160+00

50 Tristle @ 1
1950 Conduit @ .30

.05
.58 .63

244.95

Elevation at 180+00

40 Bridge @ 1
1960 @ .30

.04
.59 .63

244.32

Elevation at 200

Elevation at 200+00

244.32

1050 Siphon @ 1
1530 Conduit @ .30

1.05
.46 1.51

Elevation at 225+80

242.81

302 Conduit @ .30

.09

{ Elevation at 228+82
Same (Equation)

242.72

{ Elevation at 232+97.6

242.72

1802.4 Conduit @ .30

.54

Elevation at 257

242.18

Elevation at 0+00 254.00 ✓

963 Supply + Trunk @ 1 .76
2037 Conduit @ .45 1.37

2.33

Elevation at 40+00 251.67 ✓

377 Supply + Trunk @ 1 .35
623 Conduit @ .45 .28

.66

Elevation at 50+00 251.01 ✓

221 Trunk @ 1 .22
779 Conduit @ .45 .35

.57

Elevation at 60+00 250.44 ✓

145 Trunk @ 1 .14
855 Conduit @ .45 .39

.53

Elev at 70+00 249.91 ✓

286 Supply + Trunk @ 1 .28
714 Conduit @ .45 .32

.60

Elev at 80+00 249.31 ✓

167 Trunk @ 1 .17
1833 Conduit @ .45 .83

1.00

Elev at 100+00 248.31 ✓

194 Trunk + Supply @ 1 .19
1806 Conduit @ .45 .81

1.00

Elev at 120+00 247.31 ✓

50 Trunk @ 1 .05
1950 Conduit @ .45 .88

.93

Elev at 140+00 246.38 ✓

82 Trunk @ 1 .08
1918 Conduit @ .45 .86

.94

Elev at 160+00 245.44 ✓

50 Trunk @ 1 .05
1960 Conduit @ .45 .88

.93

Elev at 180+00 244.51 ✓

40 Trunk @ 1 .104
1760 Conduit @ .45 .88

.92

Elev at 200+00 243.59 ✓

1050 Supply @ 1 1.05
1530 Conduit @ .45 .69

1.74

Elev at 225+80 241.85

Elevation at 225+80 241.85

302 Conduit @ .45 .14

241.71

Elevation at 228+82

Same

Elevation at 232+97.6 241.71

1802.4 @ .45 .81

240.90

254.00
- 12.15

241.85

241.85
- 12.15

229.70

229.70
- 12.15

217.55

0118510
72625
85621

625
14
1000
125
875

4' deep x 4' wide - 16 sq ft =
14 cu ft water per lin ft of flume =
14 x 62.5 = 875 lbs w per lin ft of flume

3.5 ft of 2 1/2" slab @ 32 lbs per foot = 112 lbs

875 lbs w of water
112 lbs w of bottom slab
987
5(493.5)
98.7

25' span will

118.
51
67
169.
51.4
117.6
98.7
18.9 Excess

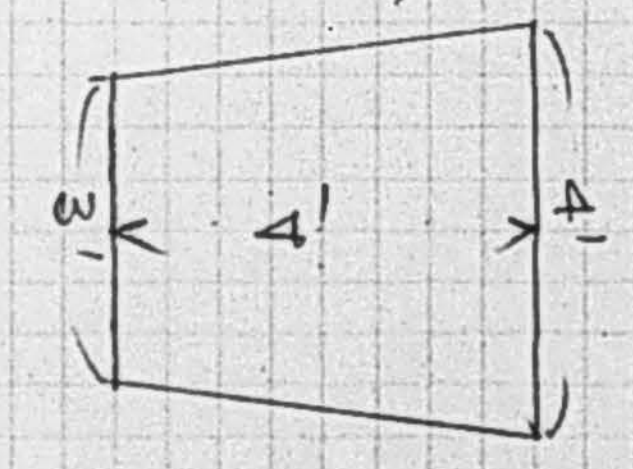
987
314
1150.1
51.4
5
257.0
51.4

169
150.1
18.9 Excess
169
124.4
vs.

Open Conduit Yardage Table for Carroll Conduit
Showing Cuyds per Lin Foot

Depth of Cut	Slope 1:1 Cuyds	Slope 1:2 Cuyds	Slope 1:4 Cuyds	Slope 1:8 Cuyds	Level Cuyds
off	.091	.049	.036		.032
1 ft	.19	.17	.17		.16
2 ft	.33	.31	.30	.30	.30
3 ft	.54	.47	.46	.46	.46
4 ft	.83	.654	.636	.627	.625
5 ft	1.195	.874	.830	.820	.820
6 ft	1.611	1.144	1.075	1.061	1.055
7 ft	2.164	1.477	1.379	1.358	1.348

Table for
Trapezoidal
Section



①

Estimate of Cu Yds per foot on

Concrete trusses for Steel Flume

Assuming average height of vents at 15 ft
& Span of 15 ft

$.5 \times .5 \times 30' = 7.50$ cu ft in uprights

$.5 \times .5 \times 5 = 1.25$ cu ft - struts

$.833 \times 1 \times 15 = 12.50$ cu ft - Stringer

$.0333 \times 5.5 \times 10 = 4.58$ cu ft - connection

25.83 cu ft

Sill $1 \times 1 \times 10 = 10.00$ cu ft

27 / 35.83 cu ft -

15 / 1.3270 cu yds

.08847 cu yds per lin foot

②

Estimate of Cu Yds per foot on Concrete Flume

Assuming average height of 5' 6"

$4' \times .833 \times 2 \times 2.5 = 166.666 =$ Girders

$3.5' \times .21 \times 2.5 = 18.375 =$ Floor Slab

$5' \times .5 \times 15 = 3.750 =$ Bent up brace

$1 \times 1 \times 9 = 9.000 =$ Sill

27 / 197.791 = Total cu ft

25 / 4.436 cu yds per 25' Section

.17745 cu yds per foot

6336.4

11260.4

17596.8

Carroll Canal

Summary of Excavation

Sheet	Yds		Total
	E	LR	
1	190.4 ✓	714.1 ✓	904.5 ✓
2	230.9 ✓	547.4 ✓	778.3 ✓
3	78.1 ✓	750.9 ✓	829.0 ✓
4	✓	1541.1 ✓	1541.1 ✓
5	347.1 ✓	735.9 ✓	1083.0 ✓
6	589.5 ✓	589.5 ✓	1179.0 ✓
7	667.9 ✓	668.1 ✓	1336.0 ✓
8	2090.5 ✓	580.5 ✓	2671.0 ✓
9	2938.0 ✓	573.3 ✓	3511.3 ✓
10	3128.0 ✓	✓	3128.0 ✓
	<u>10260.4 ✓</u>	<u>6700.8 ✓</u>	<u>16961.2 ✓</u>

$$\begin{array}{r} 10260.4 \\ 6700.8 \\ \hline 16961.2 \end{array}$$

Excavation Computation

10 Pages

①

Carroll Canal

3 ft & cut assumed except where greater is indicated on Profile

Stations based on Contour Survey by McFadden
Feb 1917 Begins at Dam site 'C'

Sta	Dist	Slope	Average Cut	CuYds per Foot	Total CuYds	Classification			Remarks
						E	L.R.	S.R.	
0+00						(10%)		(90%)	
1+00	100	1:3	3.0	.50	50.	5.		45.	
2+05	105	1:4	3.0	.49	51.5	5.2		46.3	51.45 5.14 46.31
2+60	55	Br.	—	—	—	—	—	—	
3+00	40	1:3	3.0	.50	20.0	2.		18.	
4+00	100	1:3	3.0	.50	50.	5.		45.	
5+00	100	1:3	3.0	.50	50.	5.		45.	
6+00	100	1:3	3.0	.50	50.	5.		45.	
7+00	100	1:3	3.0	.50	50.	5.		45.	
7+60	60	1:3	3.0	.50	30.	3.		27.	
8+08	48	Trestle	—	—	—	—	—	—	
8+70	62	1:3	3.0	.50	31.	3.1		27.9	
9+56	86	Trestle	—	—	—	—	—	—	
10+00	34	1:3	3.0	.50	17.	1.7		15.3	
11	100	1:3	3.0	.50	50.	5.		45.	
12	100	1:3	3.0	.50	50.	5.		45.	
13	100	1:3	3.0	.50	50.	5.		45.	
14	100	1:3	3.0	.50	50.	5.		45.	
15+10	110	1:2	3.0	.50	55.	5.5		49.5	207.33 141.90 95.23
16+40	50	Trestle	—	—	—	—	—	—	
17+10	60	1:6	6.0	1.12	6.72	33.6		33.6	
18	90	1:6	4.0	.67	6.03	30.1		30.2	
19	100	1:4	3.0	.49	4.9	24.5		24.5	
20	100	1:4	3.0	.49	4.9	24.5		24.5	
+50	50	1:4	3.0	.49	24.5	12.2		12.3	
					<u>904.5</u>	<u>190.4</u> ✓		<u>714.1</u> ✓	

$$\begin{array}{r} 117.3 \\ 170.2 \\ \hline 287.5 \end{array}$$

✓
R.M.

Sta	Dist	Slope	Average Cut	Cu Yds Per Foot	Total Cu Yds	Classification		
						E 50%	L R	S R 50%
20+50								
21	50	1:4	3.0	.49	24.5	12.3		12.2
22	100	1:3	3.0	.50	50	25		25
23	100	1:2	3.0	.50	50	25		25
	40	1:2	3.0	.50	20	10		10
+40	100	Trestle	—	—		25%		75%
24+40	60	1:2	3.0	.50	30	7.5		22.5
25	100	1:2	3.0	.50	50	12.5		37.5
26	115	1:2	3.0	.50	57.5	14.4		43.1
27+15	65	Trestle	—	—				
+80	20	1:2	3.0	.50	10	2.5		7.5
29	90	1:2	3.0	.50	45	11.3		33.7
+90	60	Trestle	—	—				
31+50	80	1:2	3.0	.50	40	10		30
32+30	70	1:3	3.0	.50	35	8.7		26.3
33	100	1:3	3.0	.50	50	12.5		37.5
34	90	1:3	3.0	.50	45	11.3		33.7
+90	60	1:4	3.0	.49	29.4	7.4		22.0
35+50	80	Trestle	—	—				
+80	120	1:3	3.0	.50	60	15		45
37	100	1:3	3.0	.50	50	12.5		37.5
38	50	1:3	3.0	.50	25	6.3		18.7
+50	84	Trestle	—	—				
39+34	71	1:4	3.0	.49	34.8	8.7		26.1
40+05		Trestle	—	—				
+65	35	1:4	3.0	.49	17.1	4.3		12.8
41	110	1:3	3.0	.50	55.0	13.7		41.3
42+10	40	Trestle	—	—				
+50					778.3	430.9		547.4

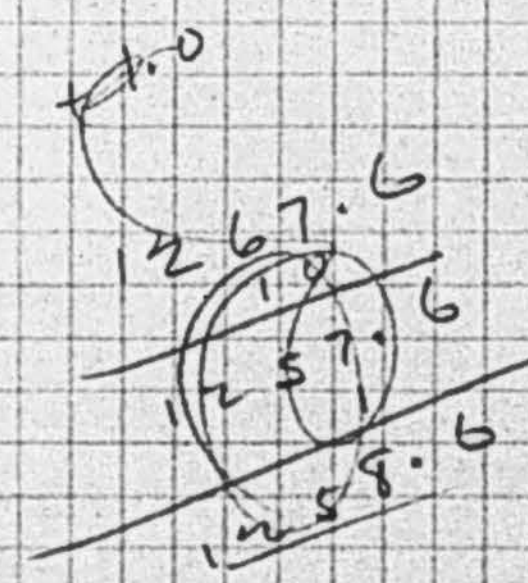
RAM.

Sta	Dist	Slope	Average Cut	Cu Yds per ft	Total Cu Yds	Classification		
						E 50%	L R	S R 50%
42+50	50	1:3	3.0	.50	25	6.2		18.8
43	50	1:2	3.0	.50	25	6.2		18.8
44	65	1:4	3.0	.49	31.8	8.0		23.8
+65	257	Syphon	—	1.0	—			
47+22	108	1:3	3.0	.50	54	13.5		40.5
48+30	20	Trestle	—	—	—			
+50	50	1:3	3.0	.50	25	6.2		18.8
49	100	1:4	3.0	.49	49			49
50	100	1:2	3.0	.50	50			50
51	50	1:2	3.0	.50	25			25
+50	20	Trestle	—	—	—			
52+30	35	1:3	3.0	.50	17.5	4.4		13.1
+85	56	1:2	3.0	.50	28	7		21
53+41	96	Trestle	—	—	—			
54+37	63	1:2	3.0	.50	31.5	7.9		23.6
55	100	1:3	3.0	.50	50	12.5		37.5
56	50	1:3	3.0	.50	25	6.2		18.8
+50	50	1:3	3.0	.50	25			25
57	100	1:2	3.0	.50	50			50
58	25	1:1	4.0	.56	14			14
+25	45	Trestle	—	—	—			
+70	130	1:2	3.0	.50	65			65
60	30	1:1	4.0	.80	24			24
+30	24	Trestle	—	—	—			
+54	19	1:1	4.0	.80	15.2			15.2
+70		Trestle	—	—	—			
61+03	95	1:1	4.0	.80	76			76
62	50	1:2	3.0	.50	25			25
+50	50	1:2	3.0	.50	25			25
63	50	1:1	4.0	.80	40			40
+50					829.0	78.1		750.9

754.9
28.
832.9

RAM.

Sta	Dist	Slope	Average @ Cut	Cu Yds per Foot	Total Cu Yds	Classification		
						E	L R	S R
63+50								100%
64+77	67	Trestle	—	—				
65	83	1:1	4.0	.80	6.64			66.4
66+14	114	1:2	3.0	.50	57.0			57.0
+68	54	Trestle	—	—				
67	32	1:1	4.0	.80	25.6			25.6
68	100	1:1	4.0	.80	8.0			8.0
69	100	1:2	3.0	.50	5.0			5.0
70	100	1:1	4.0	.80	8.0			8.0
+43	43	1:2	4.0	.69	29.7			29.7
71+10	67	1:2	4.0	.69	46.2			46.2
72	90	1:1	4.0	.80	7.2			7.2
73	100	1:1	4.0	.80	8.0			8.0
+50	50	1:1	4.0	.80	4.0			4.0
74	50	1:1	4.0	.80	4.0			4.0
75	100	1:2	3.0	.50	5.0			5.0
+38	38	1:2	3.0	.50	1.9			1.9
77+45	207	Syphon	—	1.0				
78	55	1:4	6.0	1.13	62.2			62.2
79	100	0:0	10.0	3.15	315.0			315.0
80	100	1:3	3.0	.50	5.0			5.0
81	100	1:2	3.0	.50	5.0			5.0
+40	40	Trestle	—	—				
82	60	1:2	3.0	.50	3.0			3.0
83	100	1:2	3.0	.50	5.0			5.0
84	100	1:2	3.0	.50	5.0			5.0
85	100	1:2	3.0	.50	5.0			5.0
86	100	1:2	3.0	.50	5.0			5.0
87	100	1:3	3.0	.50	5.0			5.0
+96	96	1:3	3.0	.50	48.0			48.0
					1541.1			



D.G.M.

Sta	Dist	Slope	Average @ Cut	Cu Yds per Foot	Total Cu Yds	Classification		
						E	L R	S R
87+96								100%
88+26	30	Trestle	—	—				
90	74	1:3	0.0	2.67	19.7			19.7
+33	33	Trestle	—	—				
91	67	1:3	3.0	.50	33.5			33.5
92	100	1:3	3.0	.50	5.0	25.0		37.5
93	100	1:3	3.0	.50	5.0	12.5		37.5
+60	60	1:3	3.0	.50	3.0	7.5		22.5
94+04	44	Trestle	—	—				
95	06	1:3	3.0	.50	48.0	12.0		36.0
+80	80	1:3	3.0	.50	4.0	10.0		30.0
96	20	Trestle	—	—				
97	100	1:3	3.0	.50	5.0	12.5		37.5
98	100	1:3	3.0	.50	5.0	12.5		37.5
99	100	1:4	3.0	.49	4.9	12.2		36.8
100	100	1:4	3.0	.49	4.9	12.2		36.8
101	100	1:4	3.0	.49	4.9	12.2		36.8
102	100	1:4	3.0	.49	4.9	12.2		36.8
103	100	1:4	3.0	.49	4.9	12.2		36.8
104+0	118	1:4	3.0	.49	5.78	14.4		43.4
105+18	162	Syphon	—	1.0				
106+80	20	1:3	3.0	.50	10.0	5.0		5.0
107	100	1:3	3.0	.50	5.0	25.0		25.0
108	100	1:3	3.0	.50	5.0	25.0		25.0
109	100	1:3	3.0	.50	5.0	25.0		25.0
110	100	1:2	3.0	.50	5.0	25.0		25.0
111	100	1:3	3.0	.50	5.0	25.0		25.0
112	100	1:3	3.0	.50	5.0	25.0		25.0
113	100	1:3	3.0	.50	5.0	25.0		25.0
114	100	1:3	3.0	.50	5.0	25.0		25.0
					1083.0	347.1	735.9	

1148
30
1098

752.2
347.6
1099.8

D.G.M.

Sta.	Dist.	Slope	Av. $\frac{E}{Cut}$	Cu Yds per Foot	Total Cu. Yds	Classification		
						F	LR	SR
14								
+50	50	Fill						
115	50	1:3	3.0	.50	25.	12.5		12.5
16	100	1:4	3.0	.49	49.	24.5		24.5
17	100	1:4	3.0	.49	49.	24.5		24.5
18	100	1:3	3.0	.50	50.	25.		25.
19	50	1:3	3.0	.50	25.	12.5		12.5
+50	32	Trestle		-	-			
+82	18	1:3	3.0	.50	9.0	4.5		4.5
120	100	1:2	3.0	.50	50.	25.		25.
21	100	1:2	3.0	.50	50.	25.		25.
22	50	Trestle		-	-			
22+50	50	1:2	3.0	.50	25.	12.5		12.5
23	100	1:2	3.0	.50	50.	25.		25.
24	100	1:2	3.0	.50	50.	25.		25.
25	100	1:2	3.0	.50	50.	25.		25.
26	100	1:2	3.0	.50	50.	25.		25.
27	100	1:2	3.0	.50	50.	25.		25.
28	100	1:3	3.0	.50	50.	25.		25.
29	100	1:3	3.0	.50	50.	25.		25.
30	100	1:3	3.0	.50	50.	25.		25.
31	100	1:3	3.0	.50	50.	25.		25.
32	100	1:3	3.0	.50	50.	25.		25.
33	100	1:3	3.0	.50	50.	25.		25.
34	100	1:3	3.0	.50	50.	25.		25.
35	100	1:3	3.0	.50	50.	25.		25.
36	100	1:3	3.0	.50	50.	25.		25.
37	100	1:4	3.0	.49	49.	24.5		24.5
38	100	1:4	3.0	.49	49.	24.5		24.5
139					1179.0	589.5		589.5

24' Culvert

D.A.M.

Sta	Dist	Slope	Av $\frac{E}{Cut}$	Cu Yds per ft	Total Cu Yds	Classification		
						F	LR	SR
139								
140	100	1:4	3.0	.49	49.	24.5		24.5
41	100	0:0	3.0	.56	56.	28.		28.
42	100	0:0	3.0	.56	56.	28.		28.
43	100	0:0	3.0	.56	56.	28.		28.
44	100	1:4	3.0	.49	49.	24.5		24.5
45+09	109	1:3	3.0	.50	54.5	27.2		27.3
+59	50	Trestle		-	-			
+59	41	1:3	3.0	.50	20.5	10.2		10.3
146	100	1:3	3.0	.50	50.	25.		25.
47	100	1:3	3.0	.50	50.	25.		25.
48	100	1:3	3.0	.50	50.	25.		25.
49	100	1:3	3.0	.50	50.	25.		25.
50	100	1:3	3.0	.50	50.	25.		25.
51	50	1:3	3.0	.50	25.	12.5		12.5
51+50	32	Trestle		-	-			
+82	118	1:3	3.0	.50	59.0	29.5		29.5
153	100	1:4	3.0	.49	49.	24.5		24.5
54	100	1:4	3.0	.49	49.	24.5		24.5
55	100	1:4	3.0	.49	49.	24.5		24.5
6	100	1:4	3.0	.49	49.	24.5		24.5
7	100	1:4	3.0	.49	49.	24.5		24.5
8	100	1:4	3.0	.49	49.	24.5		24.5
9	100	1:4	3.0	.49	49.	24.5		24.5
160	100	0:0	3.0	.56	56.	28.		28.
1	100	0:0	3.0	.56	56.	28.		28.
2	100	0:0	3.0	.56	56.	28.		28.
3	100	1:3	3.0	.50	50.	25.		25.
4	100	1:3	3.0	.50	50.	25.		25.
5	100	1:3	3.0	.50	50.	25.		25.
6	100	1:3	3.0	.50	50.	25.		25.
					1336.0	667.9		668.7

D.A.M.

Sta	Dist	Slope	Av Cut	Cu Yds per foot	Total Cu Yds	Classification		
						E	L R	SR
166	50	1:3	3.0	.50	2.5	12.5		12.5
+50	50	Trestle		-				
167	100	1:3	3.0	.50	5.0	25		25
8	100	1:3	3.0	.50	5.0	25		25
9	100	1:3	4.0	.69	69	34.5		34.5
70	100	1:3	4.0	.69	69	34.5		34.5
1	100	1:3	4.0	.69	69	34.5		34.5
2	100	1:3	4.0	.69	69	34.5		34.5
3	100	1:3	4.0	.69	69	34.5		34.5
4	100	1:3	4.0	.69	69	34.5		34.5
5	100	1:3	4.0	.69	69	34.5		34.5
6	100	1:3	6.0	1.16	11.6	58		58
7	100	1:3	4.0	.69	69	34.5		34.5
8	100	1:3	4.0	.69	69	34.5		34.5
9	100	1:3	4.0	.69	69	34.5		34.5
180	100	1:3	4.0	.69	69	34.5		34.5
1	100	1:3	4.0	.69	69	34.5		34.5
2	100	1:3	5.0	.92	92	46		46
3	100	1:3	4.0	.69	69	34.5		34.5
40	Bridge			-		<u>100.00</u>		
+40	60	1:3	5.0	.92	552	552		
4	100	1:4	5.0	.92	92	92		92
5	100	0:0	4.0	.80	80	80		80
6	100	0:0	5.0	1.06	106	106		106
7	100	0:0	6.0	1.41	141	141		141
8	100	0:0	6.0	1.41	141	141		141
9	100	0:0	5.0	1.06	106	106		106
190	100	0:0	5.0	1.06	106	106		106
1	100	0:0	5.0	1.06	106	106		106
2	100	0:0	4.0	.80	80	80		80
3								
					2671.0	3090.5		580.5

✓
D.A.M.

Sta	Dist	Slope	Av Cut	Cu Yds per Foot	Total Cu Yds	Classification		
						E	L R	SR
193	100	0:0	3.0	.56	56	56		56
4	100	0:0	3.0	.56	56	56		56
5	100	0:0	3.0	.56	56	56		56
6	100	0:0	3.0	.56	56	56		56
7	100	0:0	3.0	.56	56	56		56
8	100	0:0	3.0	.56	56	56		56
9	100	0:0	3.0	.56	56	56		56
200	100	0:0	3.0	.56	56	56		56
1	100	0:0	4.0	.80	80	80		80
2	100	1:4	4.0	.67	67	67		67
3	100	1:4	5.0	.88	88	88		88
4	100	1:4	5.0	.88	88	88		88
5	100	1:4	4.0	.67	67	67		67
6	100	1:4	3.0	.49	49	49		49
7	100	1:4	3.0	.49	49	49		49
8	100	1:3	5.0	.92	92	92		92
9	100	1:3	5.0	.92	92	92		92
210	100	1:3	5.0	.92	92	92		92
11	100	1:3	5.0	.92	92	92		92
12	100	1:3	4.0	.69	69	69		69
13	100	1:3	4.0	.69	69	69		69
14	132	1:3	4.0	.69	91	91		91
15+32	1050	siphon		1.0	1050.0	1050		
225+82	118	0:0	8.0	2.22	261.9	261.9		
7	100	0:0	10.0	3.15	315			315
8	82	0:0	10.0	3.15	258.3			258.3
229+82								
=								
232+98	416	Equation						
234	102	0:0	3.0	.56	57.1	57.1		57.1
					3571.3	2938.0		573.3

Adobe

✓
D.A.M.

Sta	Dist	Slope	Av Cut	Cu Yds per fast	Total Cu Yds	Classification		
						E	LR	SR
234						Adobe		
5	100	0:0	3.0	.56	56.	56		
6	100	0:0	3.0	.56	56.	56		
7	100	0:0	3.0	.56	56.	56		
8	100	0:0	4.0	.80	80.	80		
9	100	0:0	4.0	.80	80.	80		
240	100	0:0	4.0	.80	80.	80		
1	100	0:0	3.0	.56	56.	56		
2	100	0:0	6.0	1.41	141.	141		
3	100	0:0	8.0	2.22	222.	222		
4	100	0:0	9.0	2.67	267.	267		
5	100	0:0	10.0	3.15	315.	315		
6	100	0:0	12.0	4.23	423	423		
7	100	0:0	12.0	4.23	423	423		
8	100	0:0	10.0	3.15	315.	315		
9	100	0:0	9.0	2.67	267.	267		
250	100	0:0	7.0	1.85	185.	185		
1	100	0:0	5.0	1.06	106.	106		
					<u>3128.</u>	3128		



✓
S.A.M.

Concrete Pipe 20.5"	Open Conduit	Covered Conduit	Steel Cond. + Trestle	Low Trestle	Syphon
	.500 ✓		.55 ✓	.65 ✓	.257 ✓
	.554 ✓	.290 ✓	.48 ✓	.30 ✓	.213 ✓
	.410 ✓	.275 ✓	.86 ✓	.84 ✓	.162 ✓
	.64 ✓	.210 ✓	.130 ✓	.40 ✓	.1048 ✓
	1.00	.80 ✓	.100 ✓	.20 ✓	<u>1680</u>
	.260 ✓	1.00 .60	.160 ✓	.80 ✓	205
	.150 ✓	.120 ✓	.60 ✓	.55 ✓	
	.108 ✓	.71 ✓	.96 ✓	50 45	<u>1885</u>
	.188 ✓	.145 ✓	.67 ✓	.24 ✓	2
	.349 ✓	.215 ✓	.54 ✓	25 32?	<u>1887</u>
	.447 ✓	.300 ✓	.49 ✓	.30 ✓	
174	.174 ✓	.56 ✓	.33 ✓	.20 ✓	
	.327 ✓	.213 ✓	.44 ✓	.32 ✓	
	.176 ✓	.175 ✓	.50 ✓	.50 ✓	
	.018 ✓	.140 ✓	.32 ✓	.50 ✓	
	.1270 ✓	24 14?	<u>1064</u> ✓	.40 ✓	
	.218 ✓	.197 ✓		<u>695</u>	
	.2259 ✓	.245 ✓			
	.659 ✓	.197 ✓	1064 ✓		
x	.6192 ✓	.682 ✓			
	<u>1802</u>	3755			
	17225	60 +			
	x 302				

2520 / 17525
416
17109

205
17525
3770
1064
697
1680
24941
68x
257

17525
3770
257
3513
17109
416
17525
1680

65
84
80
55
100
+ 384
1064
1448
218
6192
302
1802
8514
17525
9011

14	14	132	113	4.0	.69	9.1	9.1
15+32	15+32	68			1.00	68	
16	16	100				100	
17	17	100				100	
18	18	100				100	
19	19	100				100	
20	20	100				100	
21	21	100				100	
22	22	100				100	
23	23	100				100	
24	24	100				100	
25	25	82				82	

Syphon

968
1950
1960
1530
302
1802.4
8512.4
24537.2
1172
36257
245.9
242.27
15911
16050
16961

242.18
4090
1.28

~~415.4~~

415.8

~~228+82~~
~~232+87.6~~
4
15.6

415.6
1172.0
1587.6

4612
14945

12
10100
415.6
9684.4
3
290532
1172
3077

10100
1587.6
8512.4
3
255492
1172
3726

245.90
242.823

245.90
242.174
180

122
1050
1172 @ 1 = 1.172
3.03
4.20
245.9
241.7

242.18
242.174

AVENUE.

C. 125		Tract		D		Tract		E		Tract		F		Tract.		G.		
50	A	50	A	60	A	50	A	50	A	50	A	50	A	50	A	50	A	50
	B		B		B		B		B		B		B		B		B	
	C		C		C		C		C		C		C		C		C	
	D		D		D		D		D		D		D		D		D	
5	10.	11.	E	12.	E	13.	E	14.	E	15.	E	16.	E	17.	E	18.	E	
	F		F		F		F		F		F		F		F		F	
	G		G		G		G		G		G		G		G		G	
	H		H		H		H		H		H		H		H		H	
	I		I		I		I		I		I		I		I		I	
50	J	50	J	50	J	50	J	50	J	50	J	50	J	50	J	50	J	50
73	K	73	K	73	K	73	K	73	K	73	K	73	K	73	K	73	K	73
125		125		125		125		125		125		125		125		125		125

10. STREET

11. E 12. STREET

13. E 14. STREET

15. E 16. STREET

17. E 18. STREET

AVENUE

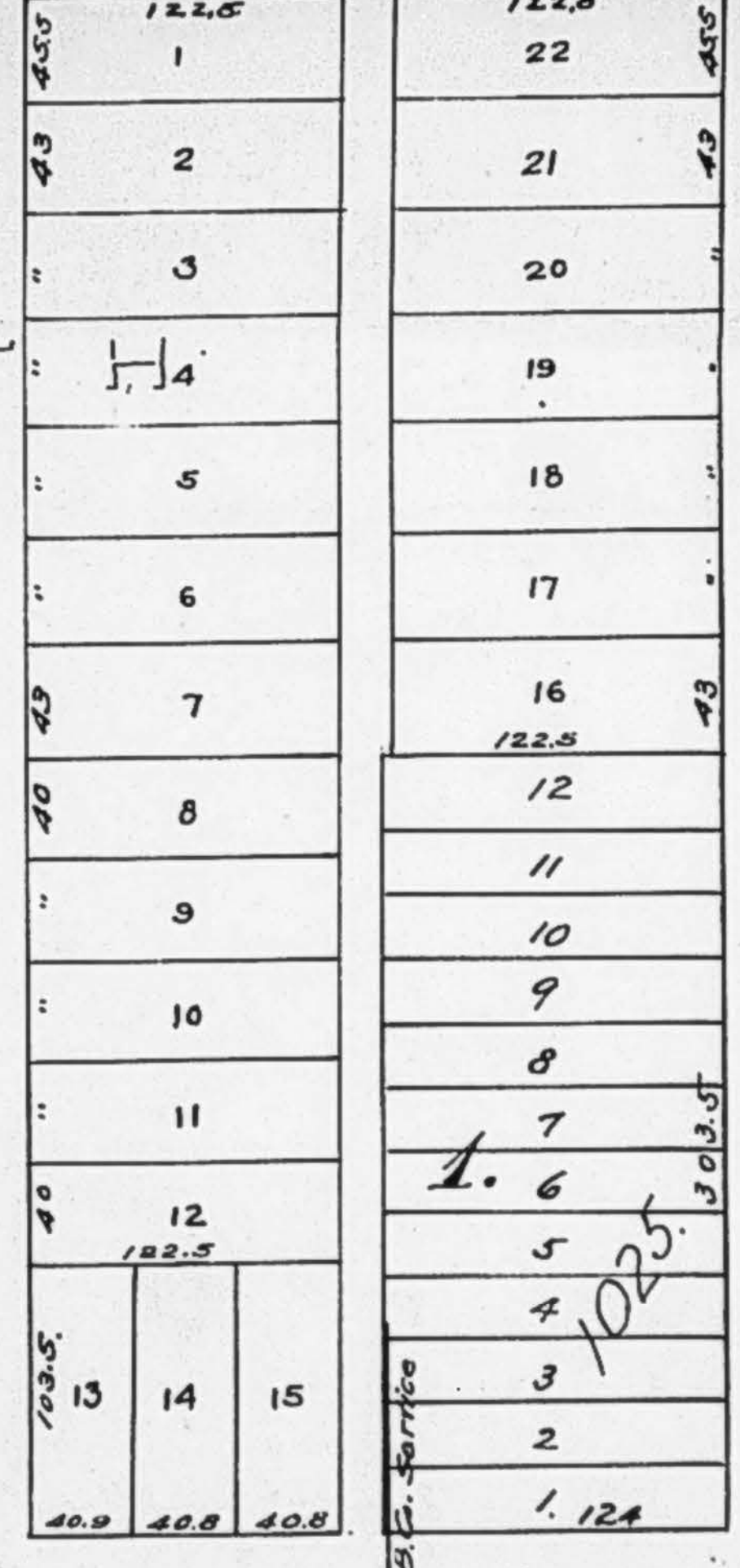
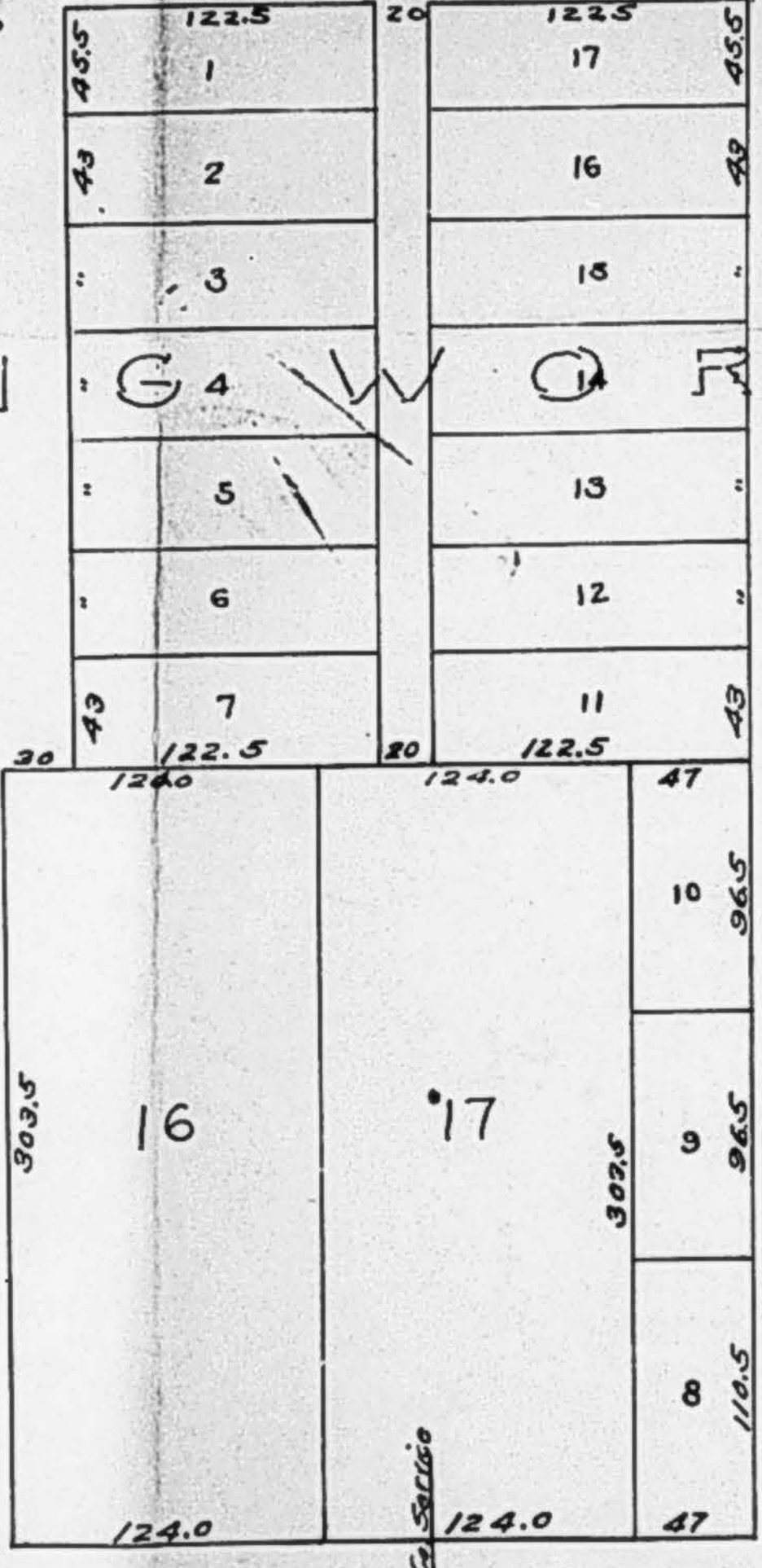
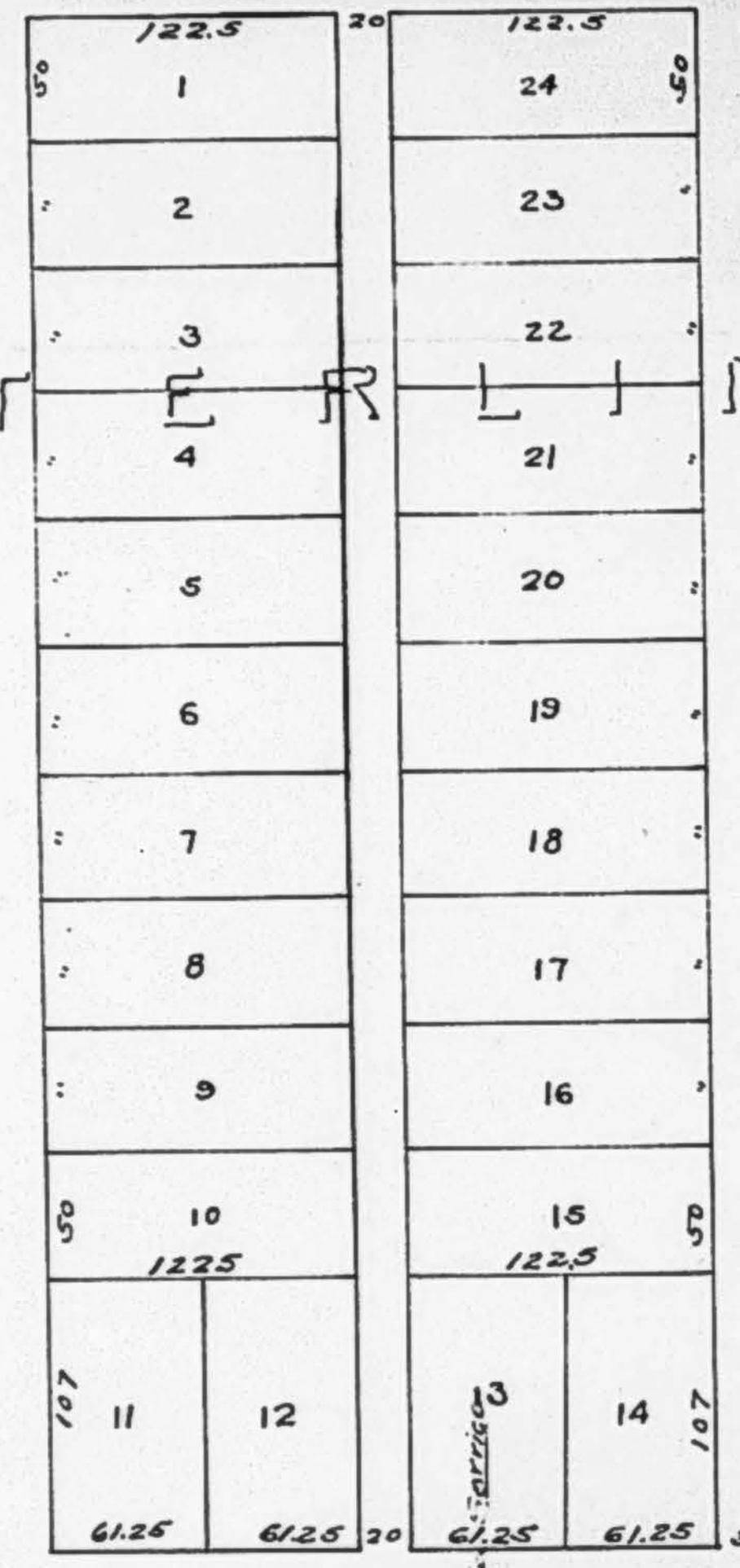
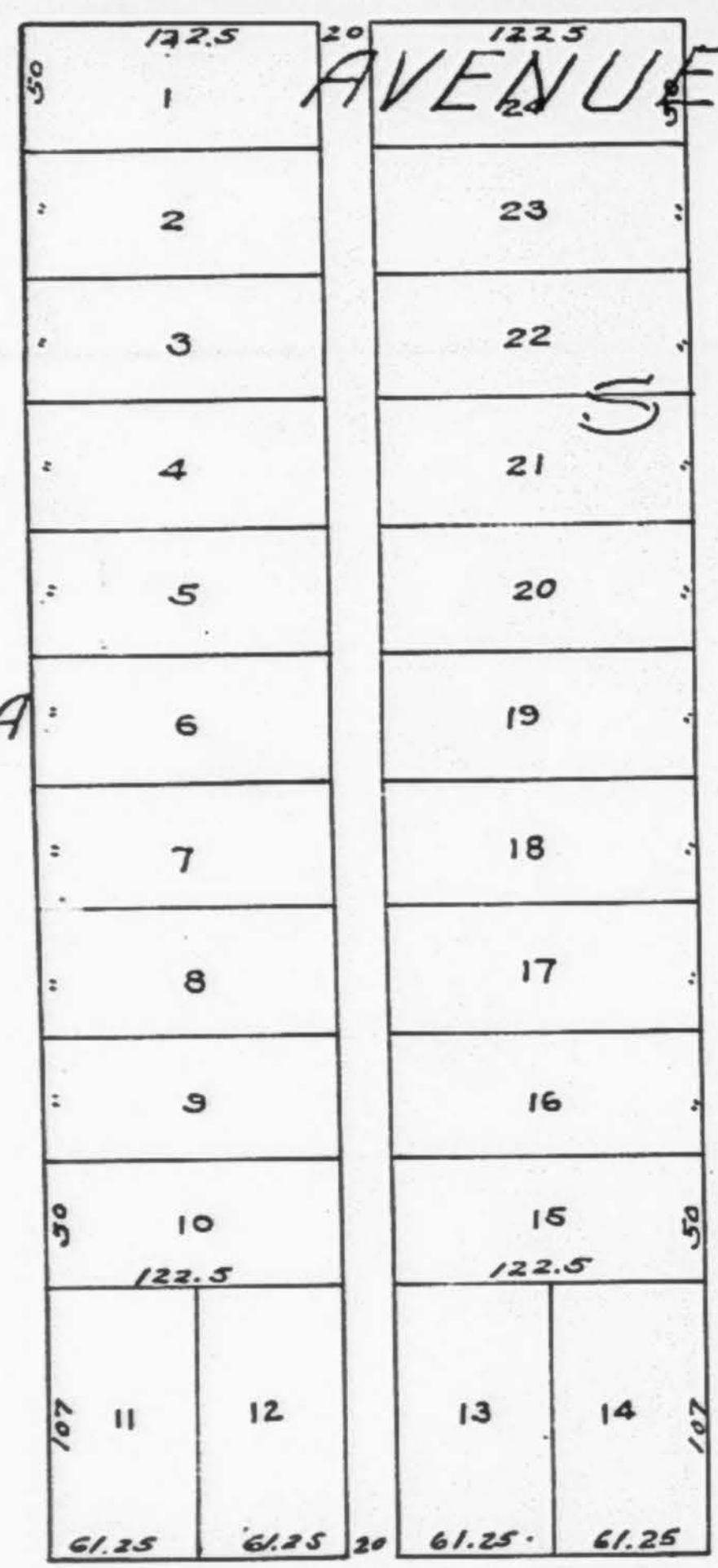
STREET

50	1	20	122.5	60	1	20	122.5	60	1	20	122.5	60	1	20	122.5	60	1	20	122.5
	2		23		2		23		2		23		2		23		2		23
	3		22		3		22		3		22		3		22		3		22

AVENUE

S T E R L I N G W O R T H

2^D STREET



AVENUE

Scale: 1" = 100'

F. B. No 88

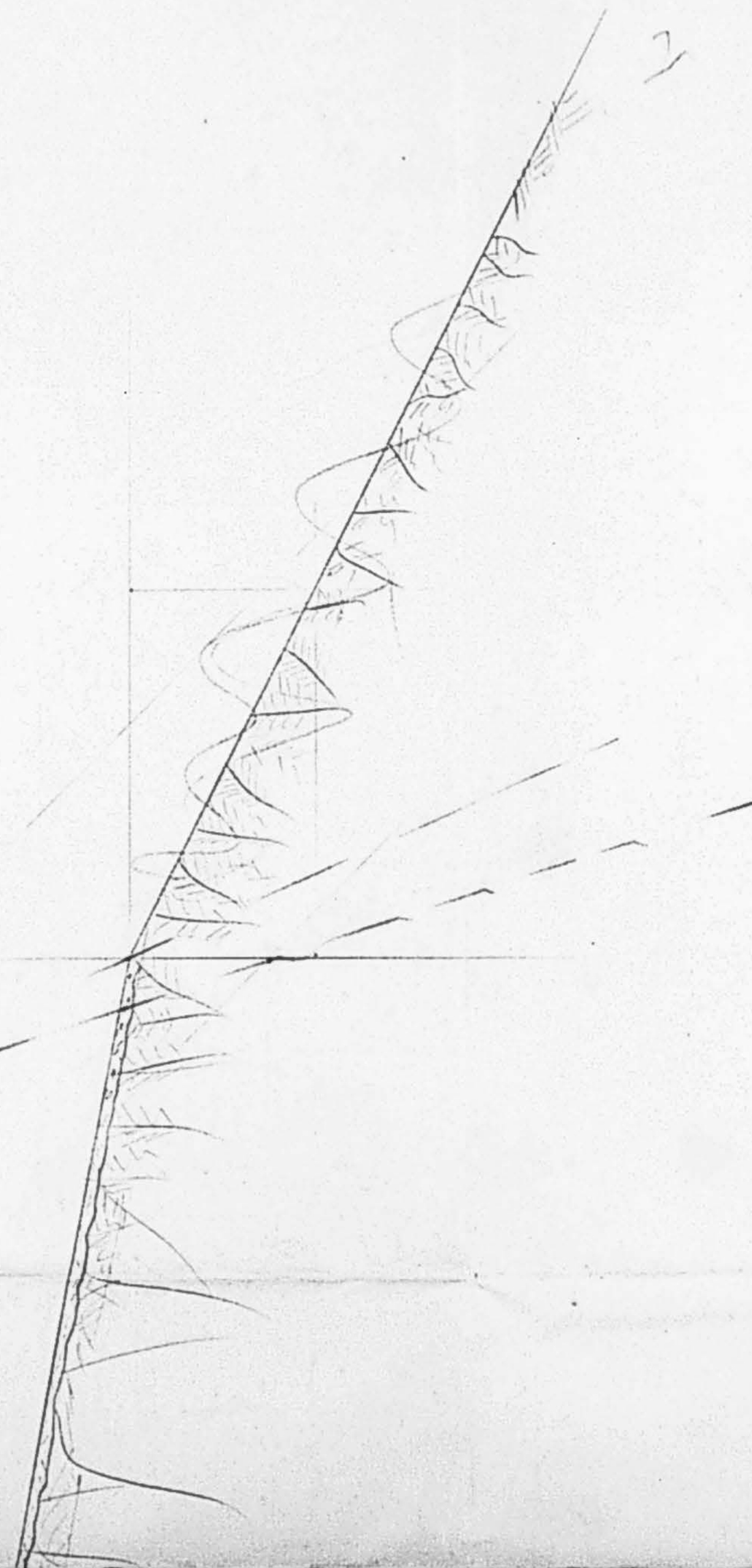
SEC. 30
N² of NE⁴
T.16.S - R.2.W.

CORRECTED DEC. 1st 1912 J.P.M.
March 26th 1913 Ed. A. Burt
Corrected to Sept. 2nd 1913 P.A.M.
" Mar. 23rd 1914 R.M.T.

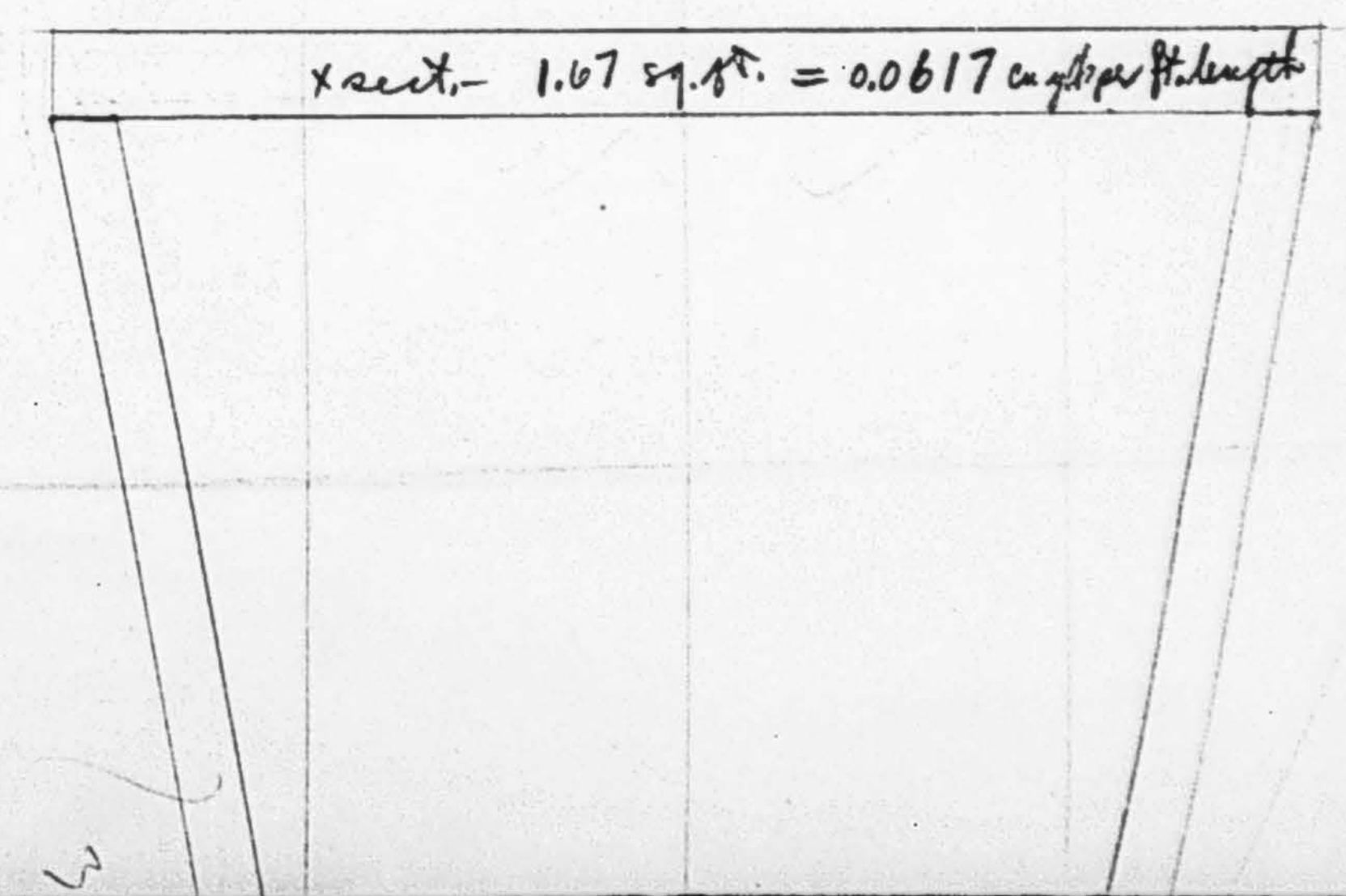
2.H.



3

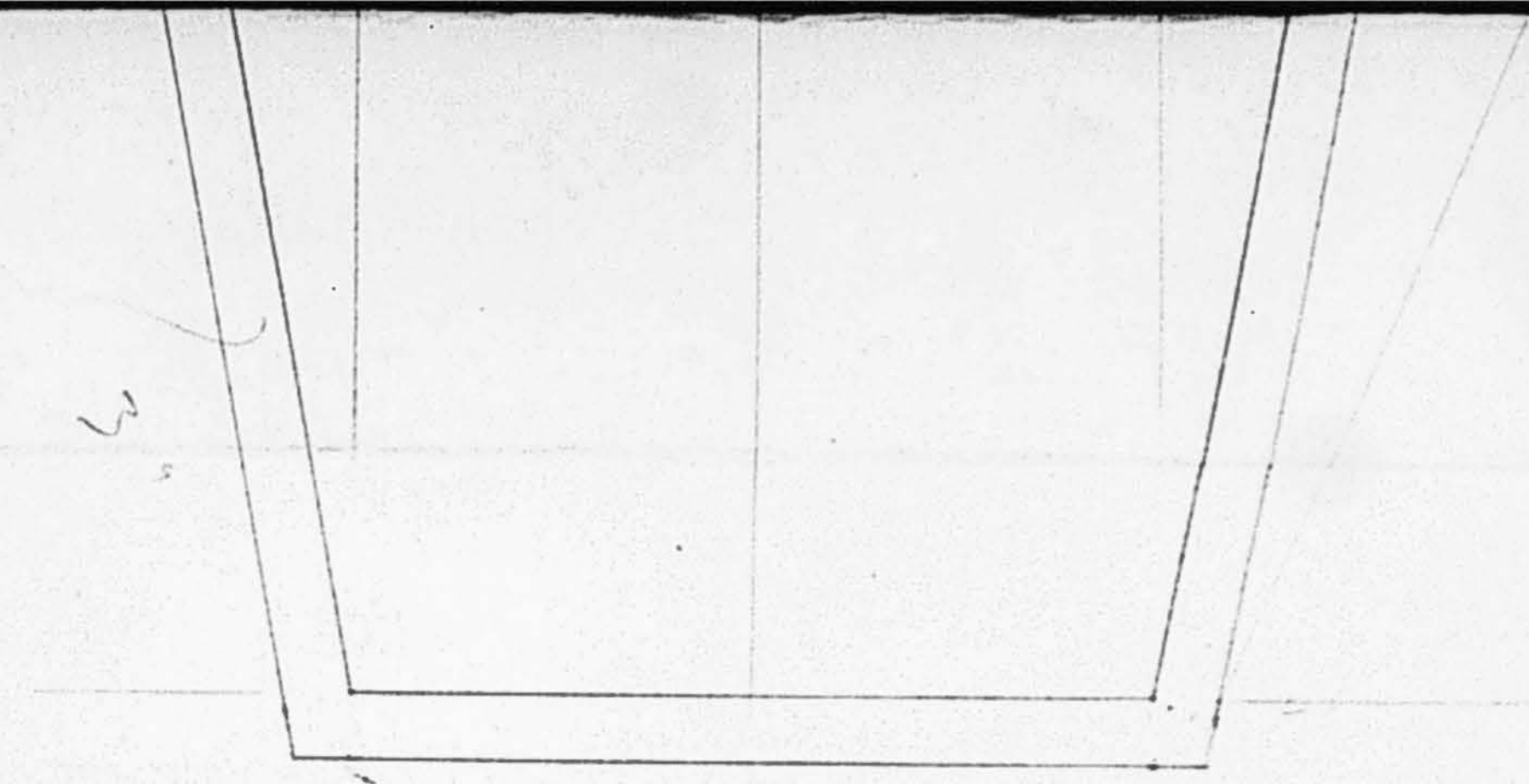


2



x sect. - 1.67 sq. ft. = 0.0617 cu ft per ft. length

3



xsect area conc. = 2.9 sq. ft. = 0.1074 cu. yds. per foot length
 Inside surface area per foot length = 11.15 sq. ft.

0.1074
 0.0617

 0.1791

1" - 1"

MONROE

STREET

113.5	17	3	125
1	4	100	25
92.1	5		
2	6		
68.75	7	100	
8			
9			
10			
11			
12			
13			
14			
15			
16			
17			
18			
19			
20			
21			
22			
23			
24			

25	1	125	15	125	18	25
2					47	
3					46	
4					45	
5					44	
6					43	
7					42	
8					41	
9					40	
10					39	
11					38	
12					37	
13					36	
14					35	
15					34	
16					33	
17					32	
18					31	
19					30	
20					29	
21					28	
22					27	
23					26	
24		125			25	125

25	1	125	125	48	25
2				47	
3				46	
4				45	
5				44	
6				43	
7				42	
8				41	
9				40	
10				39	
11				38	
12				37	
13				36	
14				35	
15				34	
16				33	
17				32	
18				31	
19				30	
20				29	
21				28	
22				27	
23				26	
24		125		25	25

40	130	Tract B
36.6		A
25		B
		C
		D
		E
		F
		G
		H
		I
		J
		K
		L
		M
		N
		O
		P
		Q
		R
		S
		T
		U
		V

36.6	130	Tract
36.6		A
25		B
		C
		D
		E
		F
		G
		H
		I
		J
		K
		L
		M
		N
		O
		P
		Q
		R
		S
		T
		U
		V

75	1	1217	25
	2		
	3		
	4		
	5		

1	23
2	22

12	OLIVE
11	

BOUNDARY

BIK A *Arata*

1	121.7
2	
3	
4	
5	
6	
7	TH
8	
9	3A
10	3A
11	
12	
13	
14	
15	
16	
17	4
18	121.7

92.2
152.87
24
92.2

80.8				
23	22	21	20	19
25				25

18' Wood Spars
12' aband.

Meter Box
Meter House
Two Meters

1	23
2	22
3	21
4	20
5	19
6	18
7	17
8	16
9	15
10	
11	
12	
13	
14	

Stacking of Boillot Sub.

MAP

35 TH

63'
83' 0" E
100% 1913
37'
83' 3"

12 OLIVE		
11		
10		
9	8	9
8		
7		
6		
5		
4		
3	18	19
2		
1		

1445

A

TER

1094' New 3" 100% 1913

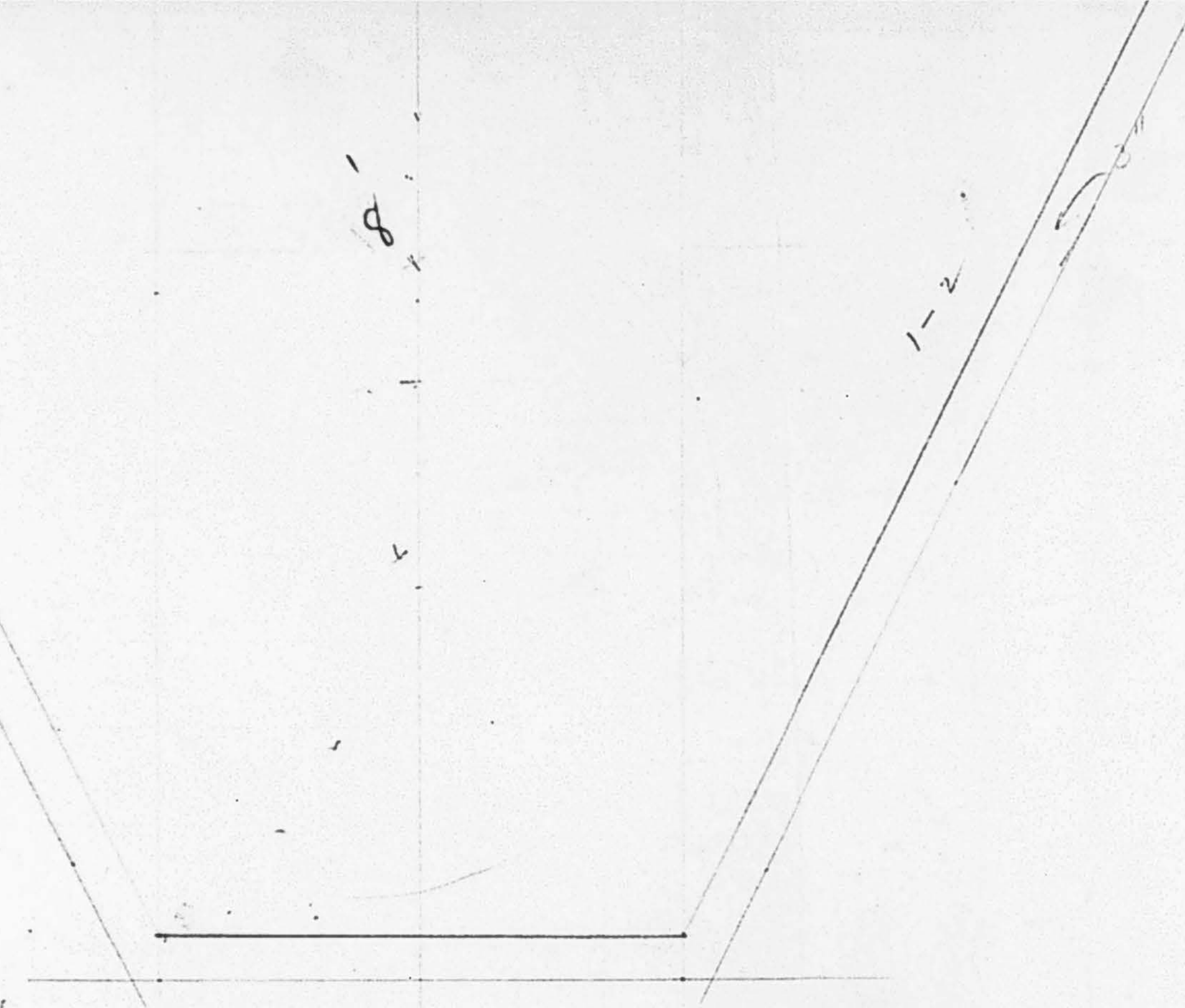
CAJON

1" - 1

3 feet

8'

1-2



$$8.25 \times \frac{17.93}{2} = 62.55$$

$$8.00 \times \frac{14}{2} = 56.00$$

$$\begin{array}{r} 62.55 \\ \underline{56.00} \\ 6.55 \end{array}$$

x sect area = 6.55 sq. ft. = 0.228 cu yds. per foot length.

Inside surface area per foot length - 20.88 sq. ft.

CARROLL CONDUIT - TYPES OF CONSTRUCTION

<u>Station</u>	<u>Grades</u>	<u>Syphon</u>	<u>Open Conduit</u>	<u>Steel Flume</u>	<u>Covered Conduit</u>
0+00 = 254.00	42" Pipe	265			
2+65	Open Conduit		450		
7+15	Steel Flume			15	
7+30	Open Conduit		42		
7+72	Steel Flume			105	
8+77	Open Conduit		581		
14+58	Steel Flume			180	
16+38	Open Conduit		717		
23+55	Steel Flume			60	
24+15	Open Conduit		318		
27+33	Steel Flume			15	
27+48	Open Conduit		232		
29+80	Steel Flume			15	
29+95	Open Conduit		95		
30+90	Steel Flume			30	
31+20	Open conduit		428		
35+48	Steel Flume			15	
35+63	Open conduit		242		
38+05	Steel Flume			15	
38+20	Open conduit		58.94		
38+63	Steel Flume			30	
38+93	Open conduit		73		
39+66	Steel Flume			75	
40+41	Open conduit		124		
41+65	Steel Flume			30	
41+95					

<u>Station</u>	<u>Grades</u>	<u>Syphon</u>	<u>Open Conduit</u>	<u>Steel Flume</u>	<u>Covered Conduit</u>
41+95	251.6377				
42+64	251.6065		69		
42+79	251.5915			15	
43+95	251.5393		116		
46+60	251.2743	265+			
47+36	251.2401		76		
47+51	251.2251			15	
48+90	251.1626		139		
52+05	250.8477	315+			
53+00	250.8048		95		
55+05	250.7126				205
55+50	250.6676			45	
57+10	250.5956				160
57+25	250.5806			15	
57+55	250.5671				30
57+70	250.5521			15	
60+39.35	250.4309				269.35
60+97	250.3709			60	
61+18	250.3614				21
61+63	250.3164			45	
62+85	250.2615				122
63+45	250.2015			60	
71+38	249.8447				793
73+60	249.6227	222+			
77+03	249.4683		343		
77+42	249.4293			39	
83+88	249.1386		646		

<u>Station</u>	<u>Grades</u>	<u>Syphon</u>	<u>Open Conduit</u>	<u>Steel Flume</u>	<u>Covered Conduit</u>
✓ 83+88	249.1386 Steel Flume			15	
✓ 84+03	249.1236 Open conduit		169		
✓ 85+72	249.0476 Steel Flume			39	
✓ 86+11	249.0086 Open conduit		326		
✓ 89+37	248.8619 Steel flume			30	
✓ 89+67	248.8319 Open conduit		195		
✓ 91+62	248.7441 Steel Flume			15	
✓ 91+77	248.7291 Open conduit		893		
✓ 100+70	248.3273 42" Pipe (or 173 slope)	168+			
✓ 102+38	248.1593 Open conduit		738		
✓ 109+76	247.8272 Steel Flume			15	
✓ 109+91	247.8122 Open conduit		452		
✓ 114+43	247.6088 Steel Flume			30	
✓ 114+73	247.5788 Open conduit		204		
✓ 116+77	247.4870 Steel Flume			60	
✓ 117+37	247.4270 Open Conduit		2213		
✓ 139+50	246.4311 42" Pipe	40			
✓ 139+90	246.3911 Open conduit		635		
✓ 146+25	246.1054 42" Pipe	60			
✓ 146+85	246.0453 Open conduit		315		
✓ 150+00	245.9036 Open conduit		1210		
✓ 162+10	245.5406 42" pipe	30			
✓ 162+40	245.5106 open conduit		1605		
✓ 178+45	245.0291 42" pipe	35			
✓ 178+80	244.9941 Open conduit		1357		
✓ 192+37	244.5870				

<u>Station</u>	<u>Grades</u>	<u>Syphon</u>	<u>Open Conduit</u>	<u>Steel Flume</u>	<u>Covered Conduit</u>
192+37	244.5870 42" pipe (or 134 slope)	133			
193+70	244.4540 Open conduit		1710		
210+80	243.9410 42" pipe (or 1068 slope)	1060			
221+40	242.8810 Open conduit		150		
222+90	242.8360 42" pipe (or 566 slope)	555			
228+45	242.2810 Open conduit		1606		
244+51					
		<hr/>	<hr/>	<hr/>	<hr/>
		3148	18,622.94	1098	1600.35

TABULATION SHOWING LENGTHS AND NUMBER OF STEEL BARS ORDERED BY
CONTRACTORS FOR EACH UNIT OF TRESTLE.

<u>Unit No. 1-B</u>			
2	pieces	1/2 x 15' 0"	= 30' 0"
2	"	1/2 x 18' 0"	= 36' 0"
4	"	1/2 x 4' 0"	= 16' 0"
4	"	1/2 x 1' 0"	= 4' 0"
Total Length -----			86' 0"
Total Number of Units ---			36

<u>Unit No. 2</u>			
2	pieces	1/2 x 14' 0"	= 28' 0"
2	"	1/2 x 16' 0"	= 32' 0"
4	"	1/2 x 4' 0"	= 16' 0"
4	"	1/2 x 1' 0"	= 4' 0"
Total Length -----			80' 0"
Total Number of Units ---			27

<u>Unit No. 3</u>			
2	pieces	1/2 x 15' 6"	= 31' 0"
2	"	1/2 x 17' 6"	= 35' 0"
4	"	1/2 x 4' 0"	= 16' 0"
4	"	1/2 x 1' 0"	= 4' 0"
Total Length -----			86' 0"
Total Number of Units ---			14

<u>Unit No. 4</u>			
2	pieces	1/2 x 17' 0"	= 34' 0"
2	"	1/2 x 19' 0"	= 38' 0"
4	"	1/2 x 4' 0"	= 16' 0"
4	"	1/2 x 1' 0"	= 4' 0"
Total Length -----			92' 0"
Total Number of Units --			5

Unit No. 5.

2	pieces	1/2 x 18' 0"	= 36' 0"
2	"	1/2 x 20' 0"	= 40' 0"
4	"	1/2 x 4' 0"	= 16' 0"
4	"	1/2 x 1' 0"	= 4' 0"
Total Length -----			96' 0"
Total Number of Units ---			4

Unit No. 6

2	pieces	1/2 x 19' 6"	= 39' 0"
2	"	1/2 x 21' 6"	= 43' 0"
4	"	1/2 x 4' 0"	= 16' 0"
4	"	1/2 x 1' 0"	= 4' 0"
Total Length -----			102' 0"
Total Number of Units ---			2

Unit No. 7

2	pieces	1/2 x 21' 0"	= 42' 0"
2	"	1/2 x 23' 0"	= 46' 0"
4	"	1/2 x 4' 0"	= 16' 0"
4	"	1/2 x 1' 0"	= 4' 0"
Total Length -----			108' 0"
Total Number of Units ---			2

Cradle

2	hairpin pos	1/2 x 8' 6"	= 17' 0"
2	"	1/2 x 13' 6"	= 27' 0"
1	"	1/2 x 8' 3"	= 8' 3"
1	"	1/2 x 9' 4"	= 9' 4"
2	"	1/2 x 5' 4"	= 10' 8"
2	"	1/2 x 1' 9"	= 1' 6"
2	"	1/2 x 1' 0"	= 2' 0"

Total Length -----			75' 9"
Total Number of Cradles ---			102

Girders

2	pieces	1/2 x 14' 11"	= 29' 10"
2	"	1/2 x 15' 9"	= 31' 6"
1	"	1/2 x 9' 0"	= 9' 0"

Total Length -----			69' 6"
Total Number of Girders -			180

<u>Braces</u>	4 pieces 1/2 x 4' 11" =	19' 8"
	Total Number of Braces ---	288
<u>Struts</u>	1 piece 1/2 x 14' 6" =	14' 6"
	2 " 1/2 x 15' 6" =	31' 0"
	Total Length -----	45' 6"
	Total Number of Struts --	24
<u>Cross-ties</u>	2 pieces 3/8" x 6' 1" round	12' 2"
	Total Number of Cross-ties --	760
<u>Slabs</u>	9 pieces 3/8 x 2' 10" round	25' 6"
	Total Number of Slabs -----	97
<u>Top Slat of Covered Conduit</u>		
	4,800 pcs 3/8" x 6' 0" round	28,800 ft.

VOLCAN LAND AND WATER COMPANY

A Comparison of Alternate Routes for Delivering Water to the City of San Diego.

Route No. 1: Via: Carroll Pumping Plant and Pipe Line.

This route presumes the construction of Warner Dam, Warner Conduit, Carroll Dam, Darroll Pumping plant and Carroll-University Pipe line. The waters of the San Luis Rey will be impounded by Warner Dam and diverted by means of the Warner Conduit into the watershed of the Santa Ysabel River, flowing in the natural channel of the Santa Ysabel until impounded by the Carroll Dam. At this point the water will be pumped three hundred feet and then delivered through a gravity pipe line to the reservoir of the City of San Diego at University Heights. This system will deliver ten million gallons per day.

The estimated construction cost is as follows:

Warner Dam - 85 ft. high -----	\$ 249,766.00
Warner Conduit - 6.3 miles -----	536,969.00
Carroll Dam - 90 ft. high -----	265,006.00
Carroll Pumping Plant -----	59,735.00
Carroll-University Pipe Line 21 1/4 miles ----	603,188.00

Total Estimated Construction Cost ----- \$1,514,664.00

Estimated Operating Costs

Interest -----	\$ 116,394.00
Depreciation -----	30,386.00
Taxes -----	18,184.00
Maintenance -----	34,000.00
Carroll Pumping Plant (fuel, labor, fixed chgs) -----	41,551.00

Total Operating Cost per Year ----- \$ 240,515.00

This will deliver 10 million gallons per day at
6.6¢ per 1,000 gallons.

Route No. 2: Via: Pamo Conduit and San Clemente Reservoir.

This route presumes the diversion of the water of the San Luis Rey River by means of the Warner Dam and Conduit, into the channel of the Santa Ysabel River, where it will flow until diverted by a small dam into the Pamo Conduit. The Pamo Conduit will convey the water to the San Clemente Dam from whence it will be conducted by means of a gravity pipe line to the University Heights Reservoir. This system will deliver 13½ million gallons per day.

The estimated cost follows:

Warner Dam - 85 ft. high -----	\$ 249,766.00
Warner Conduit - 6.3 miles -----	336,969.00
Pamo Diversion Dam -----	5,000.00
Pamo Conduit - 26.1 miles -----	1,073,400.00
San Clemente Dam - 20 ft. high -----	12,650.00
San Clemente-University Pipe Line 10.7 miles -----	<u>202,004.00</u>

Estimated total cost ----- \$1,879,789.00

Estimated Operating Costs.

Interest -----	\$ 149,823.00
Taxes -----	23,410.00
Maintenance -----	42,000.00
Depreciation -----	<u>29,828.00</u>

Estimated Total Annual Operating Cost --\$ 245,071.00
Estimated Daily Operating Cost -----\$ 672.00

OR

5¢ per 1,000 gallons.

Route No. 3: Via: Pamo Dam, Pamo Conduit and San Clemente Reservoir

This route presumes the diversion of the water of the San Luis Rey River, by means of Warner Dam and Conduit into the channel of the Santa Ysabel River, along which it will flow until impounded by the Pamo Dam. From this point the water will be conveyed through the Pamo Conduit to the San Clemente Reservoir and thence through a gravity pipe line to the University Heights Reservoir. This system will deliver 16 million gallons daily.

The estimated cost follows:

Warner Dam - 85 ft. high -----	\$ 249,766.00
Warner Conduit - 6.3 miles -----	336,969.00
Pamo Dam - 160 ft. high -----	425,000.00
Pamo Conduit - 24.8 miles -----	1,048,900.00
San Clemente Dam - 20 ft. high -----	12,650.00
San Clemente-University Pipe line - 10.7 miles -----	<u>340,149.00</u>

Estimated Total Cost ----- \$2,413,434.00
=====

Estimated Operating Cost

Interest -----	\$ 193,075.00
Taxes -----	30,200.00
Maintenance -----	45,000.00
Depreciation -----	<u>36,828.00</u>

Estimated Total Annual Operating Cost \$ 305,103.00
Estimated Daily Operating Cost -----\$ 836.00

OR

5½¢ per 1,000 gallons.

COMPARISON

	<u>Route No. 1.</u>	<u>Route No. 2.</u>	<u>Route No. 3.</u>
Delivery in Million Gallons per day -----	10	13½	16
Estimated Construction cost -----	\$1,514,664.00	\$1,879,789.00	\$2,413,434.00
Estimated Annual Operating Cost ---	\$ 240,515.00	\$ 245,071.00	\$ 305,103.00
Cost per thousand gallons -----	6.6¢	5¢	5½¢

It should be noted that the above costs do not include the cost of lands and water rights.

C. E. Hickok.

(47-A)

GENERAL ESTIMATE OF CONDUIT.

Excavation	16991.4	Cu. Yds. Solid Rock @ \$2.00 =	\$33982.80
	3782.9	" " Loose " " 1.00 -	3782.90
	.3782.9	" " Earth " .40 -	1513.16
			<u>39278.86</u>
Open Conduit	12194.94	lin. ft. lined 3" Concrete @ 1.35 -	16463.17
		This \$1.35 price based on the bid of \$13.50 per cu. yd.	
Covered Conduit	1600.35	lin. ft. @ \$1.35 + 1.88-3.23 -	5169.13
		This \$1.88 price based on concrete at \$22.50 per cu. yd.	
42" Reinforced Concrete Pipe	3148.	lin. ft. @ \$5.00 -	15740.00
Trestle supporting siphon	279.	lin. ft. @ \$3.75 -	1046.25
Steel Flume on Concrete Trestle - Trestle including		footings \$3.75	
		Flume 3.04	
		Freight .08	
Steel Flume 1098 lineal feet @		<u>6.87</u> -	7543.26
Inlet & outlet boxes - 12.75 cu. yds. for both			
Siphons each requiring 12.75 cu. yds. for intakes & outlets - 114.75 cu. yds. @ 22.50			- 2581.88
Deep Section 1605 lin. ft. 3" Concrete @ 1.62			- 2600.10
" " 1357 " " 3" " " 1.76			- 2388.32
" " 1860 " " 3" " " 2.16			- 4017.60
" " 1606 " " 3" " " 2.20			- 4336.20
			<u>101164.77</u>

To which must be added about \$7500 for cement.

7500
108665

GENERAL ESTIMATE OF CONDUIT.

Excavation	16991.4	Cu. Yds. Solid Rock	@ \$2.00	= \$33982.80
	3782.9	" " Loose	" " 1.00	- 3782.90
	.3782.9	" " Earth	" " .40	- 1513.16
				<u>39278.86</u>

Open Conduit 12194.94 lin.ft. lined 3" Concrete @ 1.35 - 16463.17
 This \$1.35 price based on the bid of \$13.50 per cu.yd.

Covered Conduit 1600.35 lin. ft. @ \$1.35 + 1.88-3.23 - 5169.13
 This \$1.88 price based on concrete at \$22.50 per cu.yd.

42" Reinforced Concrete Pipe 3148. lin. ft. @ \$5.00 - 15740.00

Trestle supporting siphon 279. lin ft. @ \$3.75 - 1046.25

Steel Flume on Concrete Trestle - Trestle Including				
		footings	\$3.75	
		Flume	3.04	
		Freight	.08	
Steel Flume 1098 lineal feet	@		<u>6.87</u>	- 7543.26

Inlet & outlet boxes - 12.75 cu. yds. for both

9 Siphons each requiring 12.75 cu. yds. for intakes & outlets - 114.75 cy. yds. @ 22.50 - 2581.88

Deep Section 1605 lin. ft. 3" Concrete @ 1.62 - 2600.10

" " 1357 " " 3" " " 1.76 - 2388.32

" " 1860 " " 3" " " 2.16 - 4017.60

" " 1606 " " 3" " " 2.20 - 4336.20

12194.94	101164.77
1600.35	30346.71
1605	131511.48
1357	3945.34
1860	<u>135456.82</u>
1606	

20223.29
 1098
 3148
24469.29

Conduit
 Flume

310 for Engineering
 Cement

Ed Fletcher Papers

1870-1955

MSS.81

Box: 47 Folder: 15

**Business Records - Water Companies - Volcan Land
and Water Company - San Dieguito System - San
Dieguito Mutual Water Company - Carroll Conduit
- Conduit design and estimate, with blue line map**



Copyright: UC Regents

Use: This work is available from the UC San Diego Libraries. This digital copy of the work is intended to support research, teaching, and private study.

Constraints: This work is protected by the U.S. Copyright Law (Title 17, U.S.C.). Use of this work beyond that allowed by "fair use" requires written permission of the UC Regents. Permission may be obtained from the UC San Diego Libraries department having custody of the work (<http://libraries.ucsd.edu/collections/mscl/>). Responsibility for obtaining permissions and any use and distribution of this work rests exclusively with the user and not the UC San Diego Libraries.